# PROVENANCE ANALYSIS BASED ON DETRITAL-ZIRCON-AGE SPECTRA OF THE LOWER CRETACEOUS FORMATIONS IN THE RYOSEKI–MONOBE AREA, OUTER ZONE OF SOUTHWEST JAPAN

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### ABSTRACT

Detrital-zircon-age spectra of the Lower Cretaceous Monobegawa and Nankai groups in the Ryoseki–Monobe area, Southwest Japan, are studied to make a provenance analysis and evaluate previous tectonic models. We also studied, for reference, the U-Pb zircon age of igneous rock cobbles, the detrital-zircon-age spectra of sandstone cobbles, and the detrital-zircon-age spectra of a sandstone samples of the Permian basement. The results are as follows. (1) The Ryoseki Formation of the Monobegawa Group contains many Permian zircons that were presumably reworked from the Permian basement sandstone. (2) The two groups contain Early Cretaceous detrital zircons and igneous rock cobbles of some 125 Ma, suggesting active acidic volcanism in the hinterland. (3) The Yunoki Formation of the Monobegawa Group contains 18% of 460–400 Ma zircons. It is concluded that the hinterland of the two groups were the Zhejiang–Fujian provinces of South China, where 145–100 Ma and 460–400 Ma felsic igneous rocks are widely exposed.

Key words : detrital zircon, Monobegawa Group, Nankai Group, provenance analysis, sinistral strike-slip motion, Southwest Japan

池田拓司・原田拓也・高地吉一・森田祥子・横川実和・山本鋼志・大藤 茂 (2016) 砕屑性ジルコン年代分布を用いた西南日本外帯領石―物部地域下部白亜系の後背地解析. 福井県立恐竜博物館紀要 15:33-84.

西南日本外帯高知県領石 - 物部地域に分布する,秩父累帯下部白亜系物部川層群及び南海層群砂岩の砕屑性ジルコンのウラン - 鉛年代を検討した.また,礫岩中の砂岩礫・火成岩礫及び物部川層群基盤のペルム系砂岩のジルコン年代も検討した.結果と考察は以下の通りである.①物部川層群領石層砂岩はペルム紀ジルコンを多量に含み,これらは基盤のペルム系砂岩からリワークされたと見られる.②両層群は前期白亜紀の砕屑性ジルコンを含み,火成岩礫のジルコン年代も約125 Maであることから,後背地では堆積と同時に活発な酸性火成活動が生じていた.③物部川層群柚ノ木層中部層砂岩は460-400 Maのジルコンを豊富に含む.以上より,両層群は,145-100 Ma及び460-400 Maの酸性火成岩が露出する南中国浙江省~福建省を後背地にしたと解釈した.

#### INTRODUCTION

Lower Cretaceous fluvial to shallow marine formations occur in the Chichibu Composite Belt in the Outer Zone of Southwest Japan. Tashiro (1985) and Tashiro and Ikeda (1987) divided them from lithofacies and faunal assemblages into the Monobegawa, Nankai, and Pre-Sotoizuimi groups (Tashiro, 1985; Tashiro and Ikeda, 1987). Tashiro (1985, 1986, 1994) suggested that the

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bivalve fauna of the Nankai Group (Tethyan Fauna) indicates a warmer environment than that of the Monobegawa Group (Northern-Tethyan Fauna) and that the Nankai Group formed to the south of the Monobegawa Group. Since the Nankai Group lies on the Pacific side of the Monobegawa Group, Tashiro (1985, 1986, 1994) presumed that an arc-subparallel sinistral strike-slip fault lay between the two groups and had carried the Nankai Group relatively northward by the Albian. Matsukawa and Eto (1987), on the other hand, attributed the lithofacies and faunal differences between the two groups in the Katsuura area of Tokushima Prefecture, 80 km to the east of the study area, to the differences in sedimentary environments and ocean currents

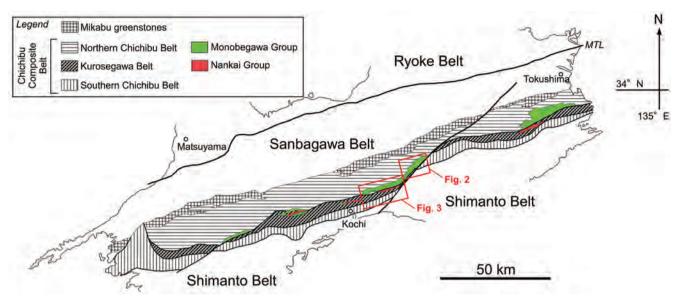


FIGURE 1. Index map showing the distribution of the Lower Cretaceous strata of the Chichibu Composite Belt and the locations of the Monobe and Ryoseki–Birafu areas drawn in Figs. 2 and 3. Modified after Yamakita (1998).

in a single sedimentary basin. They, however, also suggested a possibility of the initial separation of the basin because of the difference in clast composition of Hauterivian conglomerate in the two groups. Recent studies, reporting the presence of Tethyan–North-Tethyan mixed fauna, tend to argue that the sinistral strikeslip model only cannot explain the faunal distribution in the Monobegawa and Nankai groups (Kozai and Ishida, 2003; Kozai et al., 2007; Terabe and Matsuoka, 2009).

The Cretaceous sinistral strike-slip faulting has likely affected the distribution of Mesozoic plant fossils and major pre-Aptian geologic units of Japan. Berriasian (?)-Barremian plant fossils in the continental side of Japan (Tetori-type flora) contain many common taxa with those of Northeast China and southeast Siberia. On the other hand, Oxfordian-Barremian plant fossils in the Pacific side of Japan (Ryoseki-type flora) contain many common taxa with those of South China and the Indochina and Malay peninsulas (Kimura, 1987); the Ryoseki-type flora invaded into the continental side of Japan in the Aptian (Yabe et al., 2003). The floral contrast between the continental and Pacific sides of Japan can also be explained by an arc-parallel sinistral strike-slip fault in between that carried the geologic units with the Ryoseki-type flora relatively northward (e.g., Otoh and Yanai, 1996). The sinistral strike-slip faults can be responsible for the duplication of the pairs of pre-Aptian accretionary and non-accretionary geologic units in the continental and Pacific sides of Japan (e.g., Taira and Tashiro, 1987; Yamakita and Otoh, 2000a, b). Yamakita and Otoh (2000a, b) attributed the duplication of Permian accretionary complex (AC) in the Inner and Outer zones of Southwest Japan to the Late Cretaceous sinistral strike-slip motion along the Median Tectonic Line (MTL).

We have started provenance analysis of the Jurassic and Cretaceous formations in Japan to validate the hypothesis of the Cretaceous strike-slip faulting. In particular, detrital zircon age spectra, which reflect the changes of provenance, paleogeography, and tectonic setting, can be a powerful tool for evaluating large-scale displacements caused by plate motion (e.g., Okawa et al., 2013). In this paper, we will present the detrital zircon age spectra of sandstone samples from all the formations of the Lower Cretaceous Monobegawa and Nankai groups in the Ryoseki–Monobe area, Outer Zone of Southwest Japan (Fig. 1). We will also provide the U-Pb zircon age of igneous rock cobbles and the detrital zircon age spectra of sandstone cobbles from the conglomerate of the two groups. Moreover, we will present the detrital zircon age spectra of two pre-Cretaceous sandstone samples of the Chichibu Composite Belt for comparison. Finally, we will compare the provenance transitions of the two groups and verify the sinistral strike-slip and other related models.

### GEOLOGIC SETTING

The Chichibu Composite Belt comprises three belts: the Northern Chichibu, Kurosegawa, and Southern Chichibu belts from the continental side (from present-day north to south; Yamakita, 1998). The Northern Chichibu Belt consists of a Jurassic AC, tectonically overlying Permian AC, and the unconformably covering Lower Cretaceous Monobegawa Group. The Kurosegawa Belt consists of the following geologic bodies that have been cut and fragmented by belt-subparallel faults: pre-Jurassic metamorphic rocks, serpentinite, pre-Carboniferous basement rocks, Permian (?) chaotic rocks, Permian–Jurassic shallow marine beds, Jurassic chaotic rocks, and the Lower Cretaceous Nankai Group partly covering the Upper Jurassic-lowest Cretaceous Torinosu Group (Yamakita, 1998). The Southern Chichibu Belt consists mainly of late Early Jurassic to

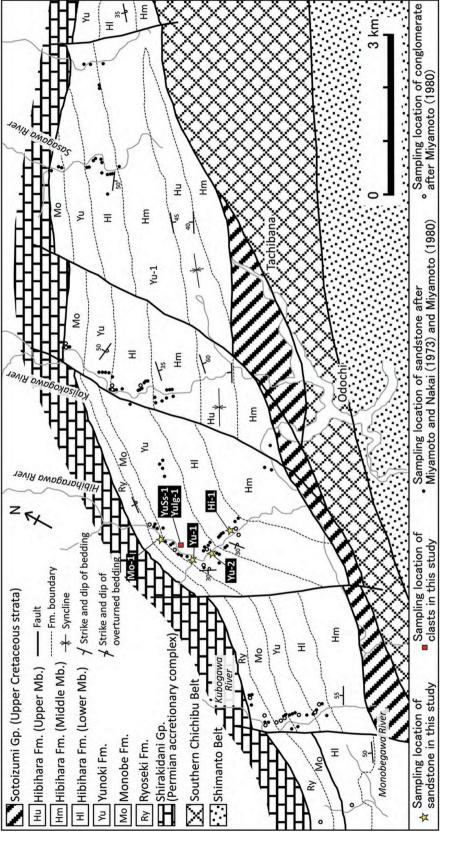


FIGURE 2. Geologic map of the Monobe area showing the sampling locations. Modified after Tashiro and Kozai (1984). Gp.: Group, Fm.: Formation, Mb.: Member.

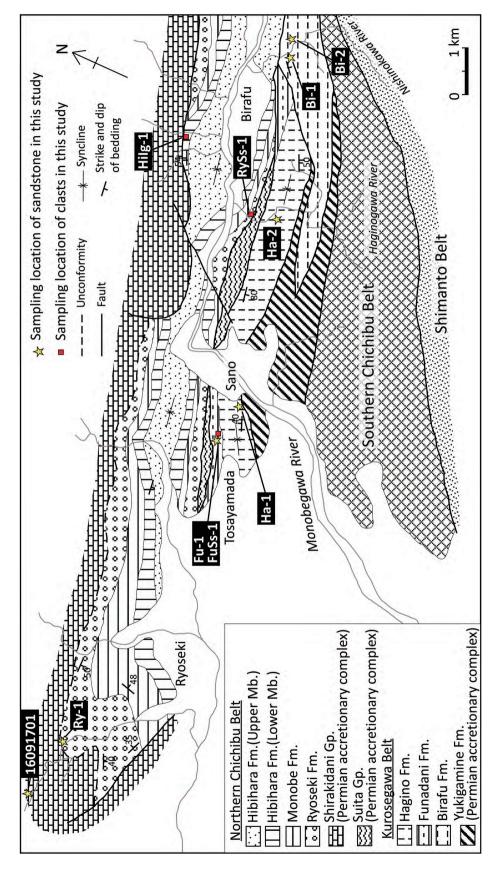


FIGURE 3. Geologic map of the Ryoseki-Birafu area showing the sampling locations. Modified after Kozai (2008). Gp.: Group, Fm.: Formation, Mb.: Member.

earliest Cretaceous AC, partly covered with the Middle Jurassic to earliest Cretaceous Naradani and Torinosu groups (Matsuoka et al., 1998).

The Monobegawa Group in the Ryoseki-Monobe area is in fault contact with or unconformably covers the Permian Shirakidani Group (AC) of the Northern Chichibu Belt on the north (Ikuma, 1980). The group is in fault contact with the Permian Suita Group, Lower Cretaceous Nankai Group, and Upper Cretaceous Sotoizumi Group on the south (Kozai et al., 2006; Hada et al., 1982; Figs. 2 and 3). The Monobegawa Group consists of the Ryoseki (Hauterivian-lowest Barremian), Monobe (Barremian), Yunoki (Aptian-lower Albian), and Hibihara (Albian) formations in ascending order and is composed mainly of siliciclastic rocks such as conglomerate, sandstone, and mudstone. Among the four formations, the Monobe Formation was originally a member of the Ryoseki Formation; Tanaka et al. (1984) separated the upper marine part of the Ryoseki Formation of the day as the Monobe Formation. The lower three formations form a conformable sequence whereas the Hibihara Formation likely covers the Yunoki Formation by disconformity (Tanaka et al., 1984; Tashiro, 1985; Fig. 4). Moreover, the Yunoki Formation does not occur in the Birafu-Ryoseki area on the west of the Kubokawa River (Kozai, 2008; Fig. 2). The Ryoseki Formation is likely of fluvial to brackish deposits because of the abundance of red beds in the lower part and the occurrence of the Ryosekitype flora in the upper part (Tanaka et al., 1984). The Monobe to Hibihara formations, on the other hand, are of brackish to marine deposits substantiated by abundant fossil fauna (Tashiro, 1985; Tanaka et al., 1984).

The Nankai Group in the study area consists of the Birafu (Oxfordian-Valanginian or Hauterivian), Funadani (upper Hauterivian-Barremian), and Hagino (Aptian) formations, in ascending order, and is in fault contact with the Suita and Monobegawa groups and the Permian Yukigamine Formation (Kozai et al., 2006; Fig. 3). The Nankai Group is mostly of brackish to marine deposits (Kozai and Ishida, 2000; Morino, 1993; Tashiro, 1985). There are some conflicting views on the position of the Birafu Formation. Morino et al. (1989) first defined the formation as a siliciclastic-rock formation with some Torinosutype limestone bodies. He assigned the Birafu Formation to a member of the Nankai Group, for two reasons. First, the mudstone in the formation contained late Valanginian to Barremian radiolarians and was significantly younger than the Torinosu Group, despite the occurrence of the Torinosu-type limestone. Secondly, the formation contained many bivalve species common with those of the Nankai Group. Kozai et al. (2004), on the other

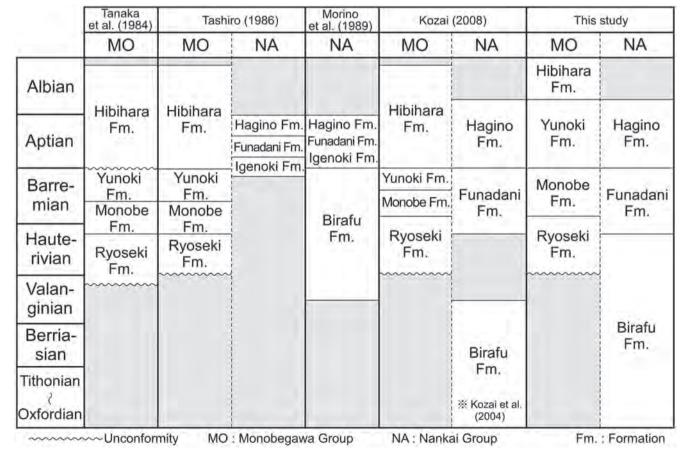


FIGURE 4. Stratigraphic correlation of the Upper Jurassic to Lower Cretaceous strata in the Ryoseki-Monobe area.

hand, separated the Birafu Formation from the Nankai Group, for three reasons. First, radiolarian and bivalve fossils indicated that the formation was of the Oxfordian to the early Valanginian and was significantly older than the Hauterivian?—Barremian Funadani Formation (Kozai, 2008), which was the oldest formation of the

Nankai Group. Secondly, the Birafu Formation is in fault contact with the Nankai Group. Finally, the southward-dipping and facing Birafu Formation is discordant in geologic structure with the Nankai Group on the north, forming a syncline. In this paper, we assign the Birafu Formation as a member of the Nankai Group

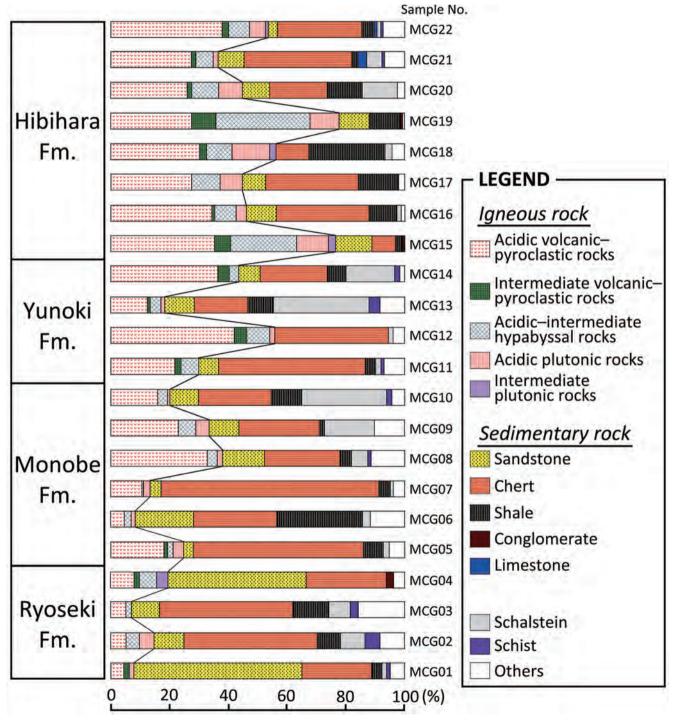


FIGURE 5. Clast compositions of the conglomerate samples from the Monobegawa Group published by Miyamoto and Nakai (1974) and Miyamoto (1980). Fm.: Formation.

from the following reasons: (1) a sandstone sample from the middle part of the Birafu Formation contains Valanginian zircons, as will be described later, and is presumably of the Valanginian or younger age; and (2) the Birafu Formation lies adjacent to the Nankai Group although a fault runs in between.

### A REVIEW OF PETROGRAPHIC STUDIES OF THE LOWER CRETACEOUS CLASTIC ROCKS IN THE STUDY AREA

In this section, we will review petrographic studies of the Lower Cretaceous clastic rocks in the Ryoseki–Monobe area. Since there are differences in the distribution of each formation among the previous studies, all the sample locations of the previous studies have been plotted on the geologic map of Tashiro and Kozai (1984) and used their formation names for description.

#### Clast composition of conglomerates of the Monobegawa Group

Miyamoto and Nakai (1974) and Miyamoto (1980) made precise petrographic studies of the Monobegawa Group in the study area. According to the studies, the Monobegawa Group contained various kinds of clasts such as igneous-, sedimentary-, and metamorphic-rock clasts. There was a tendency that sedimentary-rock clasts prevailed in the lower part, whereas felsic-to intermediate-igneous-rock clasts increased upwards (Fig. 5). Sedimentary-rock clasts consisted mainly of chert, sandstone, and shale, among which chert clasts were most abundant. In some conglomerate horizons of the Ryoseki Formation, sandstone clasts were exceptionally more than chert clasts. The average proportion of the sedimentary-rock clasts in the Ryoseki (R), Monobe (M), Yunoki (Y), and Hibihara (H) formations was 72.8%, 59.3%, 43.1%, and 39.2%, respectively. On the other hand, the average proportion of the felsic to intermediate igneous rock clasts in the four formations was 12.5% (R), 23.1% (M), 37.1% (Y), and 54.7% (H), in ascending order. The conglomerates also contained small amounts of "schalstein" and metamorphic-rock clasts.

#### Sandstone modal composition of the Monobegawa Group

According to the classification of Okada (1971), the sandstone of the four formations of the Monobegawa Group was mostly assigned to lithic wacke (R; Ryoseki Formation), lithic wacke (M; Monobe Formation), lithic to feldspathic wacke (Y; Yunoki Formation), and feldspathic wacke (H; Hibihara Formation), in ascending order (Miyamoto and Nakai, 1974; Miyamoto, 1980; Fig. 6). Only one sample from the Yunoki Formation and three samples from the Hibihara Formation were assigned to arenite out of the 103 sandstone samples they studied. Thus, the greywacke type sandstone, relatively rich in the matrix, represents the Monobegawa Group. The average proportions of quartz, feldspar, rock fragments, and the matrix in the four formations were as follows. Quartz grains were 13.3% (R), 22.2% (M), 22.2% (Y), and 19.1% (H); feldspar grains were 13.8% (R), 20.8% (M), 28.8% (Y), and 37.1% (H); rock fragments were

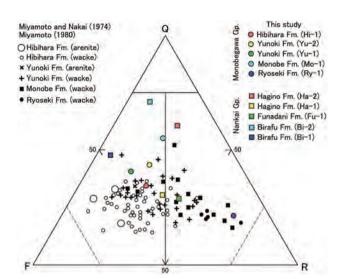


FIGURE 6. A Q-F-R diagram showing the sandstone compositions of the Monobegawa and Nankai groups provided by Miyamoto and Nakai (1974), Miyamoto (1980), and this study. Gp.: Group, Fm.: Formation, Q: quartz, F: feldspar, R: rock fragments.

36.8% (R), 32.4% (M), 22.1% (Y), and 20.0% (H); and the matrix was 36.1% (R), 24.6% (M), 26.9% (Y), and 23.8% (H). There are overall trends that the proportions of rock fragments and the matrix decrease and feldspar grains increase upwards. Miyamoto (1980) described species of rock fragments and their proportions, along the Kubokawa River route, suggesting that the ratio of sedimentary rock fragments decreased and volcanic rock fragments increased upwards (Fig. 7). The trend is concordant with the upward transition of clast proportion in conglomerates.

#### Lithology of the clastic rocks of the Nankai Group

Morino (1993) described that the Birafu Formation consisted mainly of mudstone and interbedded arkose sandstone and mudstone, with minor intercalations of the Torinosu-type limestone, sandstone, conglomerate, and tuff. The clasts of conglomerates were mostly pebble to granule size and consisted chiefly of greenish gray chert, with minor amounts of reddishbrown chert and granitic rocks (Morino et al., 1989). The Funadani Formation contained thick conglomerate beds having the clasts of chert and sandstone, with minor amounts of tuffaceous sandstone and limestone. The Hagino Formation was characterized by a repetitive occurrence of medium to fine sandstone, rich in arenite, and gray silty mudstone (Tashiro, 1993). Moreover, the formation in the Sano area (former Igenoki Formation; Kozai, 2008; Fig. 3) intercalated conglomerate with felsic igneous rock clasts in the bed of the Monobegawa River (Kozai and Ishida, 2000). The Nankai Group as a whole was characterized by the absence of red clastic rocks and abundance of arenite (Tashiro, 1985). Moreover, the occurrence of felsic igneous rock clasts in the conglomerate and arkose sandstone from each formation indicated the exposure of felsic igneous bodies in the provenance.

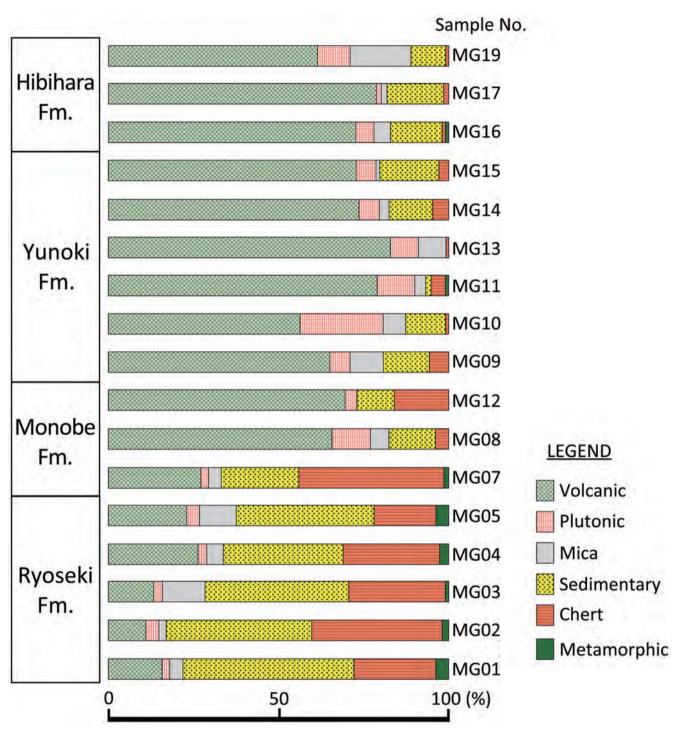


FIGURE 7. Compositions of rock fragments in sandstone samples of the Monobegawa Group published by Miyamoto and Nakai (1974) and Miyamoto (1980). Fm.: Formation.

### Paleocurrent and sediment transport

Miyamoto (1980) concluded from the slump structures and sole marks developed in the Hibihara Formation in the study area that there was a land to the north (in the present coordinate) of the

sedimentary basin and that the clastic sediments were supplied from north to south. Miyamoto (1980) further proposed that Early Cretaceous igneous rock bodies that were exposed along the southern boundary of the Ryoke Belt but were completely eroded away supplied the igneous-rock clasts of the Monobegawa Group

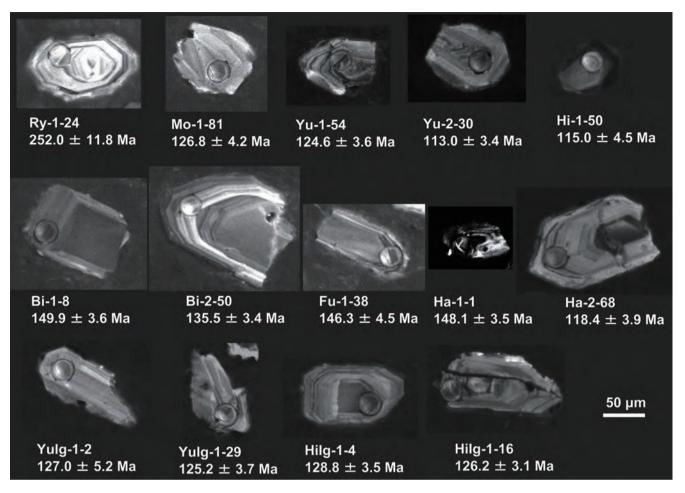


FIGURE 8. Cathodoluminescence images of some zircons analyzed in this study. For grain numbers, see Table 1.

in the study area. Kozai and Ishida (2000), on the other hand, found an Early Devonian radiolarian *Devoniglanssus unicus* from a tuffaceous-sandstone clast of the Funadani Formation of the Nankai Group. Since the radiolarian species had commonly been reported from the tuffaceous sandstone in the G4 horizon of the Yokokurayama Group (Wakamatsu et al., 1990), they suggested that the clast was derived from the Siluro–Devonian of the Kurosegawa Belt.

In summary, the source of sedimentary-rock clasts in the conglomerate and sandstone of the Monobegawa Group in the study area is likely the pre-Cretaceous rocks of the Northern Chichibu Belt. The reasons are as follows: (1) the Monobegawa Group unconformably covers the Permian AC of the Northern Chichibu Belt; (2) the pre-Cretaceous AC of the Northern Chichibu Belt mainly occur on the north of the Monobegawa Group and sedimentary structures indicate the sediment supply from the north; and (3) the sediment source of the Monobegawa Group in the Katsuura area has been proposed to have been the pre-Cretaceous rocks of the Northern Chichibu Belt (Ishida and Hashimoto, 1997; Matsukawa and Eto, 1987; Ogawa, 1971). A sediment source of the Nankai Group was likely a geologic entity that now constitutes

the Kurosegawa Belt (Kozai and Ishida, 2000).

#### SAMPLE DESCRIPTIONS

We studied the following seventeen samples: (1) five sandstone samples from the Monobegawa Group, (2) five sandstone samples from the Nankai Group, (3) three sandstone cobbles from the Ryoseki, Yunoki, and Funadani formations, (4) two igneous rock cobbles from the Yunoki and Hibihara formations, and (5) two sandstone samples from the Shingai Unit and Shirakidani Group, members of the Permian AC of the Northern Chichibu Belt. Here follows the description of the samples studied. The modal composition of a sandstone sample was measured from a thin-section using a petrological microscope and an automatic point counter. We counted five hundred points for each sandstone sample (three hundred points for each sandstone cobble) and calculated the percentages of (1) single quartz, (2) single feldspar, (3) the rock fragment, including chert fragments and mineral grains other than quartz and feldspar, and (4) matrix.

#### Monobegawa Group

# Sandstone of the Ryoseki Formation (Sample Ry-1; 33° 37' 11.67" N, 133° 36' 39.87" E)

Sample Ry-1 of the Ryoseki Formation was collected from an exposure of the lowermost part of the formation on the northern side of Kochi Prefectural Road 269 along the Kasanokawa River (Fig. 3). The sample was of non-marine, red, ill-sorted, angular to sub-rounded, medium- to coarse-grained lithic wacke in the sense of Okada (1971), consisting of quartz (12.2%), feldspar (7.8%), rock fragments (37.2%), and matrix (42.8%). The rock fragments were mostly of sedimentary and metamorphic rocks with volcanic rocks and chert. The metamorphic rock fragments were mostly of an aggregate of elongated quartz grains with sutured grain boundaries and the longest dimensions arranging subparallel to each other (sheared quartz or stretched metamorphic quartz). Among the zircon grains we collected, 43% were euhedral, and 57% were abraded. They were mostly colorless, and only 3% were purple. The euhedral zircons had the aspect ratio of 1.2–3.0 (2.0 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# Sandstone of the Monobe Formation (Sample Mo-1; $33^{\circ}$ 42' 51.15" N, $133^{\circ}$ 50' 05.49" E)

Sample Mo-1 of the Monobe Formation was collected from an exposure of the lower part of the formation along the Hibiharagawa River (Fig. 2). The sample was of light-gray, moderately- to well-sorted, sub-angular to rounded feldspathic arenite, consisting of quartz (48.1%), feldspar (20.3%), rock fragments (18.6%), and matrix (13.0%). Among the zircon grains we collected, 62% were euhedral, and 38% were abraded. They were mostly colorless, and 6% were purple or brown. The euhedral zircons had the aspect ratio of 1.0–3.3 (2.0 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# Sandstone of the lower part of the Yunoki Formation (Sample Yu-1; 33° 42' 31.17" N, 133° 50' 01.71" E)

Sample Yu-1 of the Yunoki Formation was collected from an exposure of the Lower Marine Member (Tanaka et al., 1984) along the Hibiharagawa River (Fig. 2). The sample was of lightgray, moderately-sorted, sub-angular to sub-rounded mediumgrained feldspathic arenite, consisting of quartz (38.0%), feldspar (38.8%), rock fragments (15.2%), and matrix (8.0%). Among the zircon grains we collected, 65% were euhedral, and 35% were abraded. They were mostly colorless, and 5% were purple. The euhedral zircons had the aspect ratio of 1.5–2.8 (2.1 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# Sandstone of the middle part of the Yunoki Formation (Sample Yu-2; 33° 42' 23.83" N, 133° 50' 13.85" E)

Sample Yu-2 of the Yunoki Formation was collected from an exposure of the Middle Non-marine Member (Tanaka et al., 1984) along the Hibiharagawa River (Fig. 2). The sample was of dark-gray, ill-sorted, sub-angular to sub-rounded, fine- to very fine-grained feldspathic wacke with abundant carbonized plant fragments. The sample consisted of quartz (23.2%), feldspar

(18.2%), rock fragments (11.7%), and matrix (47.0%). Among the zircon grains we collected, 68% were euhedral, and 32% were abraded. They were mostly colorless, and 4% were purple. The euhedral zircons had the aspect ratio of 1.4–3.0 (2.1 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# Sandstone of the Hibihara Formation (Sample Hi-1; $33^{\circ}$ 42' 15.36" N, $133^{\circ}$ 50' 34.28" E)

Sample Hi-1 of the Hibihara Formation was collected from an exposure of the Middle Marine Member (Tanaka et al., 1984) along the Hibiharagawa River (Fig. 2). The sample was of darkgray, ill- to moderately-sorted, sub-angular to sub-rounded, fine-to very fine-grained feldspathic wacke, consisting of quartz (17.6%), feldspar (20.6%), rock fragments (13.0%), and matrix (48.8%). Among the zircon grains we collected, 39% were euhedral, and 61% were abraded. They were mostly colorless, and 3% were purple. The euhedral zircons had the aspect ratio of 1.3–2.8 (1.9 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

### Nankai Group

# Sandstone of the lower part of the Birafu Formation (Sample Bi-1; 33° 38' 55.27" N, 133° 47' 52.38" E)

Sample Bi-1 of the Birafu Formation was collected from an exposure of the A2 Member (Kozai et al., 2004, 2006) along the Nishinokawa River (Fig. 3). The sample was of gray, moderately-to well-sorted, sub-angular to rounded, very fine-grained feldspathic arenite, consisting of quartz (43.0%), feldspar (42.6%), rock fragments (4.8%), and matrix (9.6%). Among the zircon grains we collected, 67% were euhedral, and 33% were abraded. They were mostly colorless, and only 1% were purple. The euhedral zircons had the aspect ratio of 1.5–2.7 (2.1 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# Sandstone of the middle part of the Birafu Formation (Sample Bi-2; 33° 38' 55.66" N, 133° 48' 07.93" E)

Sample Bi-2 of the Birafu Formation was collected from an exposure of the B1 or B2 Member on the eastern side of Kochi Prefectural Road 30 along the Nishinokawa River (Fig. 3). The sample was of white, ill- to moderately-sorted, angular to rounded, coarse-grained feldspathic arenite, consisting of quartz (70.9%), feldspar (20.2%), rock fragments (8.7%), and matrix (0.2%). Among the zircon grains we collected, 62% were euhedral, and 38% were abraded. They were mostly colorless, and 7% were purple or brown. The euhedral zircons had the aspect ratio of 1.6–4.0 (2.1 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# Sandstone of the Funadani Formation (Sample Fu-1; $33^{\circ}$ 37' 22.79" N, $133^{\circ}$ 41' 59.69" E)

Sample Fu-1 of the Funadani Formation was collected from an exposure near the Meoto Pond (Fig. 3). The sample was of weathered, brown, moderately-sorted, sub-angular to rounded, fine- to medium-grained lithic wacke, consisting of quartz (22.4%), feldspar (24.4%), rock fragments (32.3%), and matrix (20.9%).

Among the zircon grains we collected, 65% were euhedral, and 35% were abraded. They were mostly colorless, and 8% were purple or brown. The euhedral zircons had the aspect ratio of 1.6–3.3 (2.1 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# Sandstone of the Hagino Formation from Sano (Sample Ha-1; 33° 37' 16.89" N, 133° 42' 42.87" E)

Sample Ha-1 of the Hagino Formation was collected from an exposure in Sano (Fig. 3). The sample was of weathered, brown, well-sorted, sub-angular to rounded, fine- to very fine-grained feldspathic wacke, consisting of quartz (22.0%), feldspar (26.2%), rock fragments (25.4%), and matrix (26.4%). Among the zircon grains we collected, 61% were euhedral, and 39% were abraded. They were mostly colorless, and 3% were brown. The euhedral zircons had the aspect ratio of 1.4–5.0 (2.4 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# Sandstone of the Hagino Formation from Hagino (Sample Ha-2; 33° 38' 03.12" N, 133° 45' 25.74" E)

Sample Ha-2 of the Hagino Formation was collected from an exposure along the Haginogawa River in Hagino (Fig. 3). The sample was of light-gray, moderately- to well-sorted, angular to rounded, medium- to coarse-grained lithic arenite, consisting of quartz (60.8%), feldspar (14.8%), rock fragments (24.2%), and matrix (0.2%). Among the zircon grains we collected, 60% were euhedral, and 40% were abraded. They were mostly colorless, and 5% were purple or brown. The euhedral zircons had the aspect ratio of 1.4–3.4 (2.0 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

#### Cobbles from conglomerate

# A sandstone cobble from the Ryoseki Formation, Monobegawa Group (Sample RySs-1; 33° 38' 17.23" N, 133° 45' 23.01" E)

Sample RySs-1 was collected from an exposure of conglomerate of the Ryoseki Formation, Monobegawa Group, along the Haginogawa River (Fig. 3). The sample was of a subangular cobble of dark-gray, ill-sorted, angular to sub-rounded, coarse-grained lithic arenite, consisting of quartz (38%), feldspar (13.7%), rock fragments (37%), and matrix (11.3%). Among the zircon grains we collected, 53% were euhedral, and 47% were abraded. They were mostly colorless. The euhedral zircons had the aspect ratio of 1.3–2.7 (2.0 in average). Most of the collected zircons showed oscillatory zoning in CL images.

### A sandstone cobble from the Yunoki Formation, Monobegawa Group (Sample YuSs-1; 33° 42' 43.20" N, 133° 50' 06.09" E)

Sample YuSs-1 was collected from an exposure of conglomerate of the middle part of the Yunoki Formation, Monobegawa Group, along the Hibiharagawa River (Fig. 2). The sample was of a round cobble of dark-gray, moderately-sorted, sub-angular to sub-rounded, medium- to coarse-grained feldspathic arenite, consisting of quartz (37.3%), feldspar (31.3%), rock fragments (25.3%), and matrix (6%). Among the zircon grains we collected, 56% were euhedral, and 44% were abraded. They were mostly colorless, and 8% were purple. The euhedral zircons had the aspect ratio of 1.1–2.6 (1.9 in average). Most of

the collected zircons showed oscillatory zoning in CL images.

### A sandstone cobble from the Funadani Formation, Nankai Group (Sample FuSs-1; 33° 37' 21.28" N, 133° 42' 02.22" E)

Sample FuSs-1 was collected from an exposure of conglomerate of the Funadani Formation, Nankai Group, near the Meoto Pond (Fig. 3). The sample was of a subround cobble of dark-gray, ill-sorted, angular to sub-rounded, medium-grained feldspathic arenite, consisting of quartz (36.8%), feldspar (43.4%), rock fragments (10.6%), and matrix (9.3%). Among the zircon grains we collected, 68% were euhedral, and 32% were abraded. They were mostly colorless, and only 1% were purple. The euhedral zircons had the aspect ratio of 1.4–2.8 (1.7 in average). Most of the collected zircons showed oscillatory zoning in CL images.

### A rhyolite cobble from the Yunoki Formation, Monobegawa Group (Sample YuIg-1; 33° 42' 43.20" N, 133° 50' 06.09" E)

Sample YuIg-1 was collected from the same exposure with sample YuSs-1 (Fig. 2). The sample was of a round cobble of rhyolite with quartz and plagioclase phenocrysts floated in a groundmass (Fig. 9a-c). Among the zircon grains we collected, 78% were euhedral, and 22% were abraded. They were mostly colorless, and 5% were purple or brown. The euhedral zircons had the aspect ratio of 1.5–3.2 (2.2 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

# A granodiorite cobble from the Hibihara Formation, Monobegawa Group (Sample Hilg-1; 33° 39' 34.69" N, 133° 46' 01.87" E)

Sample HiIg-1 was collected from an exposure of conglomerate of the Hibihara Formation, Monobegawa Group, along a northern branch of the Monobegawa River (Fig. 3). The sample was of a round cobble of granodiorite with quartz, plagioclase, and minor chlorite (Fig. 9d-f). Among the zircon grains we collected, 92% were euhedral, and 8% were abraded. They were mostly colorless, and 3% were brown. The euhedral zircons had the aspect ratio of 1.3–3.6 (2.1 in average). Most of the collected zircons showed oscillatory zoning in CL images (Fig. 8).

### Pre-Cretaceous sandstone of the Northern Chichibu Belt

# Sandstone of the Shingai Unit (Sample 13072103; 33 $^{\circ}$ 36' 16.44" N, 133 $^{\circ}$ 28' 22.83" E)

The Shingai Unit is a geologic unit of the Permian AC of the Northern Chichibu Belt, correlative to the Shirakidani Group in the Ryoseki area (Fig. 3). The Shingai Unit consists mainly of sandstone, mudstone, chert, basalt, and limestone (Wakita et al., 2007). Sample 13072103 was collected from an exposure along the Kochi Prefectural Road 33 at Kagamiimai, Kochi City. The sample was of grayish-green, moderately sorted, fine- to mediumgrained lithic arenite, consisting of quartz (32.9%), feldspar (14.2%), rock fragments (52.9%), and matrix (12.8%). The rock fragments were mostly of volcanic rocks. Among the zircon grains we collected, 56% were euhedral, and 44% were abraded. They were mostly colorless, and 2% were purple or brown. Most of the collected zircons showed oscillatory zoning in CL images.

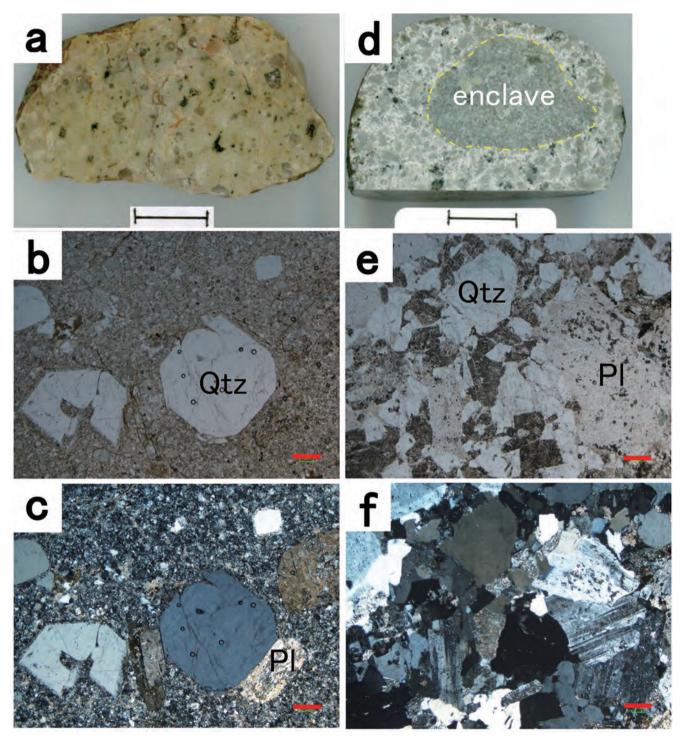


FIGURE 9. Photographs of studied igneous-rock clasts. **a–c**, A rhyolite clast from the Yunoki Formation (sample YuIg-1). **a**, A hand specimen (Scale bar = 1.0 cm); **b**, A photomicrograph (Open nicol; Scale bar = 0.2 mm). **d–f**, A granodiorite clast from the Hibihara Formation (HiIg-1). **d**, A hand specimen (Scale bar = 1.0 cm); **e**, A photomicrograph (Open nicol; Scale bar = 0.2 mm); **f**, A photomicrograph (Crossed nicols; Scale bar = 0.2 mm). Qtz: quartz, Pl: plagioclase.

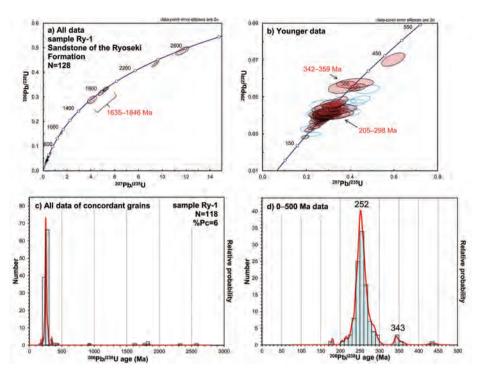


FIGURE 10. Analytical data of detrital zircons from sandstone of the Ryoseki Formation (sample Ry-1). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with a histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. Open (light blue) circles in the concordia diagrams from Fig. 10 to Fig. 26 show the analytical data for discordant grains. N: total number, %Pc: percentage of Precambrian zircons.

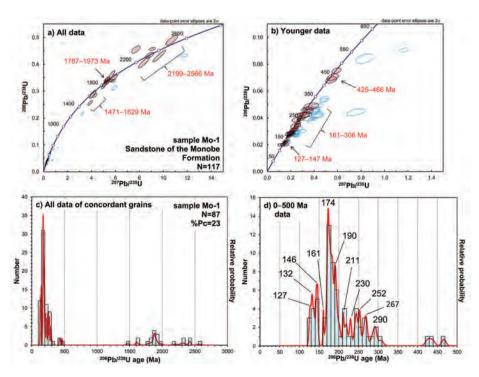


FIGURE 11. Analytical data of detrital zircons from sandstone of the Monobe Formation (sample Mo-1). **a,** Concordia diagram for all data; **b,** Concordia diagram for a younger data set; **c,** Probability density plot with a histogram for all data of concordant grains; **d,** Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

# Sandstone of the Shirakidani Group (Sample 16091701; $33^{\circ}$ 37' 16.18" N, $133^{\circ}$ 35' 47.18" E)

The Shirakidani Group is a geologic unit of the Permian AC of the Northern Chichibu Belt in the Ryoseki area (Fig. 3). The Shirakidani Group consists mainly of sandy mudstone, sandstone, and mudstone, with blocks (olistoliths; Suyari et al., 1983) of chert, limestone, and basaltic tuff and lava. Sample 16091701 of the Shirakidani Group was collected from an exposure on the northern side of Kochi Prefectural Road 269 along the Kasanokawa River (Fig. 3). The sample was of gray, moderatelyto ill-sorted, sub-angular to rounded, medium- to coarse-grained lithic arenite, consisting of quartz (18%), feldspar (24.4%), rock fragments (51.2%), and matrix (6.4%). The rock fragments were mostly of volcanic rocks. Among the zircon grains we collected, 50% were euhedral, and 50% were abraded. They were mostly colorless, 2% were purple, and 5% were brown. The euhedral zircons had the aspect ratio of 1.4-4.3 (2.2 in average). Most of the collected zircons showed oscillatory zoning in CL images.

#### ANALYTICAL METHOD

The zircon samples for analyses were prepared following the procedures described in Kawagoe et al. (2012). The measurement was carried out on laser ablation inductively coupled plasma mass spectrometers (LA-ICPMS) equipped in the Graduate School of Environmental Studies, Nagoya University. The ICPMS instrument was an Agilent 7700x quadrupole-based ICPMS connected with a New Wave Research NWR-213-type LA system, which used the frequency quintupled Nd-YAG 213-nm wavelength. The measurement conditions, optimized to reduce matrix effects, were as follows: energy density of 11.7 J/cm<sup>-2</sup>, pulse repetition rate of 10 Hz, pre-ablation time of 8 s, ablation time of 10 s, and the ablation pit size of 25  $\mu$ m (Kouchi et al., 2015). The analyses were carried out in a peak-jumping mode, and the peaks of <sup>202</sup>Hg, <sup>204</sup>(Hg+Pb), <sup>206</sup>Pb, <sup>207</sup>Pb, <sup>232</sup>Th, and <sup>238</sup>U were monitored. Data were acquired in sequences of 28 analyses, consisting of 5 analyses of gas blank, 4 NIST (National Institute of Standards and Technology, U.S.A.) SRM 610 glass standard, one standard zircon (91500 zircon with the <sup>206</sup>Pb/<sup>238</sup>U age of 1062.4 ± 0.4 Ma; Wiedenbeck et al., 2004), nine unknown, 4 SRM 610 standard, and five gas blank.

### **RESULTS**

We sampled an outer part (rim or mantle) of collected zircon grains with the laser ablation technique and analyzed with the ICPMS. After the analyses, we plotted all the data on a concordia diagram. Then we chose concordant grains with the %conc value  $(100 \cdot (^{206}\text{Pb}/^{238}\text{U age})/(^{207}\text{Pb}/^{235}\text{U age}))$  between 90 and 110 and drew a probability density plot and a histogram with the data interval of 50 Myr  $(^{206}\text{Pb}/^{238}\text{U age})$ . Among the peaks in the probability density plot that consist of two or more zircon data, the youngest one will be designated as the youngest peak (YP) in this paper. The data processing was carried out using the Isoplot 4.15 software (Ludwig, 2012). Here follow the results of our analyses.

#### Monobegawa Group

#### Sandstone of the Ryoseki Formation (Sample Ry-1)

We obtained 128 analyses from 128 zircon grains collected from sandstone sample Ry-1 of the Ryoseki Formation. 118 grains out of 128 gave concordant results (Fig. 10). We detected three age groups and five single plots of concordant detrital zircons on the concordia diagram: 205–298 Ma (105 grains; 89% of 118 concordant grains), 342–359 Ma (3%), 1635–1846 Ma (3%), 180 Ma (1%), 437 Ma (1%), 929 Ma (1%), 2318 Ma (1%), and 2552 Ma (1%) (Each age denotes the <sup>206</sup>Pb/<sup>238</sup>U age at the centers of the youngest and oldest age plots of each cluster or at the center of each single plot.) (Fig. 10a, b). The percentage of Precambrian zircons (%Pc) was 6, and the 206Pb/238U age of the youngest zircon (YZ) was 179.8 ± 4.8 Ma. The probability density plot for the 0–500 Ma data set showed a single peak at 252 Ma (Fig. 10d).

#### Sandstone of the Monobe Formation (Sample Mo-1)

We obtained 117 analyses from 117 zircon grains collected from sandstone sample Mo-1 of the Monobe Formation. 87 grains out of 117 gave concordant results (Fig. 11). We detected six age groups of concordant zircons: 161–306 Ma (60%), 127–147 Ma (14%), 1787–1973 Ma (13%), 2199–2566 Ma (7%), 425–466 Ma (3%), and 1471–1629 Ma (3%), with %Pc of 23 and the YZ of 126.8  $\pm$  4.2 Ma (Fig. 11a–c). The probability density plot for the 0–500 Ma data set showed the largest peak at 174 Ma, second largest peaks at 146 Ma and 190 Ma, and small peaks at 127 Ma, 132 Ma, 161 Ma, 211 Ma, 230 Ma, 244 Ma, 252 Ma, 267 Ma, and 290 Ma (Fig. 11d). The youngest peak (YP) was at 127 Ma, and the concordant age of the three grains that constitute the 127 Ma peak was 127.4  $\pm$  2.9 Ma (MSWD = 0.14, Probability = 0.71).

# Sandstone of the lower part of the Yunoki Formation (Sample Yu-1)

We obtained 131 analyses from 131 zircon grains collected from sandstone sample Yu-1 of the lower part of the Yunoki Formation. 92 grains out of 131 gave concordant results (Fig. 12). We detected three age groups and two single plots of concordant detrital zircons: 116-237 Ma (74%), 1580-2036 Ma (16%), 254-301 Ma (8%), around 2209 Ma (1%), and around 2961 Ma (1%), with %Pc of 19 and the YZ of  $115.5 \pm 2.7$  Ma (Fig. 12a-c). The probability density plot for the 0-500 Ma data set showed the largest peaks at 173 Ma, 181 Ma, and 189 Ma, a second largest peak at 131 Ma, and small peaks at 124 Ma, 221 Ma, 235 Ma, and 259 Ma (Fig. 12d). The YP was at 124 Ma, and the concordant age of the two grains that constitute the 124 Ma peak was 124.3  $\pm 2.4$  Ma (MSWD = 0.67, Probability = 0.41).

# Sandstone of the middle part of the Yunoki Formation (Sample Yu-2)

We obtained 125 analyses from 125 zircon grains collected from sandstone sample Yu-2 of the middle part of the Yunoki Formation. 91 grains out of 125 gave concordant results (Fig. 13). We detected four age groups and one single plot of concordant detrital zircons: 107–318 Ma (65%), 379–466 Ma (20%), 1638–1852 Ma (12%), 2067–2198 Ma (2%), and around 2407 Ma (1%), with %Pc of 15 and the YZ of 107.3  $\pm$  3.1 Ma (Fig. 13a–c). The probability density plot for the 0–500 Ma data set showed

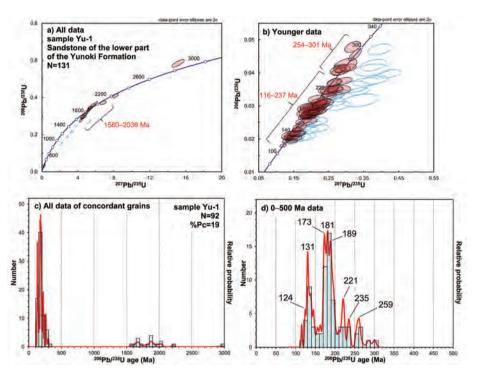


FIGURE 12. Analytical data of detrital zircons from sandstone of the lower part of the Yunoki Formation (sample Yu-1). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

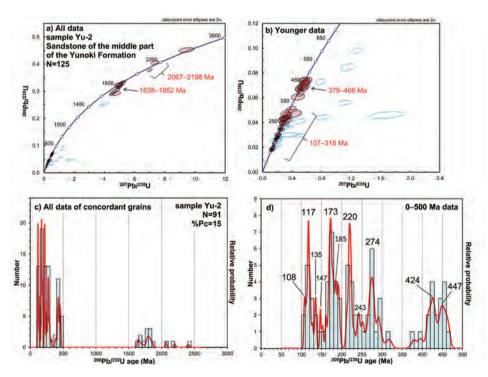


FIGURE 13. Analytical data of detrital zircons from sandstone of the middle part of the Yunoki Formation (sample Yu-2). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

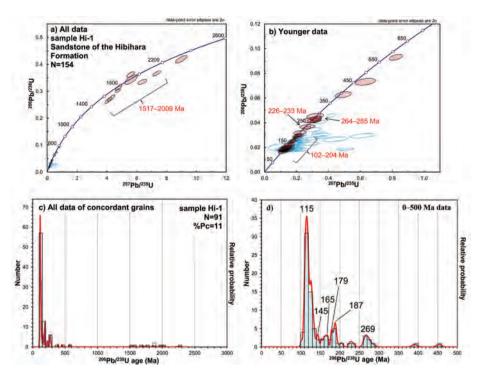


FIGURE 14. Analytical data of detrital zircons from sandstone of the Hibihara Formation (sample Hi-1). **a,** Concordia diagram for all data; **b,** Concordia diagram for a younger data set; **c,** Probability density plot with a histogram for all data of concordant grains; **d,** Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

the largest peaks at 117 Ma, 173 Ma, and 220 Ma, second largest peaks at 274 Ma and 185 Ma, and small peaks at 108 Ma, 135 Ma, 147 Ma, 191 Ma, 243 Ma, 274 Ma, 424 Ma, and 447 Ma (Fig. 13d). The YP was at 108 Ma, and the concordant age of the two grains that constitute the 108 Ma peak was  $108.2 \pm 2.4$  Ma (MSWD = 3.7, Probability = 0.053).

### Sandstone of the Hibihara Formation (Sample Hi-1)

We obtained 154 analyses from 154 zircon grains collected from sandstone sample Hi-1 of the Hibihara Formation. 91 grains out of 154 gave concordant results (Fig. 14). We detected four age groups and four single plots of concordant detrital zircons: 102-204 Ma (78%), 1517-2009 Ma (9%), 264-285 Ma (7%), 226-233 Ma (2%), 391 Ma (1%), 454 Ma (1%), 572 Ma (1%), and 2251 Ma (1%), with %Pc of 11 and the YZ of  $102.0 \pm 4.8$  Ma (Fig. 14a-c). The probability density plot for the 0-500 Ma data set showed the largest and youngest peak at 115 Ma, a second largest peak at 187 Ma, and small peaks at 145 Ma, 165 Ma, 179 Ma, and 269 Ma (Fig. 14d). The YP was at 115 Ma, and the concordant age of the thirty grains that constitute the 115 Ma peak was  $114.9 \pm 0.8$  Ma (MSWD = 5.9, Probability = 0.015).

#### Nankai Group

# Sandstone of the lower part of the Birafu Formation (Sample Bi-1)

We obtained 128 analyses from 128 zircon grains collected from sandstone sample Bi-1 of the lower part of the Birafu Formation. 82 grains out of 128 gave concordant results (Fig. 15). We detected six age groups of concordant detrital zircons: 1489-2181 Ma (44%), 150-221 Ma (35%), 241-270 Ma (11%), 292-320 Ma (4%), 2413-2625 Ma (4%), and 397-420 Ma (3%), with %Pc of 48 and the YZ of  $149.9 \pm 3.6$  Ma (Fig. 15a-c). The probability density plot for the 0-500 Ma data set showed the largest peak at 179 Ma, second largest peaks at 188 Ma and 197 Ma, and small peaks at 169 Ma (YP), 214 Ma, 221 Ma, 241 Ma, and 267 Ma (Fig. 15d).

# Sandstone of the middle part of the Birafu Formation (Sample Bi-2)

We obtained 126 analyses from 126 zircon grains collected from sandstone sample Bi-2 of the middle part of the Birafu Formation. 104 grains out of 126 gave concordant results (Fig. 16). We detected six age groups of concordant detrital zircons: 128–255 Ma (66%), 1509–1980 Ma (23%), 290–317 Ma (3%), 2110–2205 Ma (3%), 2535–2605 Ma (3%), and 2390–2409 Ma (2%), with %Pc of 31 and the YZ of 128.1  $\pm$  4.7 Ma (Fig. 16a–c). The probability density plot for the 0–500 Ma data set showed the largest peak at 172 Ma, the second largest and youngest peak at 136 Ma, and small peaks at 151 Ma, 221 Ma, and 242 Ma (Fig. 16d). The eight grains that constitute the YP gave the concordant age of 136.5  $\pm$  2.5 Ma (MSWD = 0.65, Probability = 0.42).

### Sandstone of the Funadani Formation (Sample Fu-1)

We obtained 123 analyses from 123 zircon grains collected from sandstone sample Fu-1 of the Funadani Formation. 98 grains out of 123 gave concordant results (Fig. 17). We detected four

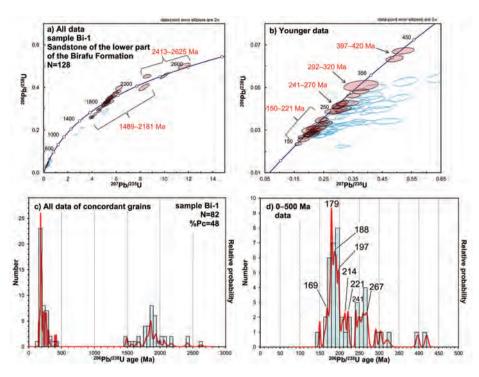


FIGURE 15. Analytical data of detrital zircons from sandstone of the lower part of the Birafu Formation (sample Bi-1). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with a histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

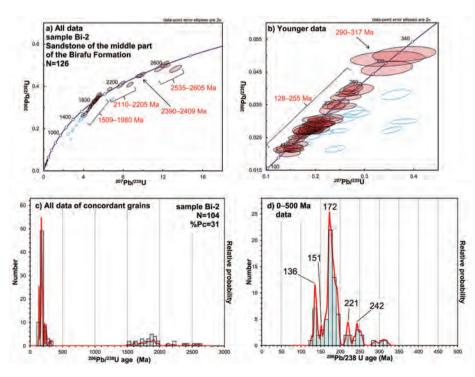


FIGURE 16. Analytical data of detrital zircons from sandstone of the middle part of the Birafu Formation (sample Bi-2). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with a histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

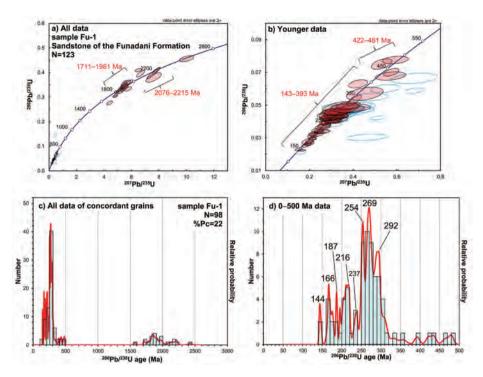


FIGURE 17. Analytical data of detrital zircons from sandstone of the Funadani Formation (sample Fu-1). **a,** Concordia diagram for all data; **b,** Concordia diagram for a younger data set; **c,** Probability density plot with a histogram for all data of concordant grains; **d,** Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

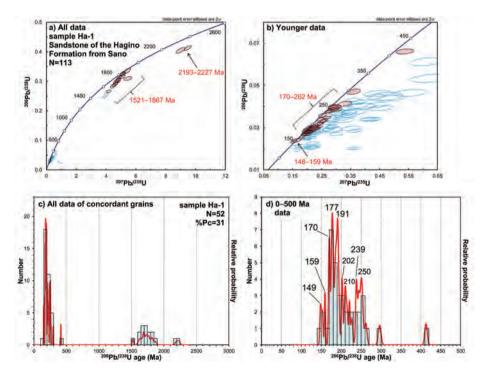


FIGURE 18. Analytical data of detrital zircons from sandstone of the Hagino Formation from Sano (sample Ha-1). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with a histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

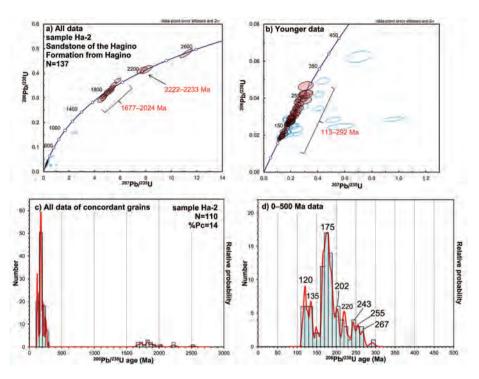


FIGURE 19. Analytical data of detrital zircons from sandstone of the Hagino Formation from Hagino (sample Ha-2). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with a histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

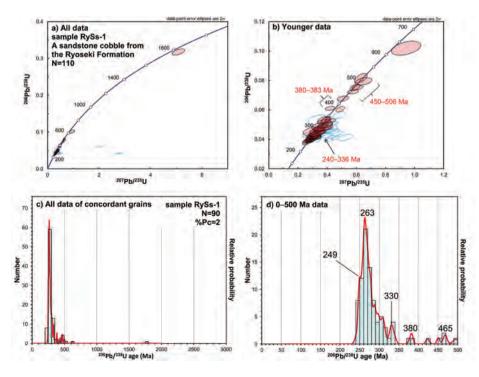


FIGURE 20. Analytical data of detrital zircons from a sandstone cobble from the Ryoseki Formation (sample RySs-1). **a,** Concordia diagram for all data; **b,** Concordia diagram for a younger data set; **c,** Probability density plot with a histogram for all data of concordant grains; **d,** Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

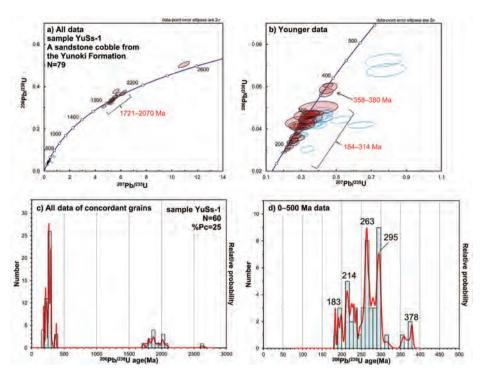


FIGURE 21. Analytical data of detrital zircons from a sandstone cobble of the Yunoki Formation (sample YuSs-1). **a,** Concordia diagram for all data; **b,** Concordia diagram for a younger data set; **c,** Probability density plot with a histogram for all data of concordant grains; **d,** Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

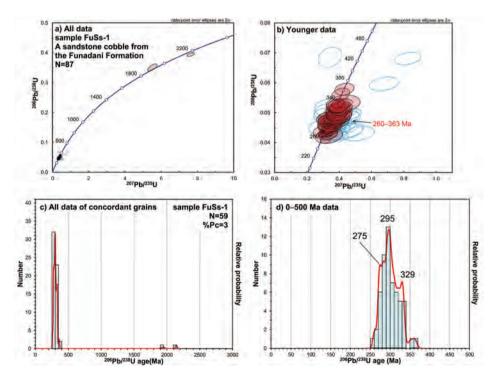


FIGURE 22. Analytical data of detrital zircons from a sandstone cobble of the Funadani Formation (sample FuSs-1). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with a histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

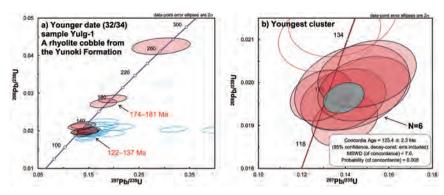


FIGURE 23. Analytical data of zircons from a rhyolite cobble of the Yunoki Formation (sample YuIg-1). a, Concordia diagram for a younger data set; b, Concordia diagram for the data set forming the youngest cluster (the light blue filled ellipse denotes the concordant age). N: total number.

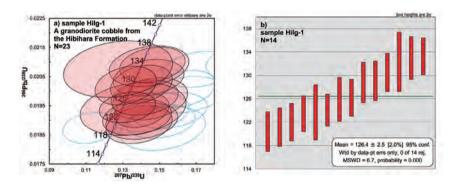


FIGURE 24. Analytical data of zircons from a granodiorite cobble of the Hibihara Formation (sample HiIg-1). **a**, Concordia diagram for all data (except for no.15 zircon of Table 1); **b**, <sup>206</sup>Pb/<sup>238</sup>U ages for the 14 concordant zircons with the calculated weighted mean age. N: total number.

age groups and two single plots of concordant detrital zircons: 143-393 Ma (73%), 1711-1981 Ma (15%), 2076-2215 Ma (5%), 422-481 Ma (4%), around 1570 Ma (1%), and around 2424 Ma (1%), with %Pc of 22 and the YZ of  $143.4 \pm 3.2$  Ma (Fig. 17a-c). The probability density plot for the 0-500 Ma data set showed the largest peak at 269 Ma, second largest peaks at 254 Ma and 292 Ma, and small peaks at 144 Ma (YP), 166 Ma, 187 Ma, 216 Ma, and 237 Ma (Fig. 17d).

# Sandstone of the Hagino Formation from Sano (Sample Ha-1)

We obtained 113 analyses from 113 zircon grains collected from sandstone sample Ha-1 of the Hagino Formation. 52 grains out of 113 gave concordant results (Fig. 18). We detected four age groups and two single plots of concordant detrital zircons: 170–262 Ma (60%), 1521–1867 Ma (26%), 148–159 Ma (6%), 2193–2227 Ma (4%), 297 Ma (2%), and 413 Ma (2%), with %Pc of 31 and the YZ of 148.1  $\pm$  3.5 Ma (Fig. 18a–c). The probability density plot for the 0–500 Ma data set showed the largest peaks at 177 Ma and 191 Ma, a second largest peak at 170 Ma, and small peaks at 149 Ma (YP), 159 Ma, 202 Ma, 210 Ma, 239 Ma, and 250 Ma (Fig. 18d).

# Sandstone of the Hagino Formation from Hagino (Sample Ha-2)

We obtained 137 analyses from 137 zircon grains collected from sandstone sample Hs-2 of the Hibihara Formation. 110 grains out of 137 gave concordant results (Fig. 19). We detected three age groups and one single plot of concordant detrital zircons: 113–292 Ma (86%), 1677–2024 Ma (11%), 2222–2233 Ma (2%), and around 2525 Ma (1%), with %Pc of 14 and the YZ of 112.9  $\pm$  3.9 Ma (Fig. 19a–c). The probability density plot for the 0–500 Ma data set showed the largest peak at 175 Ma, the second largest and youngest peak at 120 Ma, and small peaks at 135 Ma, 150 Ma, 202 Ma, 220 Ma, 243 Ma, 255 Ma, and 267 Ma (Fig. 19d). The ten grains that constitute the YP gave the concordant age of 119.3  $\pm$  1.8 Ma (MSWD = 0.051, Probability = 0.82).

### **Cobbles from conglomerate**

# A sandstone cobble from the Ryoseki Formation, Monobegawa Group (Sample RySs-1)

We obtained 110 analyses from 110 zircon grains collected from sandstone cobble sample RySs-1 of the Ryoseki Formation. 90 grains out of 110 gave concordant results (Fig. 20). We detected three age groups and three single plots of concordant detrital zircons: 240–336 Ma (89%), 450–506 Ma (6%), 380–383

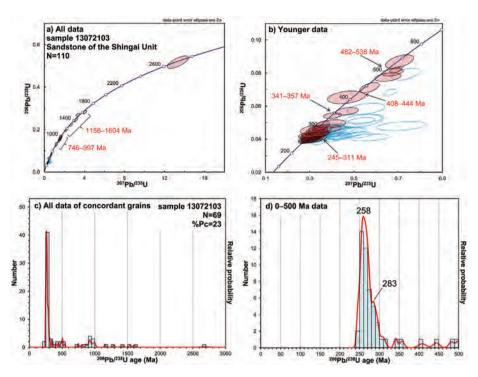


FIGURE 25. Analytical data of detrital zircons from sandstone of the Shingai Unit (sample 13072103). **a,** Concordia diagram for all data; **b,** Concordia diagram for a younger data set; **c,** Probability density plot with a histogram for all data of concordant grains; **d,** Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

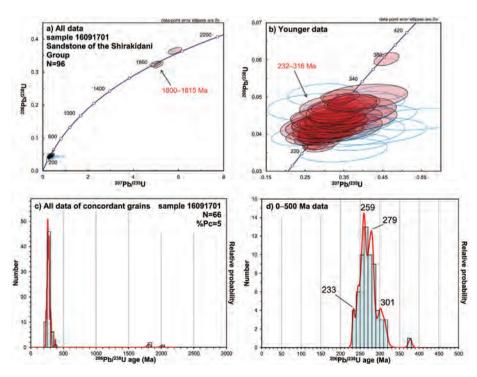


FIGURE 26. Analytical data of detrital zircons from sandstone of the Shirakidani Group (sample 16091701). **a**, Concordia diagram for all data; **b**, Concordia diagram for a younger data set; **c**, Probability density plot with a histogram for all data of concordant grains; **d**, Probability density plot with a histogram for the 0–500 Ma data set. N: total number, %Pc: percentage of Precambrian zircons.

Ma (2%), 423 Ma(1%), 626 Ma (1%), and 1779 Ma (1%), with %Pc of 2 and the YZ of  $240.2 \pm 7.7$  Ma (Fig. 20a-c). The probability density plot for the 0-500 Ma data set showed the largest peak at 263 Ma and small peaks at 330 Ma, 380 Ma, and 465 Ma (Fig. 20d).

# A sandstone cobble from the Yunoki Formation, Monobegawa Group (Sample YuSs-1)

We obtained 79 analyses from 79 zircon grains collected from sandstone cobble sample YuSs-1 of the middle part of the Yunoki Formation. 60 grains out of 79 gave concordant results (Fig. 21). We detected three age groups and one single plot of concordant detrital zircons: 184–314 Ma (70%), 1721–2070 Ma (23%), 358–380 Ma (5%), and 2633 Ma (2%), with %Pc of 25 and the YZ of 183.6  $\pm$  2.6 Ma (Fig. 21a–c). The probability density plot for the 0–500 Ma data set showed the largest peak at 263 Ma, a second largest peak at 295 Ma, and small peaks at 183 Ma (YP), 199 Ma, 214 Ma, 230 Ma, 281 Ma, and 378 Ma (Fig. 21d).

# A sandstone cobble from the Funadani Formation, Nankai Group (Sample FuSs-1)

We obtained 87 analyses from 87 zircon grains collected from sandstone cobble sample FuSs-1 of the Funadani Formation. 59 grains out of 87 gave concordant results (Fig. 22). We detected one age group and two single plots of concordant detrital zircons: 260-363 Ma (97%), 1940 Ma (2%), and 2143 Ma (2%) with %Pc of 3 and the YZ of  $259.7 \pm 7.2$  Ma (Fig. 22a-c). The probability density plot for the 0-500 Ma data set showed the largest peak at 295 Ma and second largest peaks at 275 Ma (YP) and 329 Ma (Fig. 22d).

# A rhyolite cobble from the Yunoki Formation, Monobegawa Group (Sample YuIg-1)

We obtained 34 analyses from 34 zircon grains collected from rhyolite cobble sample YuIg-1 of the middle part of the Yunoki Formation. 12 grains out of 34 gave concordant results (Fig. 23). We detected two age groups and two single plots of concordant zircons: 122–137 Ma (8 grains), 174–181 Ma (2 grains), 269 Ma (1 grain), and 2334 Ma (1 grain) (Fig. 23a). The concordia age of the youngest 6 grains was 125.4  $\pm$  2.3 Ma (MSWD = 7.0, Probability = 0.008), which we interpreted as the formation age of the rhyolite (Fig. 23b).

### A granodiorite cobble from the Hibihara Formation, Monobegawa Group (Sample HiIg-1)

We obtained 24 analyses from 24 zircon grains collected from granodiorite cobble sample HiIg-1 of the Hibihara Formation. 14 grains out of 24 gave concordant results, which form a single age group at 120–133 Ma (Fig. 24a). The weighted mean of the 206Pb/238U ages of 14 grains was  $126.4 \pm 2.5$  Ma (MSWD = 6.7, Probability = 0.0), which we interpreted as the formation age of the granodiorite (Fig. 24b).

### Pre-Cretaceous sandstone of the Northern Chichibu Belt

### Sandstone of the Shingai Unit (Sample 13072103)

We obtained 110 analyses from 110 zircon grains collected from sandstone sample 13072103 of the Shingai Unit. 69 grains out of 110 gave concordant results (Fig. 25). We detected six age groups and one single plot of concordant detrital zircons: 245–311 Ma (65%), 746–997 Ma (15%), , 1156–1604 Ma (7%), 482–538 Ma (6%), 341–357 Ma (3%), 408–444 Ma (3%), and 2690 Ma (1%), with %Pc of 23 and the YZ of 245.2  $\pm$  7.0 Ma(Fig. 25a–c). The probability density plot for the 0–500 Ma data set showed a single peak at 258 Ma (Fig. 25d).

### Sandstone of the Shirakidani Group (Sample 16091701)

We obtained 96 analyses from 96 zircon grains collected from sandstone sample 16091701 of the Shirakidani Group. 66 grains out of 96 gave concordant results (Fig. 26). We detected two age groups and two single plots of concordant detrital zircons: 232–316 Ma (94%), 1800–1815 Ma (3%), 377 Ma (2%), and 2007 Ma (2%), with %Pc of 5 and the YZ of 232.2  $\pm$  7.5 Ma (Fig. 26a–c). The probability density plot for the 0–500 Ma data set showed the largest peak at 259 Ma, second largest peak at 279 Ma, and small peaks 233 Ma (YP) and 301 Ma (Fig. 26d).

#### DISCUSSION

# Age of deposition of the Lower Cretaceous formations in the study area

The mineral zircon is crystallized from acidic to intermediate magma (e.g., Hoskin and Schaltegger, 2003) and memorizes the age of formation of the felsic to intermediate-igneous-rock body from the magma. Due to the erosion of the igneous-rock body, the zircon grains in the rock body are transported to a sedimentary basin, together with reworked older zircons from sedimentary and/or metamorphic rock bodies. Okawa et al. (2013) concluded, from their study of detrital zircon ages from 14 sandstone samples of the South Kitakami Belt, that the YP of a sandstone sample on the probability density plot is a good measure for the upper age limit of the deposition of the sample. Following Okawa et al. (2013), we assume that the YP age or the concordia age of the YPforming zircons (if calculated) of a sample is the upper limit of the age of deposition. In this study, we found that the upper age limit of the Yunoki and Birafu formations inferred from detrital zircon ages is significantly younger than the age of deposition inferred from fossils. In the following discussion, we will revise the age of deposition of the two formations.

### **Yunoki Formation**

The Yunoki Formation has been correlated with the upper Barremian from a Neocomian type ammonite, *Paracrioceras* (?) sp. from the upper part of the formation (Tanaka et al., 1984; Fig. 4). The overlying Hibihara Formation, on the other hand, was correlated with the Aptian–Albian from ammonites. The lower Middle Member of the Hibihara Formation yields *Cheloniceras* (C.) sp. and is correlated with the lower Aptian; the upper Middle Member yields *Eodouvilleiceras* sp. and *Nolaniceras* (?) sp. and is correlated with the upper Aptian; and the Uppermost Member yields *Hysteroceras* aff. *H. carinatum*, *Engonoceras* aff. *E. stolleyi*, *Tetragonites* cf. *T. timotheanus*, *Idiohamites* sp., and *Pseudhelioceras* sp. and is correlated with the Albian (Tanaka et al., 1984; Fig. 4). In this study, we found that the concordia age of the two zircon grains forming the YP of sample Yu-1

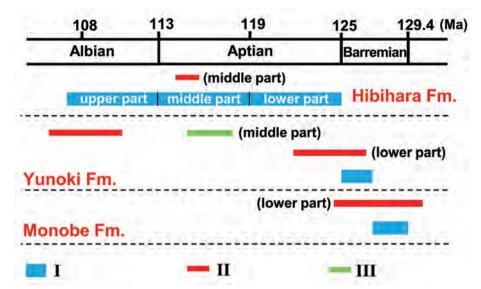


FIGURE 27. A diagram comparing the age constraints from fossils and zircons of the Monobegawa Group. Keys I: The age-range of index fossils, II: The age-range of zircons (with  $2\sigma$  errors) forming the YP of each sample of the Monobegawa Group, III: The age-range of zircons (with  $2\sigma$  errors) forming the second YP in sample Yu-2, Fm.: Formation, YP: youngest peak in the probability density plot.

from the lower part of the Yunoki Formation was  $124.3 \pm 2.4$  Ma. For sample Yu-2 from the middle part, the concordia age of the two zircon grains forming the YP was  $108.2 \pm 2.4$  Ma, and the concordia age of the five zircon grains forming the second youngest peak was  $116.4 \pm 1.5$  Ma (MSWD = 0.7, Probabilility = 0.4). Moreover, the age of the rhyolite cobble from the middle part of the Yunoki Formation (sample YuIg-1) was  $125.4 \pm 2.3$  Ma. According to International Commission for Stratigraphy (ICS) (2016), these age data strongly suggest that the Yunoki Formation is correlated with the Aptian (-Albian) (Fig. 27). The reason for the discrepancy between the fossil and zircon ages is still unknown. We have to wait for the definition of the base Aptian GSSP and its numerical age assignment, and the reexamination of the first appearance and last appearance biohorizons of the ammonite fossils from the Yunoki and Hibihara formations.

#### **Birafu Formation**

There were two interpretations on the correlation of the Birafu Formation, which was subdivided into A1-3, B1-2, and C members, in ascending order (Kozai et al., 2004, 2006). Morino et al. (1989) found radiolarian fossils from two locations including the B members along the Nishinokawa River and correlated the formation with the upper Valanginian-Barremian. Kozai et al. (2004, 2006), on the other hand, studied the radiolarian and bivalve fossils from the formation and correlated the it with the Oxfordian-lower Valanginian, suggesting that the Jurassic-Cretaceous boundary lies between the A3 and B1 members. We found that sample Bi-1 from the A2 Member had the YZ and YP of 149.9  $\pm$  3.6 Ma and 169 Ma, respectively, and did not contain Early Cretaceous zircons. Since a tuff layer just above Bi-1 yields Oxfordian radiolarians such as Kilinora spiralis (Kozai et al., 2006), we propose that sample Bi-1 is Oxfordian or younger in age, and our data do not contradict with the interpretation of Kozai et al. (2004, 2006) that the A members are correlated with the Upper Jurassic. We also found that sample Bi-2 from the B members had the YZ and YP of  $128.1 \pm 4.7$  Ma and 136 Ma, respectively, and 9 zircon grains out of 104 were of the Early Cretaceous. Since the concordia age of the 8 grains forming the YP was  $136.5 \pm 2.5$  Ma, the age of deposition of sample Bi-2 must have been 139 Ma (Early Valanginian; ICS, 2016) or younger. Considering the fact that the C Member of the Birafu Formation, overlying the B members, consists of more than 200 m thick fine-grained rocks such as mudstone and interbedded fine sandstone and mudstone, we suppose that the age of the Birafu Formation ranges from the Oxfordian (Fig. 20) to the Late Valanginian or even the Hauterivian.

### Provenance change of the Monobegawa and Nankai groups

### Monobegawa Group

The detrital-zircon-age spectra of the Monobegawa Group are summarized as follows. The detrital zircons of the Ryoseki Formation (sample Ry-1) consisted mostly of Permian (51%) and Triassic (38%) zircons (Table. 1; Figs. 28 and 29), and the probability density plot showed a prominent peak at 252 Ma. On the other hand, the Monobe and Yunoki formations (samples Mo-1 and Yu-1) contained abundant Mesozoic zircons: i.e., Triassic, Jurassic, and Early Cretaceous zircons, whereas the uppermost Hibihara Formation (sample Hi-1) contained 60% of Early Cretaceous zircons (Figs. 28 and 29). Previous petrographical study of clastic rocks of the Monobegawa Group indicated that the clastic grains of the Ryoseki Formation were mainly derived from older sedimentary rocks, whereas the contribution of felsic to intermediate (the former in particular) igneous-rock fragments gradually increased upwards from the Monobe to Hibihara

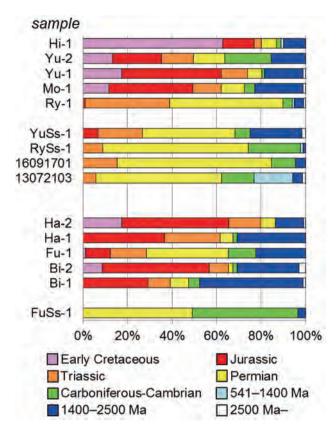


FIGURE 28. Bar graphs showing the age composition of detrital zircons from sandstone samples including the samples of sandstone cobbles.

formations (Miyamoto and Nakai, 1974; Miyamoto, 1980). We will discuss the provenance of detrital zircons in the Monobegawa Group from these data and previous studies.

The predominant Permian and Triassic zircons in the Ryoseki Formation strongly indicate the rework of detrital zircons from the pre-Cretaceous AC of the Northern Chichibu Belt, for four reasons. (1) Previous studies suggested that the clastic grains of the Ryoseki Formation were mainly supplied from the pre-Cretaceous sedimentary rocks of the Northern Chichibu Belt (Miyamoto and Nakai, 1974; Miyamoto, 1980). (2) The sandstone cobbles in the Ryoseki and Yunoki Formations (samples RySs-1 and YuSs-1) contain many Permian and Triassic zircons. (3) In particular, the detrital-zircon-age spectra of the sandstone cobble (sample RySs-1) and sandstone (sample Ry-1) of the Ryoseki Formation are very similar. (4) The detrital-zircon-age spectra of the sandstone of the Shingai Unit (sample 13072103), the Shirakidani Group (sample 16091701) and the Ryoseki Formation (sample Ry-1) are also very similar (Figs. 28 and 29).

On the other hand, our data and previous studies imply that igneous activity gradually became active in the hinterland during the deposition of the Monobe, Yunoki, and Hibihara formations. The reasons are as follows. (1) The proportion of Early Cretaceous zircons, which were absent in the Ryoseki Formation, gradually increases upwards (Fig. 28). (2) The proportion of feldspar and

rock fragments in sandstone and of felsic-igneous-rock clasts in conglomerate gradually increases upwards (Figs. 5–7). (3) The age of igneous rock cobbles in the Monobegawa Group (samples YuIg-1 and HiIg-1) is approximately 125 Ma.

Thus the provenance of the Monobegawa Group in the Ryoseki–Monobe area changed from the pre-Cretaceous rocks of the Northern Chichibu Belt (Ryoseki period) to an Early Cretaceous igneous province and pre-Cretaceous rocks of the Northern Chichibu Belt (Monobe–Hibihara period). A similar provenance change has been proposed in the Lower Cretaceous Sanchu Group in the Kanto Mountains from the petrography of clastic rocks (Takei, 1980) and the temporal change of the detrital-zircon-age spectra (Nakahata et al., 2016).

#### Nankai Group

The detrital-zircon-age spectra of the Nankai Group are summarized as follows. The Funadani Formation (sample Fu-1) was characterized by the abundance of Permian (37%) zircons, whereas the Birafu and Hagino formations (samples Bi-1, Bi-2, Ha-1, and Ha-2) were characterized by the abundance of Jurassic (28–48%) zircons (Figs. 28 and 29). Among them, the Permian zircons in the Funadani Formation were likely derived from older sedimentary rocks from the following reasons. (1) The conglomerate of the Funadani Formation mostly contains sedimentary-rock clasts, and (2) the sandstone cobble of the Funadani Formation (sample FuSs-1) was rich in Permian zircons (Figs. 28 and 29).

#### Origin of Triassic and Jurassic zircons

It is a little hard to judge if the Triassic and Jurassic zircons in the two groups have been derived from older sedimentary rocks or older igneous rocks. However, we propose that Jurassic igneous rocks were widespread in the hinterland of the Birafu Formation, because the sandstone of the Birafu Formation (samples Bi-1 and Bi-2), containing many Jurassic zircons, is feldspathic arenite derived from felsic plutonic rocks. Further, the Aptian Kurohara Formation (Kozai and Ishida, 2006) in the Sakawa area, some 50 km to the west of the study area, contains a 227 Ma granite cobble (Ikeda et al., 2016), suggesting that Triassic igneous rocks were also exposed in the hinterland of the Lower Cretaceous beds of the study area.

# Paleogeography of the Lower Cretaceous formations of the Ryoseki–Monobe area

#### **Sediment supply from South China**

We inferred that Early Cretaceous igneous rocks were exposed in the hinterland of most of the Lower Cretaceous formations in the study area from the detrital-zircon-age spectra. Along the present continental margin of East Asia, Early Cretaceous rock bodies that can supply enough detrital zircons occur most widely along the eastern margin of South China (145–90 Ma: e.g., Li et al., 2014; Wang et al., 2013). Smaller Early Cretaceous igneous rock bodies also occur in the Kitakami (130–110 Ma: Tsuchiya et al., 2015) and Abukuma (120–85 Ma: e.g., Kawano and Ueda, 1965; Shibata and Uchiumi, 1983; Ishihara and Orihashi, 2015; Kon et al., 2015) belts of Northeast Japan, in the Higo Belt of

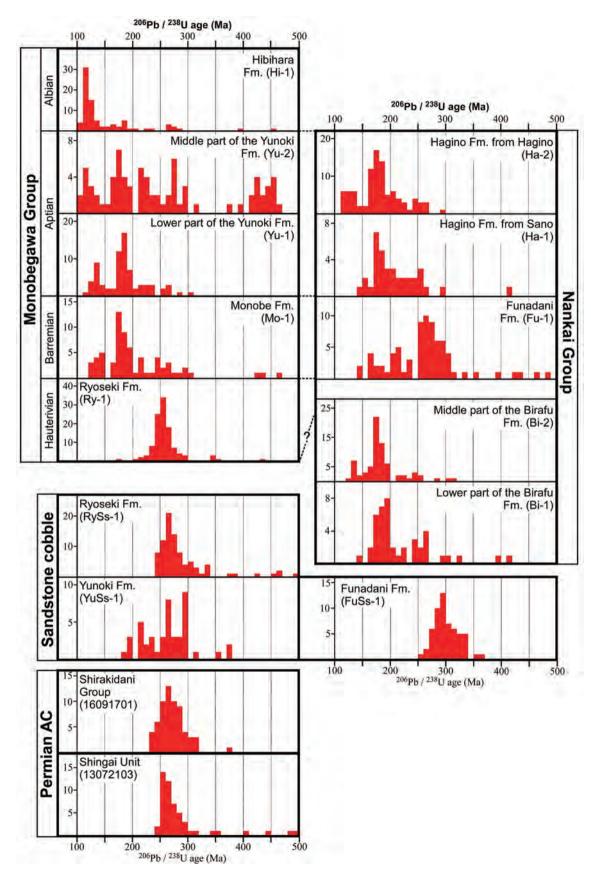


FIGURE 29. Histograms showing the detrital-zircon-age distribution of sandstone samples including the samples of sandstone cobbles. Fm: Formation.

Kyushu, Southwest Japan (120–110 Ma: e.g., Sakashima et al., 2003), and around the Bohai and West Korea bays, Northeast China (135–110 Ma: e.g., Kiminami and Imaoka, 2013; Wang et al., 2012; Wu et al., 2007). Among these areas, we propose that the Early Cretaceous zircons in the Lower Cretaceous formations of the study area were supplied from the Zhejiang–Fujian coast of South China, for three reasons.

- (1) The detrital-zircon-age spectra of the Monobegawa and Nankai groups do not show the influence of the magmatic hiatus in Korea, which is supposed to have been 158–110 Ma (Sagong et al., 2005). The distribution of 145–100 Ma felsic-igneous rocks is limited along the eastern margin of South China among the above areas.
- (2) Possible provenances of the 125 Ma felsic-igneous-rock clast (cobble) are along the east coast of South China, Kitakami Belt, and around the Bohai and West Korea bays, where felsic-igneous-rocks of approximately 125 Ma are widely exposed (Fig. 30). Considering the size and abundance of igneous rock clasts, it is hard to imagine that they were transported from rock bodies far from the coast. In this sense we exclude the 125 Ma felsic-igneous-rock-bodies around the Bohai and West Korea bays from the candidates of the provenance.
- (3) The Ryoseki Formation of the Monobegawa Group yields many elements of the Ryoseki-type flora, which occurs in South China (Zhejiang Province and to the south), Indochina, and the Malay Peninsula in continental Asia (Kimura, 1987). The distribution of the flora is concordant with our idea that the Monobegawa Group was deposited along the eastern coast of South China.

The Monobegawa and Nankai groups also contain many Triassic and Jurassic zircons, and at least parts of them are igneous origin as discussed above. However, the Triassic–Jurassic zircons were not enough useful to detect the provenance, because Triassic–Jurassic (> 158 Ma) igneous rocks widely occur in East Asia. Nevertheless, the presence of Triassic–Jurassic zircons does not contradict with our idea; Triassic–Jurassic igneous rocks, including those formed during the magmatic hiatus of Korea, are widely distributed in the eastern part of the Zhejiang–Fujian provinces of South China.

Sandstone from the middle part of the Yunoki Formation (sample Yu-2) of the Monobegawa Group (Northern Chichibu Belt) contains a certain amount of 460-400 Ma zircons (18%). In Japan, 460-400 Ma felsic-igneous-rock bodies occur in (1) the South Kitakami Belt, Northeast Japan (e.g., Shimojo et al., 2010), (2) the Yakuno Complex, Inner Zone of Southwest Japan, and (3) the Kurosegawa Belt, Outer Zone of Southwest Japan (Mitaki igneous rocks; e.g., Hada et al., 2000), but the present areas of their distribution are very narrow. Although we cannot completely deny the possibility that the 460-400 Ma zircons in sample Yu-2 were supplied from the 460-400 Ma rock bodies in present-day Japan, the age composition of igneous rocks in South China (Fig. 30) and the presence of the Ryoseki-type flora in the Monobegawa Group strongly indicates that the 460-400 Ma Kwangsian Granite in South China (e.g., Wang et al., 2013) was most likely the provenance of the 460-400 Ma zircons.

#### **Evaluation of sinistral strike-slip models**

In the previous section, we concluded that the provenance of Early Cretaceous zircons in the Monobegawa and Nankai groups and 460-400 Ma zircons in the Yunoki Formation was Early Cretaceous and 460-400 Ma igneous rock bodies in the Zhejiang-Fujian province of South China. The distance from the Ryoseki-Monobe area and the Zhejiang-Fujian province is roughly 1,500 km. It is also possible that the basement of the Yellow Sea Basin consists partly of Early Cretaceous igneous rocks that cropped out on the land surface in the Early Cretaceous and supplied Early Cretaceous zircons to the Monobegawa Group and/or Nankai Group. Even in this case, the distance between the Ryoseki-Monobe area and the mouth of the Yellow Sea is about 500 km. Hence we interpret that the Monobegawa and Nankai groups have moved at least 500-1,500 km northeastward (Fig. 30). We further interpret that the sinistral strike-slip motion along the Median Tectonic Line (Miyata and Iwamoto, 1994; Yamakita and Otoh, 2000a, b) was responsible for at least a part of the above displacement.

It is still hard to verify, only with our zircon data, the strikeslip model of Tashiro (1985), which described that the arcsubparallel sinistral strike-slip motion between the Monobegawa and Nankai groups had carried the Nankai Group relatively northward by the Albian. There are significant differences in the detrital-zircon-age spectra between the coeval samples of the Monobegawa and Nankai groups, but we cannot so precisely specify the site of deposition of each sample as to evaluate the strike-slip model of Tashiro (1985). For example, samples Ry-1 (Ryoseki Formation, Monobegawa Group) and Bi-2 (middle part of the Birafu Formation, Nankai Group) can be contemporaneous, but the differences in the positions of the largest peak (Ry-1 at 252 Ma and Bi-2 at 172 Ma; Figs. 10d and 16d) and in %Pc value (6 for Ry-1 and 31 for Bi-2; Figs. 10c and 16c) suggest different provenances. Sample Fu-1 (Funadani Formation, Nankai Group) can also be coeval with sample Ry-1, but the position of the largest peak (269 Ma; Fig. 17d) and %Pc value (22; Fig. 17c) differ from those of sample Ry-1. Sample Mo-1 (Monobe Formation, Monobegawa Group) in turn can be coeval with sample Fu-1, but the position of the largest peak (174 Ma; Fig. 11d) differs from that of sample Fu-1. Moreovre, the following differences in sandstone and conglomerate petrography also indicate the different provenances between the Monobegawa and Nankai groups. (1) The sandstone of the Monobegawa Group is primarily ill-sorted wacke, whereas that of the Nankai Group is mainly well-sorted arenite (Tashiro, 1985). (2) The conglomerate of the Shobu Formation of the Nankai Group in the Katsuura area characteristically contains felsic-igneous-rock clasts, whereas the coeval conglomerate of the Tatsukawa Formation of the Monobegawa Group is characterized by sedimentary-rock clasts (Matsukawa and Eto, 1987). In contrast, the detrital-zircon-age spectra of the following two Aptian samples are similar with each other: sample Yu-1 from the lower part of the Yunoki Formation and sample Ha-2 from the Hagino Formation from Hagino (Fig. 31). The similarity indicates the common provenance of the Monobegawa and Nankai groups in the Aptian. Even if the strike-

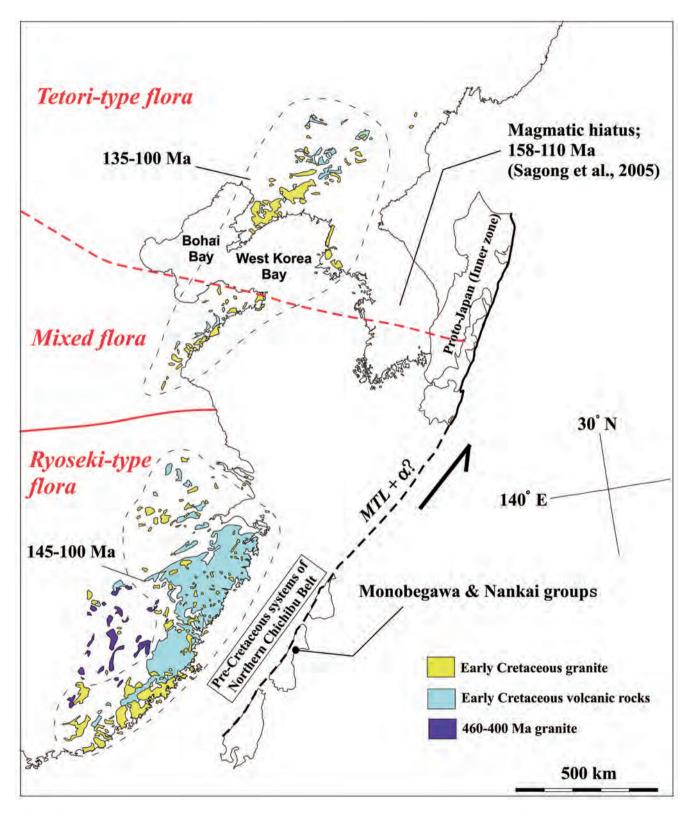


FIGURE 30. A paleogeographic map showing the possible reconstruction model for the sedimentary basins of the Lower Cretaceous formations in the Ryoseki–Monobe area, Outer Zone of Southwest Japan.

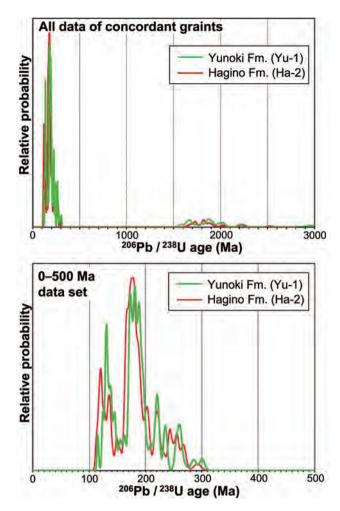


FIGURE 31. Probability density plots showing the similarity of detrital-zircon-age distribution between sample Yu-1 (lower part of the Yunoki Formation) and Ha-2 (Hagino Formation from Hagino).

slip model of Tashiro (1985) is close to the reality, the movement may have ceased by the end of Aptian.

### Evaluation of the Paleo-Ryoke model

Many previous studies implied that a geologic entity called the Paleo-Ryoke Belt, consisting of Permian and Early Cretaceous granite and metamorphic rocks, was once exposed between the Ryoke and Sambagawa belts but have mostly been eroded away (Ichikawa, 1964; Takagi and Shibata, 2000; Miyamoto et al., 2000). Miyamoto (1980) attributed the origin of igneous-rock clasts in the Monobegawa Group of the study area to the missing geologic entity along the southern margin of the Ryoke Belt. As we discussed above, however, we concluded that the igneous-rock clasts in the Monobegawa Group were supplied from igneous-rock bodies in the Zhejiang–Fujian provinces of South China from the botanical paleogeography (Kimura, 1987) and the sinistral strikeslip motion along the Median Tectonic Line separating the Ryoke and Sanbagawa belts (e.g., Miyata and Iwamoto, 1994; Yamakita and Otoh, 2000a, b). Moreover, (1) the presence of Permian

igneous and metamorphic rocks along the southern margin of the Jurassic AC of the Ryoke Belt and (2) the short distance between the Lower Cretaceous AC (i.e., Early Cretaceous subduction zone) of the Shimanto Belt and the Ryoke Belt (ca. 60 km) have not been explained in the Paleo-Ryoke model in a plate-tectonic framework.

Aoki et al. (2014) proposed that there was a topographic barrier that obstructed the southward transport of continent-derived sediments in the Early Cretaceous, because the Ryoseki Formation of the Hauterivian forearc basin contained very few continentderived Proterozoic zircons that dominated in the brackish to shallow-marine Toyonishi Group (Inner Zone of Southwest Japan) of the latest Jurassic to earliest Cretaceous back-arc basin. Aoki et al. (2014) concluded that the barrier was the Early Cretaceous igneous arc developed in the older orogen and was thrusted southward for more than 200 km along the Median Tectonic Line during the opening of the Sea of Japan in the Middle Miocene. However, we detected more than 20% Proterozoic zircons from the Monobe (Barremian; 22%), lower Birafu (latest Jurassic; 46%), middle Birafu (early Early Cretaceous; 28%), and Funadani (Hauterivian-Barremian; 22%) formations. Moreover, the Monobegawa and Nankai groups contained many Triassic to Jurassic zircons, in spite of the fact that there are virtually no Triassic to Jurassic igneous rocks to the south of the distribution of the Toyonishi Group. Thus, our data are not concordant with the barrier model of Aoki et al. (2014). We tentatively think that the amount of Proterozoic detrital zircons depends on the area of exposure of Proterozoic igneous rocks in the hinterland and the distance between the Proterozoic igneous rock bodies and the sedimentary basin. In addition, we doubt the Miocene southward thrust model, because the distance between the Paleogene volcanic front (the southern boundary of the San-in granite belt) and trench (Southern Shimanto Belt) was 300 km, close to the arc-trench gap in the present-day Northeast Japan, and we expect no arc-orthogonal shortening in the Miocene.

# Importance of reworked zircons in the study of detrital-zircon-age spectra

Nakahata et al. (2016) conducted a similar study with ours of the Sanchu Cretaceous in the Kanto Mountains, north of Tokyo. They concluded that Permo-Triassic igneous rock bodies were widely exposed in the hinterland of the Hauterivian Shiroi Formation, because Permo-Triassic zircons occupied 76% of the detrital zircons in the formation. They further suggested that clastic materials from Permo-Triassic igneous rock bodies were widely supplied to the Hauterivian forearc of Kanto and Shikoku, because the detrital-zircon-age spectra of the Shiroi and Ryoseki formations are very similar, and the Ryoseki Formation contains many 300-200 Ma zircons (Aoki et al., 2012). However, the distribution of Permian igneous rocks near Japan is limited to Northeast China and Indochina, although there are few Permian igneous rock bodies in the Maizuru Belt in Southwest Japan (e.g., Herzig et al., 1997). This study implied that the detrital zircons of the Ryoseki Formation were mainly derived from the Permian clastic rocks of the Northern Chichibu Belt. The sandstone of the Sanchu Cretaceous is lithic with many sedimentary-rock fragments

in the lower part and felspathic in the upper part, suggesting the change from a sedimentary-rock-rich hinterland to a graniterich hinterland (Takei, 1980). Moreover the conglomerate of the Hauterivian Tatsukawa Formation of the Monobegawa Group in the Katsuura area consists mostly of older-sedimentary-rock clasts (Ishida and Hashimoto, 1997; Matsukawa and Eto, 1987; Ogawa, 1971). Hence we propose that the Hauterivian formations of the Outer Zone of Southwest Japan from Kanto to Shikoku had a hinterland widely occupied by older sedimentary rock bodies and received detrital zircons from them. We further propose that it is misleading to think that the detrital zircons were all derived from igneous-rock bodies in the hinterland. To make a proper provenance analysis using detrital zircons, we have to make a comprehensive study including (1) the modal composition of the sandstone for detrital zircon study and (2) the detrital-zircon-age spectra of the basement sedimentary rocks and sandstone clasts in the conglomerate. Although the proportion of abraded zircons might be a criterion for the recognition of reworked zircons, the criterion cannot be applied to our present study. The proportion of abraded zircons in the sandstone of the Ryoseki Formation (Ry-1), the sandstone clast in the Ryoseki Formation (RySs-1), and the 300-230 Ma zircons in the sandstone of the Shirakidani Group (16091701) were 57, 54, and 50%, respectively, and did not show a significant difference. The result may reflect a short distance of transportation of the reworked zircons.

#### CONCLUSIONS

We studied detrital-U-Pb-zircon-age spectra of the sandstone sample from every formation of the Lower Cretaceous Monobegawa and Nankai groups (part of the Nankai Group is Upper Jurassic) of the Chichibu Composite Belt in the Ryoseki–Monobe area, Southwest Japan. In addition, we measured the U-Pb zircon age of (1) igneous rock cobbles in these formations and detrital-zircon-age spectra of (2) the sandstone cobbles from these formations and (3) the basement Permian sandstone of the Northern Chichibu Belt. The major results are summarized as follows.

- 1. The detrital-zircon-age spectra of the sandstone and sandstone cobble of the Ryoseki Formation and the Permian sandstone of the Northern Chichibu Belt are very similar. Combining the data with previous studies, we conclude that the clastic materials of the Ryoseki Formation were supplied from the pre-Cretaceous sedimentary rocks of the Northern Chichibu Belt.
- 2. Early Cretaceous zircons were absent in the Ryoseki Formation, but suddenly increased in the Monobe–Hibihara formations. Moreover, the U-Pb zircon age of the igneous rock cobbles from the Yunoki and Hibihara formations was approximately 125 Ma. Combining with the previous petrographical studies of sandstone and conglomerate, we conclude that an acidic to intermediate igneous activity took place in the hinterland concurrently with the deposition of the Monobegawa Group.
- 3. The petrography of clastic rocks implies that felsic-igneous-

- rock-bodies were exposed in the hinterland of the Nankai Group. The detrital-zircon-age spectra of the group indicate that the igneous rock bodies contained Early Cretaceous ones.
- 4. The hinterland of the two groups must have been the Zhejiang–Fujian provinces of South China, because (1) the study of botanical paleogeography of Kimura (1987) indicated that the Ryoseki Formation and South China commonly yield the Ryoseki-type flora, (2) detrital zircons formed during the magmatic hiatus in Korea were included in both the Monobegawa and Nankai groups, and (3) 460–400 Ma detrital zircons from the middle part of the Yunoki Formation were most likely from the Kwangsian Granite of South China.
- 5. The Monobegawa and Nankai groups likely had different hinterland by the Aptian. The previous petrographical studies and the similarity of detrital-zircon-age spectra of the lower part of the Yunoki Formation (Monobegawa Group) and the Hagino Formation (Nankai Formation) indicate that the two groups had common hinterland in the Aptian.
- 6. The two groups were deposited with the Zhejiang-Fujian provinces as the hinterland. The two groups must have shifted relatively northward by 500-1,500 km along the Median Tectonic Line sinistral fault system.
- 7. Detrital zircons were not all supplied from igneous rock bodies in the hinterland, but can be provided from older sedimentary and metamorphic rocks as reworked zircons. To make a proper provenance analysis using detrital zircons, we have to make a comprehensive study including (1) the modal composition of the sandstone for detrital zircon study and (2) the detrital-zircon-age spectra of the basement sedimentary rocks and sandstone clasts in the conglomerate.

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\* : in Japanese with English abstract

\*\* : in Japanese

### < 地名・地層名 >

Abukuma Belt · · · · 阿武隈带
Birafu ····· 美良布
Birafu Formation · · · · 美良布層
Chichibu Composite Belt … 秩父累带
Funadani Formation · · · · · · · 船谷層
Hagino····· 萩野
Hagino Formation · · · · 萩野層
Haginogawa River ······ 萩野川
Hibihara Formation · · · · 日比原層
Hibiharagawa River ······ 日比原川
Higo Belt····· 肥後帯
Igenoki Formation 神母ノ木層
Kagamiimai····· 鏡今井
Kajisakogawa River ······· 楮佐古川
Kasanokawagawa River ····· <u>禁</u> ノ川川
Katsuura area 勝浦地域
Kitakami Belt ······ 北上带
Kochi City ······ 高知市
Kochi Prefecture · · · · · 高知県
Kubogawa River · · · · 久保川
Kurohara Formation · · · · · 果原層

Kurosegawa Belt······ 黒瀬川帯
Kyushu ····· 九州
Kanto Mountains · · · · · 関東山地
Meoto Pond 女夫池
Mitaki igneous rocks … 三滝火成岩類
Monobe Formation · · · · 物部層
Monobegawa Group · · · · 物部川層群
Monobegawa River ····· 物部川
Yokokurayama Group 横倉山層群
Nankai Group · · · · · · 南海層群
Nishinokawa River ····· 西の川
Northeast Japan · · · · 東北日本
Northern Chichibu Belt · · · 北部秩父带
Odochi ····· 大栃
Pre-Sotoizumi Group ··· 先外和泉層群
Ryoke Belt ····· 領家帯
Ryoseki Formation 領石層
Ryoseki-Monobe area
Sakawa area ····· 佐川地域
Sanbagawa Belt 三波川帯

Sano ····· 佐野
Sasagawa River ······ 笹川
Shikoku ····· 四国
Shimanto Belt ····· 四万十带
Shingai Unit 新改ユニット
Shirakidani Group 白木谷層群
Shobu Formation · · · · · 菖蒲層
Sotoizumi Group
Southern Chichibu Belt … 南部秩父带
Southwest Japan 西南日本
Suita Group ······ 杉田層群
Tachibana ······ 立花
Tatsukawa Formation · · · · · 立川層
Tokushima Prefecture · · · · · · 徳島県
Torinosu Group ······ 鳥巣層群
Torinosu-type Limestone
Tosayamada······ 土佐山田
Yakuno Complex ··· 夜久野複合岩類
Yukigamine Formation 雪ヶ峰層
Yunoki Formation 柚ノ木層

TABLE 1. U-Pb isotopic data for zircons analyzed in this study. All errors are 2o. % conc = 100·(207Pb/235U age)/(206Pb/238U age) is a measure of concordance between 206Pb/238U and 207Pb/235U ages. Analyses shown in italics are discordant and are not included in the probability density plots and histograms.

Th/U	0.84	0.48	0.34	0.83	0.15	7.02	1,02	0.55	0.27	0.40	0.42	0.95	09.0	0.43	0,49	0.30	0.45	0.62	0.77	0.52	0.52	0.55	0.59	98.0	0.20	0.86	0.71	09.0	19'0	0.64	1.07	0.48	0.53	0.32	0.51	0.34	0.75	0.55	0.47	1.11	0.62	0.58	0.73	0.10	U.I.e.
%conc	8.46	6.86	95.5	100.7	986	0.66	02.2	08.7	98.3	81.3	102.2	96.4	118.2	97.6	100.2	102 0	101.5	100.7	1.96	6'66	95.2	97.3	102.7	95.0	0.00	98.3	97.8	96.2	95.8	94.6	108.8	7.76	666	97.2	100.4	8.76	96.1	95.5	110.6	98.5	100.0	100.7	9.06	0 30	33.2
Pb/Uage (Ma)	$275 \pm 25$	$242 \pm 15$	$287 \pm 74$	$247 \pm 18$	942 ± 42	25/8 ± 101	39/ = 30	51 ± 787	253 ± 14	376 ± 30	249 ± 24	263 ± 20	245 ± 41	262 ± 15	262 ± 19	364 ± 41	262 ± 15	255 ± (3	264 ± 45	$291 \pm 29$	$257 \pm 16$	247 ± 25	248 ± 26	291 ± 36	475 ± 35	253 ± 19	288 ± 19	$268 \pm 28$	265 ± 33	258 ± 20	318 ± 48	250 ± 12	248 ± 16	259 ± 13	358 ± 59	$270 \pm 38$	248 ± 9	288 ± 20	188 + 73	259 ± 16	255 ± 32	256 ± 23	275 ± 30	11 1 11	11 + /67
(Ma)	260,7 ± 8.8	239.3 ± 7.3	$274.6 \pm 14.5$	248.5 ± 7.9	929.0 ± 27.5	2021, 1 200	340:0 = 12:0	2530 + 8.0	248.7 ± 7.7	305.5 ± 10.5	254.7 ± 9.0	253,3 ± 8.4	289.5 ± 12.2	256.1 ± 8.1	262.2 ± 8.5	250.3 ± 9.4	265.9 ± 7.7	256.7 ± 7.2	$255.7 \pm 11.0$	290.6 ± 9.8	244.3 ± 7.2	$240.5 \pm 8.2$	254.2 ± 8.6	276.5 ± 10.3	1024 E 0.4501	248.5 ± 10.5	281.4 ± 11.7	$257.4 \pm 11.6$	$254.0 \pm 12.1$	244.4 ± 10.4	1./1 = 2.046	243.9 ± 4.6	246,7 ± 5.3	252,0 ± 4.9	$359.1 \pm 13.4$	263.9 ± 8.7	238.1 ± 4.4	274,8 ± 6.3	2083 + 75	255.5 ± 7.4	254.8 ± 9.5	258,0 ± 8.3	$249.5 \pm 8.9$	444 0 1 4 4	234.8 ± 0.4
707Pb/235U	$0.311 \pm 0.028$	#1	$0.327 \pm 0.084$	$0.275 \pm 0.020$		0.470 ± 0.455	H -	0.320 ± 0.024	1 1	4	+	#1	+	H :	0.294 ± 0.021	# 4	1	-11	+	+	$0.288 \pm 0.018$	91	Ħ	$0.332 \pm 0.041$	0.507 ± 0.517	H H	1	+1	+	# :	0.308 ± 0.033	1 1	+1	$0.291 \pm 0.015$	+1	#	#	0.328 ± 0.023	H +	(H	#(	#	+1		0.2/3 ± 0.012
O. Ph/23%	$0.0413 \pm 0.0014$	$0.0378 \pm 0.0012$	$0.0435 \pm 0.0023$	$0.0393 \pm 0.0012$	0.1550 ± 0.0046	0.4856 ± 0.0143	0.004 ± 0.0019	0.0413 ± 0.0013	0.0393 ± 0.0012	0.0485 ± 0.0017	41		0.0459 ± 0.0019	0.0405 ± 0.0013	0.0415 ± 0.0014	0.0463 + 0.0018	4		0.0405 ± 0.0017	$0.0461 \pm 0.0016$			0.0402 ± 0.0014	0.0438 ± 0.0016	0.0000 ± 0.0120	0.0393 ± 0.0017	14	+	+1	#	0.0552 ± 0.0027	0.0386 ± 0.0007	41	-#	-44	46	41 .	0.0435 ± 0.0010	# +	1	- 91	$0.0408 \pm 0.0013$	+11	MINNEY : MANNEY	H
Grain	Ry-1-51	Ry-1-52	Ry-1-53	Ry-1-54	Ry-1-55	Ky-1-50	Ky-1-2/	Ky-1-58	Rv-1-60	Rv-1-61	Ry-1-62	Ry-1-63	Ry-1-64	Ry-1-65	Ky-1-66	Dv. 1.69	Rv-1-69	Ry-1-70	Ry-1-71	Ry-1-72	Ry-1-73	Ry-1-74	Ry-1-75	Ry-1-76	Dy 1 70	Rv-1-79	Ry-1-80	Ry-1-81	Ry-1-82	Ry-1-83	Ky-1-84	Rv-1-86	Ry-1-87	Ry-1-88	Ry-1-89	Ry-1-90	Ry-1-91	Ry-1-92	Re-1-93	Rv-1-95	Ry-1-96	Ry-1-97	Ry-1-98	Pari 1 200	KV-1-99
Th/U		0.34	0.22	89.0	0.35	10.0	0.47	0.70	0.44	0.81	0.50	69.0	0.38	0.60	0.80	0.70	0.59	1.15	0.43	0,33	0,40	0.45	0.42	0.47	0.19	0.57	0.46	96.0	89.0	0.36	0.37	0.74	0.59	0.58	0.54	0.64	0.76	0.55	0.50	090	69.0	0.44	0.24	200	0.50
%conc		0.66	102.7	105.5	9101	506	2000	103.5	101.5	104.4	88.9	97101	7.86	9.98	98.3	.00.2	100.8	94.4	6.7.6	6.96	8.48	92.8	97.6	8.66	C 10	93.6	106.2	96.2	102.1	94.8	0.00	105.0	96.2	8.46	7.66	101.9	102.0	95.4	07.0	97.3	0.66	79.4	94.5		4.00
(Ma)		289 ± 25	$233 \pm 28$	235 ± 19	255 ± 14	263 ± 19	203 # 32	240 ± 15	260 ± 37	222 ± 24	$213 \pm 25$	244 ± 30	253 ± 17	319 ± 43	218 ± 18	1867 ± 66	216 ± 23	284 ± 24	305 ± 28	262 ± 17	242 ± 16	271 ± 25	258 ± 22	248 ± 25	27. ± 24.	277 ± 74	263 ± 44	257 ± 15	259 ± 29	264 ± 20	240 ± 13	249 ± 23	272 ± 25	365 ± 28		282 ± 34	256 ± 32	255 ± 15	284 + 36	4	262 ± 29	$331 \pm 45$	289 ± 43	274 1 1745	239 ± 19
(Ma)		286.1 ± 7.3		#	259.0 ± 5.3		# >	240.1 ± 2.1	264.1 ± 9.0	+	+0	248.3 ± 7.7	249.8 ± 5.6	276.2 ± 9.7	214.3 ± 5.2	1946 d ± 3d d			298.4 ± 14.2	+	#	+	H :	247.6 ± 8,4		259.2 ± 14.6				250.6 ± 7.9	231.0 ± 6.9	260.9 ± 8.0	41	#	#	#	41	243.4 = 6.6	278.0 ± 10.8	1	259.3 ± 9.4	+	+1	20 2 200	H
207 Pb/235 U	ki Formation (Ry-1;	0.329 ± 0.029	$0.258 \pm 0.031$	$0.261 \pm 0.022$	0.285 ± 0.016	0.295 ± 0.022	0.290 = 0.030	0.20/ ± 0.016	0.292 ± 0.041	0.244 ± 0.027	0.233 ± 0.027	$0.272 \pm 0.034$	0.283 ± 0.019	0.369 ± 0.050	0.240 ± 0.020	5.250 ± 0.021	0.237 ± 0.025	0.323 ± 0.028	0,350 ± 0,032	$0.294 \pm 0.019$	$0.270 \pm 0.018$	0.306 ± 0.028	0.290 ± 0.024	0.277 ± 0.028	0.308 ± 0.027	0.314 ± 0.084	0.296 ± 0.049	$0.288 \pm 0.017$			0.273 ± 0.017		0.307 ± 0.028	0.432 ± 0.033	$0.287 \pm 0.048$	$0.320 \pm 0.039$	0.286 ± 0.036	0.286 ± 0.017	0323 + 0.041	0.284 ± 0.027	0.294 ± 0.032	$0.385 \pm 0.052$	0.330 ± 0.050	WALL TOWN	0.200 = 0.021
7852/9d <sub>900</sub>	Sandstone of the Ryoseki Formation (Ry-1; 33" 37"	$0.0454 \pm 0.0012$	$0.0378 \pm 0.0012$	$0.0392 \pm 0.0009$	0.0410 ± 0.0008	0.0400 ± 0.0009	0.0404 = 0.0013	0.03/9 = 0.0008	0.0418 ± 0.0014	$0.0366 \pm 0.0010$	0,0297 ± 0,0009	$0.0393 \pm 0.0012$	$0.0395 \pm 0.0009$	0.0438 ± 0.0015	0.0338 ± 0.0008	0.0301 = 0.0009	0.0344 ± 0.0017	$0.0425 \pm 0.0020$	$0.0474 \pm 0.0023$	$0.0401 \pm 0.0018$	$0.0363 \pm 0.0016$	$0.0398 \pm 0.0019$	0.0399 ± 0.0019	0.0392 ± 0.0013	0.0413 ± 0.0014	$0.0410 \pm 0.0023$	$0.0443 \pm 0.0019$	$0.0391 \pm 0.0012$	$0.0418 \pm 0.0015$	0.0396 ± 0.0012	0.0366 ± 0.0011	0.0413 ± 0.0013	$0.0414 \pm 0.0013$	$0.0551 \pm 0.0016$	$0.0405 \pm 0.0017$	$0.0455 \pm 0.0016$	$0.0413 \pm 0.0014$	0.0385 ± 0.0010		0.0390 ± 0.0013	$0.0410 \pm 0.0015$	0.0416 ± 0.0018	$0.0433 \pm 0.0018$	CANAN DATA	0.0399 ± 0.0013
Grain		Ry-1-1	Ry-1-2	Ry-1-3	Ry-1-4	Ry-1-5	Ry-1-0	Ky-1-/	Rv-1-9	Rv-1-10	Ry-1-11	Ry-1-12	Ry-1-13	Ry-1-14	Ky-1-15	Ry-1-10	Rv-1-18	Ry-1-19	Ry-1-20	Ry-1-21	Ry-1-22	Ry-1-23	Ry-1-24	Ry-1-25	Py-1-20	Rv-1-28	Ry-1-29	Ry-1-30	Ry-1-31	Ry-1-32	Ry-1-53	Rv-1-35	Ry-1-36	Ry-1-37	Ry-1-38	Ry-1-39	Ry-1-40	Ry-1-41	Rv-1-43	Rv-1-44	Ry-1-45	Ry-1-46	Ry-1-47	No. 1 40	KV-1-43

Grain	$\Omega_{8\epsilon Z}/9d_{VOL}$	U255/49T05	<sup>206</sup> Pb/ <sup>238</sup> U age (Ma)	207Pb/235U age (Ma)	%conc	Th/U	Grain	$\Omega_{852}/9d_{902}$	$\Omega_{SE7}/9d_{LOC}$	200/Pb/238U age (Ma)	<sup>207</sup> Pb/ <sup>225</sup> U age (Ma)	%conc	Th/U
Ry-1-102	$0.0435 \pm 0.0014$	0,330 ± 0,023	274.7 ± 9.0	289 ± 20	95.0	0.54	Mo-J-23	0.0444 ± 0.0013	0,406 ± 0.045	280.3 ± 8.3	346 ± 38	81.0	0.4
Ry-1-103	$0.0403 \pm 0.0014$	0.276 ± 0.026	$255.0 \pm 9.0$	248 ± 24	102,9	0.62	Mo-1-24	0.0290 ± 0.0008	#1	184.0 ± 5.2	226 ± 24	81.3	0.57
Ry-1-104	$0.0323 \pm 0.0011$	$0.214 \pm 0.018$	$204.8 \pm 6.9$	$197 \pm 16$	104.0	0.31	Mo-1-25	$0.0400 \pm 0.0013$	+	$253.1 \pm 8.3$	$249 \pm 16$	101.5	0.38
Ry-1-105	$0.0414 \pm 0.0019$	$0.306 \pm 0.052$	$261.6 \pm 11.9$	271 ± 46	6.96	0.33	Mo-1-26	0.0458 ± 0.0019		288.5 ± 11.9	$327 \pm 49$	88.1	0.38
Ry-1-106	$0.0383 \pm 0.0013$	$0.280 \pm 0.024$	$242.3 \pm 8.4$	$251 \pm 22$	7.96	0.58	Mo-1-27	$0.0269 \pm 0.0009$	$0.193 \pm 0.016$	171,4 ± 5.9	$179 \pm 15$	95.8	0.21
Ry-1-107	$0.0449 \pm 0.0016$	$0.310 \pm 0.032$	282.9 ± 10.2	275 ± 28	103.0	92.0	Mo-1-28	$0.0214 \pm 0.0008$	$0.153 \pm 0.016$	$136.8 \pm 5.0$	$145 \pm 16$	94.4	0,54
Ry-1-108	$0.0411 \pm 0.0017$	$0.279 \pm 0.041$		250 ± 37	104.0	0.81	Mo-1-29	$0.0289 \pm 0.0010$	$0.202 \pm 0.016$	183,6 ± 6.2	187 ± 15	4.86	0.3
Ry-1-109	$0.0354 \pm 0.0011$	$0.247 \pm 0.012$	$224.1 \pm 6.9$	224 ± 11	8.66	0.43	Mo-1-30	$0.0385 \pm 0.0014$	+1	243.4 ± 9.0	226 ± 27	107.7	0.84
Ry-1-110	$0.0417 \pm 0.0019$	$0.291 \pm 0.048$	263.2 ± 11.7	259 ± 43	101.5	0.80	Mo-1-31	$0.0272 \pm 0.0009$	#	172.9 ± 5.8	172 ± 13	100.4	0.39
Ry-1-111	$0.0395 \pm 0.0012$	$0.292 \pm 0.029$		260 ± 26	36.2	0.74	Mo-1-32	$0.0278 \pm 0.0009$	# 1	176.7 ± 5.7	$176 \pm 11$	100.3	0.5
Ry-1-112	$0.0283 \pm 0.0008$	$0.195 \pm 0.014$	179.8 ± 4.8	181 ± 13	9.66	0.50	Mo-1-33	+)	#	1470.5 ± 45.7	1616 ± 64	91.0	0,42
Ry-1-113	$0.0361 \pm 0.0009$	0.260 ± 0.015	-14	234 ± 14	9.76	69.0	Mo-1-34	$0.0270 \pm 0.0010$	H	$171.6 \pm 6.3$	217 ± 20	79.2	0.5
Ry-1-114	$0.0408 \pm 0.0015$	$0.282 \pm 0.040$	$257.8 \pm 9.5$	252 ± 36	102.2	0.53	Mo-1-35		#	2565.6 ± 79.4	$2499 \pm 95$	102.7	1.04
Ry-1-115	$0.0391 \pm 0.0010$	$0.269 \pm 0.020$	$247.1 \pm 6.6$	242 ± 18	102:0	0.41	Mo-1-36	+	+	520.3 ± 18.1	614 ± 46	84.8	0.62
Ry-1-116	$0.0380 \pm 0.0009$	0.274 ± 0.014	240.7 ± 5.9	246 ± 13	8.76	0.24	Mo-1-37	#	अ	284.9 ± 9.4	$316 \pm 20$	0.06	0.5
Ry-1-117	$0.4326 \pm 0.0098$	$9.409 \pm 0.232$		2379 ± 59	97.4	0.16	Mo-1-38	#	+)	173.9 ± 6.7	$220 \pm 23$	1.67	0.5
Ry-1-118	$0.3283 \pm 0.0075$	5,245 ± 0.144	140	18€0 ± 51	98.4	0.15	Mo-1-39	144	+11	204.1 ± 7.4	245 ± 22	83.2	0,5
Ry-1-119	$0.0474 \pm 0.0013$	$0.394 \pm 0.026$	298.8 ± 7.9	338 ± 22	88.5	96.0	Mo-1-40	#		466.4 ± 10.8	$471 \pm 26$	6'86	0.8
Ry-1-120	$0.0544 \pm 0.0011$	$0.422 \pm 0.021$	$341.7 \pm 6.7$	357 ± 17	95.7	0.32	Mo-1-41		0.174 ± 0.018	139.5 ± 4.3	163 ± 17	85.5	0.92
Ry-1-121	0.0468 ± 0.0014	$0.416 \pm 0.046$	295.1 ± 8.9	353 ± 39	83.6	0.64	Mo-1-42	$0.0361 \pm 0.0009$	$0.261 \pm 0.020$	228.9 ± 5.9	236 ± 18	97.1	0.8
Ry-1-122	$0.0426 \pm 0.0010$	$0.294 \pm 0.026$	$268.9 \pm 6.6$	$261 \pm 23$	102.8	0.52	Mo-1-43	4	$0.175 \pm 0.020$	$176.8 \pm 5.3$	$164 \pm 18$	107.9	0.45
Ry-1-123	$0.0378 \pm 0.0008$	$0.262 \pm 0.015$	-11	$236 \pm 14$	101.5	0.32	Mo-1-44	$0.0465 \pm 0.0011$	$0.333 \pm 0.022$	$293.2 \pm 7.1$	$292 \pm 19$	100.4	0.20
Ry-1-124	$0.0403 \pm 0.0013$	$0.312 \pm 0.039$		276 ± 35	92.3	0.53	Mo-1-45	$0.3440 \pm 0.0073$	5.353 ± 0.171	1906,1 ± 40,6	$1877 \pm 60$	101.5	0.25
Ry-1-125	$0.0422 \pm 0.0017$	$0.319 \pm 0.058$		$281 \pm 51$	94.7	0.50	Mo-1-46	$0.0202 \pm 0.0010$	$0.150 \pm 0.031$	$128.7 \pm 6.1$	$142 \pm 29$	90.5	0.57
Ry-1-126	$0.0392 \pm 0.0010$	$0.250 \pm 0.024$	240	226 ± 22	9.601	0.54	Mo-1-47	0.0276 ± 0.0009	₩.	$175.5 \pm 5.5$	181 # 18	2.96	0,64
Ry-1-127	$0.0401 \pm 0.0009$	$0.270 \pm 0.020$	+1	243 ± 18	1043	0.35	Mo-1-48	$0.0272 \pm 0.0009$	$0.224 \pm 0.024$	$172.7 \pm 5.7$	205 ± 22	84.1	0.62
Ry-1-128	$0.0427 \pm 0.0011$	0,306 ± 0.027	$269.7 \pm 6.7$	$271 \pm 24$	5.66	0.80	Mo-1-49	$0.0424 \pm 0.0012$	$0.285 \pm 0.021$	267,8 ± 7.5	255 ± 19	105.2	0.73
							Mo-1-50	$0.0450 \pm 0.0017$	$0.383 \pm 0.052$	283.8 ± 10.9	329 ± 45	86.2	0.46
	Sandstone of the Mon	Sandstone of the Monobe Formation (Mo-1; 33 42, 51.15" N,	33 42 51.15" N,	133 50' 05.49" E)			Mo-1-51	$0.0208 \pm 0.0006$	$0.140 \pm 0.010$	$132.5 \pm 3.7$	133 ± 10	9.66	0.49
Mo-1-1	$0.0319 \pm 0.0009$	$0.230 \pm 0.014$	202.3 ± 5.5		4.96	0.40	Mo-1-52	$0.0347 \pm 0.0010$	$0.258 \pm 0.019$	$219.7 \pm 6.2$	233 ± 17	94.3	0.84
Mo-1-2	$0.0287 \pm 0.0008$	$0.186 \pm 0.013$	$182.5 \pm 5.1$	173 ± 12	105.5	0.52	Mo-1-53	4	41 -	$127.5 \pm 5.9$	$119 \pm 25$	107.6	0.9
Mo-1-3	$0.0289 \pm 0.0008$	0.211 ± 0.017	183.5 = 5.4	194 ± 15	94.4	0.50	Mo-1-54	+1 -	# -	2414,8 ± 60.9	2199 ± 84	8.601	0
Mo-1-4	0.0286 ± 0.0008	0.211 ± 0.014			93.5	0.40	Mo-1-55	# :	40	268.1 ± 11.7	349 ± 47	16.8	0.43
Mo-1-5	0.3127 ± 0.0078	5.917 ± 0.187		+1	89.3	0.12	Mo-1-56	#( :	0.148 ± 0.020	124.5 ± 5.1	140 ± 19	88.8	0.91
Mo-1-6	0.0543 ± 0.0015	0.485 ± 0.030	340.7 ± 9.4	402 ± 24	84.8	0.00	Mo-1-57	$0.3274 \pm 0.0100$	5.159 ± 0.201	1825.6 ± 55.8	1846 ± 72	686	0.62
Mo-1-/	0.0413 ± 0.0014	0.429 ± 0.040		302 ± 34	17.7	0.03	Mo-1-58	# .	# :	175.9 ± 5.8	179 ± 13	1.86	0
Mo-1-8	$0.0311 \pm 0.0011$	0.231 ± 0.028	197.2 ± 7.1	211 ± 26	93.3	0.50	Mo-1-59	0.3195 ± 0.0097	+1 -	1787.4 ± 54.2	1827 ± 68	8.76	0.3
Mo-1-9	0.0386 ± 0.0008	0.2/9 ± 0.020	244.4 ± 4.8	250 ± 18	6/6	0.20	Mo-1-60	Ð.,	# .	306,2 ± 12.7		4.46	0.41
01-1-0W	0.0900 ± 0.0012	1.171 ± 0.033	238.9 ± 7.3	78/ # 75/	0.17	7770	10-1-0W	# -	H =	192.2 ± 0.7	#1 = C17	2000	0.72
Moriell	0.0271 ± 0.0004	0.194 ± 0.010		180 # 3	1.00	0.35	Mo-1-62	H	0.149 ± 0.015	141.9 # 3.2	71 # 161	5005	5 6
Mo-1-12	0.0290 ± 0.0009	5740 ± 0.027	Н -	184 ± 23	100.0	07.0	Mo-1-03	Η -	H -	131.3 ± 0.0	200 ± 10	20.9	0.33
Min-1-12	0.3390 = 0.0047	5.240 ± 0.146	1007 = 0.1001	20 # 9501	2.101	0.04	NA-1-04	0.020/ = 0.00/0	6.05A ± 0.018	1070 1 + 55 7	1024 + 00	000	0.00
Ma-1-15	0.000 + 0.000	0475 + 0.047	H +	107 H 30	85.0	0.77	Mo-1-66	1.4	4 4	1880 + 69	194 + 16	0.00	5 0
160 1 16	0.0750 - 0.0000	1400 - 5740	1773 + 60	100 - 33	2.70	0.66	Me 1 67	4. 9	1 4	156 1 4 6.1	173 - 16	20.2	100
Mo-1-17	0.3383 + 0.0054	\$ 873 ± 0.157	1878 3 # 30 1	1950 + 53	6 90	0.11	Mo-1-68	9 9	4	2110 + 32	327 ± 13	03.0	0.30
Me I 10	0.0363 + 0.0007	7.00 ± 0.000		922 ± 14	9 80	46.0	Me 1 60	02300 + 0.0036	1.9	100 1 4 1001	1000 T 40	020	0.11
Mo-1-19	0.0298 ± 0.0007	0.212 ± 0.017	189.4 ± 4.2		96.8	0.55	Mo-1-70	1 +	1 1	2423.2 ± 25.1	2347 ± 55	103.2	0.0
Mo-1-20	0.0225 ± 0.0004	0.156 ± 0.008	143.4 ± 2.7	147 ± 8	7.76	0.45	Mo-1-71		+	146.3 ± 2.1	159 ± 8	8.16	0.32
1000	100000000000000000000000000000000000000						-				1	1	
Mo-1-21	$0.0306 \pm 0.0006$	$0.223 \pm 0.014$	194.6 ± 5.9	204 ± 13	95.3	0.29	Mo-1-72	$0.0300 \pm 0.0005$	$0.215 \pm 0.016$	190.6 ± 3.4	198 ± 15	96.3	0.48

Grain	$\Omega_{822}/9d_{WG}$	Osta/9d <sub>Lint</sub>	<sup>206</sup> pb/ <sup>238</sup> U age (Ma)	207Pb/235U age (Ma)	%conc	Th/U	Grain	$\Omega_{8EZ}/Qd_{yoz}$	D <sub>5E</sub> /9d <sub>205</sub>	20%Pb/ <sup>238</sup> U age (Ma)	<sup>207</sup> Pb/ <sup>225</sup> U age (Ma)	%conc	Th/U
Mo-1-74	$0.0401 \pm 0.0006$	0,286 ± 0,015	253.2 ± 3,7	255 ± 14	99.2	0,48	9-I-nA	$0.0294 \pm 0.0012$	$0.187 \pm 0.021$	187,0 ± 7,4	174 ± 20	107.2	0.5
Mo-1-75	$0.4317 \pm 0.0046$	$11.732 \pm 0.274$	2313,5 ± 24,5	#	89.6	0.65	Yu-1-7		$0.193 \pm 0.019$	$173.9 \pm 6.7$	179 ± 18	97.1	0.55
Mo-1-76	$0.3360 \pm 0.0042$	5.314 ± 0.171		410	8.66	0.65	Yu-1-8	0.0275 ± 0.0010	0.188 ± 0.015	$174.6 \pm 6.3$	175 ± 14	666	0.67
Mo-1-77	0.0418 ± 0.0018	0.299 ± 0.049	263,7 ± 11.2	265 ± 44	99.4	0.63	Vu-1-9	0.0271 ± 0.0010	0.200 ± 0.016	1/2.1 ± 6.3	183 ± 15	92.9	0.35
MIO-1-/8	0.0301 ± 0.0009	0.216 ± 0.014	1467 = 47	198 ± 15	200	0.54	Ve. 1 11	0.2430 ± 0.0043	# 7	1415.0 ± 45.0	1367 ± 37	2.60	0.79
Mo-1-80	0.0230 ± 0.0000	0.00 = 0.010		242 + 12	900	0.57	Vn-1-17	+ +	7	2221 + 53	230 + 18	03.1	0.32
Mo-1-81	0.0199 ± 0.0007	0.136 ± 0.014		129 ± 13	98.2	0.63	Yu-1-13	0.0277 ± 0.0007	1 11	176.3 ± 4.1	188 ± 14	93.5	0.3
Mo-1-82	$0.0270 \pm 0.0007$	0.181 ± 0.010	-#	169 ± 10	101.3	0.36	Yu-I-14	0.0286 ± 0.0006	+	181.7 ± 3.7	194 ± 10	93.6	0.55
Mo-1-83	$0.0310 \pm 0.0011$	0.226 ± 0.025	$6.9 \pm 6.961$	207 ± 23	95.2	09.0	Yu-1-15	-91	+	$236.0 \pm 6.6$	310 ± 28	0.94	0.83
Mo-1-84	$0.0214 \pm 0.0007$	$0.154 \pm 0.012$	136.6 ± 4.2	145 ± 12	0.40	0.61	Yu-1-16	$0.3368 \pm 0.0061$	5.212 ± 0.138	$1871.1 \pm 34.1$	$1855 \pm 49$	100.9	0.29
Mo-1-85	$0.0682 \pm 0.0020$	$0.545 \pm 0.038$	$425.3 \pm 12.2$	442 ± 31	€963	99.0	Yu-1-17	$0.0243 \pm 0.0006$	-81	154.8 ± 3.6	177 ± 13	87.4	0.4
Mo-1-86	$0.2160 \pm 0.0054$	3.243 ± 0,106	1260.6 ± 31.6	1468 ± 48	85.9	0.28	Yu-1-18	$0.0297 \pm 0.0008$	#	$188.6 \pm 5.0$	$201 \pm 19$	93.7	0.54
Mo-1-87	$0.0299 \pm 0.0010$	0.300 ± 0.027	189.9 ± 6.2	266 ± 24	71.3	1.10	Vu-1-19	*	$^{\rm H}$	2209,1 ± 45.9	2252 ± 70	98.1	0.47
Mo-1-88	$0.0395 \pm 0.0011$	0.303 ± 0.017	249.6 ± 6.8	269 ± 15	92.8	0.13	Yu-1-20	0.0397 ± 0.0010	$0.423 \pm 0.026$	251.1 ± 6.3	358 ± 22	70.1	0.4
Mo-1-89	$0.0207 \pm 0.0006$	$0.150 \pm 0.012$	+1	$142 \pm 11$	93.1	0.81	Yu-1-21	#	#	$198.7 \pm 6.0$	$208 \pm 22$	92.6	0,50
Mo-1-90	$0.0292 \pm 0.0009$	0.198 ± 0.016	185.5 ± 5.5	+1	6'001	0.34	Yu-1-22	**	++	239.6 ± 6.6	328 ± 26	73.0	0.71
Mo-1-91	$0.0702 \pm 0.0020$	$0.559 \pm 0.041$		451 ± 33	6.96	66.0	Yu-1-23	#	4	142.5 ± 3.4	$167 \pm 70$	85.3	0.47
Mo-1-92	$0.0273 \pm 0.0008$	$0.213 \pm 0.015$	173.4 ± 5.0	196 ± 14	88.3	0.21	Yu-1-24	#	# .	254,4 ± 6.0	250 ± 15	101.9	0.7
Mo-1-93	$0.0225 \pm 0.0007$	0.150 ± 0.012		142 ± 12	101.0	0.32	Yu-1-25	# -	$0.211 \pm 0.013$	188.8 ± 4.5	194 ± 12	97.3	0.35
Mo-1-94	$0.0339 \pm 0.0016$	0.234 ± 0.027	214.9 ± 10.2	214 ± 25	100.5	0,75	Yu-1-26	41 -	+1 -	115,5 ± 2,7	115 ± 7	9.001	1.06
MO-1-95	0.4299 ± 0.0182	9.075 ± 0.45/		2404 ± 109	40.5	0.24	17-1-11	44 4	0.150 ± 0.021	17/0 # 4/1	197 # 20	00.7	050
Mo.1.97	0.0442 ± 0.0021	5 656 ± 0.004	1077 6 4 83 8	1075 ± 90	102 5	0.10	Vo. 1.70	0.0204 ± 0.0000	0.140 ± 0.009	1736 ± 5.8	133 # 8	98.2	0.30
16. 1.00	0.03584 + 0.0017	0.200 + 0.200	301 + 700	317 + 18	76.5	0.56	Vu. 1.30	03110 + 0.0086	4 865 + 0.187	1750 0 + 48 4	1706 + 67	07.4	0.24
Mo-1-99	0.2874 ± 0.0125	4.125 ± 0.230		1659 ± 92	98.2	0.63	Yu-1-31	$0.0331 \pm 0.0010$	H 44	209.7 ± 6.5	242 ± 18	86.6	0.77
Mo-1-100	0.0339 ± 0.0016	0.258 ± 0.024	215.1 ± 9.9	233 ± 22	92.4	0.74	Yu-1-32		$0.224 \pm 0.019$	189.9 ± 6.1	206 ± 18	92.4	0.43
Mo-1-101	$0.4064 \pm 0.0173$	8.405 ± 0.397		2276 ± 107	9.96	0.92	Yu-1-33		+	184.6 ± 6.0	193 ± 17	95.5	0.37
Mo-1-102	$0.0395 \pm 0.0013$	$0.356 \pm 0.040$		310 ± 34	80.8	0.45	Yu-1-34	0.0357 ± 0.0015	40	226.2 ± 9.3	276 ± 38	81.8	0.62
Mo-1-103	$0.0461 \pm 0.0015$	$0.340 \pm 0.039$	290.8 ± 9.3	297 ± 34	8.7.6	0.60	Yu-1-35	+	-11	$193.0 \pm 6.4$	208 ± 19	97.6	0.53
Mo-1-104	$0.0281 \pm 0.0007$	$0.195 \pm 0.012$	44	$181 \pm 11$	6'86	0.81	Yu-1-36	44	+1	$300.5 \pm 8.7$	$280 \pm 16$	107.2	0.27
Mo-1-105	$0.0277 \pm 0.0008$	$0.210 \pm 0.021$		194 ± 20	8.06	69.0	Yu-1-37	4	+	$234.2 \pm 5.3$	240 ± 15	97.5	0.35
Mo-1-106	$0.2830 \pm 0.0062$	$4.305 \pm 0.151$	$1606.3 \pm 35.1$	1694 ± 59	94.8	0.37	Yu-1-38	+	#1	$124.1 \pm 3.4$	137 ± 13	90.4	1.25
Mo-1-107	$0.0271 \pm 0.0006$	0.192 ± 0.012	172.5 ± 4.1	178 ± 11	6.7	0.39	Yu-1-39		#	$179.2 \pm 5.9$	193 ± 24	93.1	0.8
Mo-1-108	0.0277 ± 0.0007	0.193 ± 0.014	88.18	179 ± 13	98.2	0.37	Yu-1-40	40	#	165.8 ± 4.3	187 ± 15	88.8	0.69
Mo-1-109	$0.0428 \pm 0.0011$	$0.307 \pm 0.024$		$272 \pm 21$	666	0.49	Yu-1-41	#	#1	$171.7 \pm 4.1$	176 ± 13	97.6	0.62
Mo-1-110	$0.0271 \pm 0.0006$	0.185 ± 0.012	172.7 = 4.1	172 ± 11	100.1	0.40	Yu-1-42	0,2895 ± 0.0058	4.492 ± 0.147	1639.0 ± 32.6	1730 ± 57	8.4.8	0.42
Mo-1-111	0.4320 ± 0.0091	8,808 ± 0,288	1003 + 54	0/ ± 4267	2.66	0.74	Va. 1.44	0.00330 ± 0.0000	0.252 ± 0.017	261 0 ± 5.0	271 ± 120	0.16	0.30
Marietta	0.0423 ± 0.0014	0 332 + 0 042			010	0.61	V.1.45	4 4	1 +	2106 + 55		000	0.71
Mo-1-114	0.0394 ± 0.0000	0.402 ± 0.023	248.8 ± 5.9	343 ± 19	72.6	0.33	Yu-1-46	(-4)	1	1911.0 ± 41.5	1887 ± 80	101.3	0.19
Mo-1-115	0.0530 ± 0.0013	0.480 ± 0.029			83.7	0.53	Yu-1-47	-11	+1	198.1 ± 5.6	243 ± 21	81.5	0.57
Mo-1-116	$0.3320 \pm 0.0069$	5,318 ± 0,172	41		7.86	61.0	Yu-1-48	+	+	197.4 ± 4.7	+	94.2	0.37
Mo-1-117	$0.0267 \pm 0.0006$	$0.180 \pm 0.011$	$169.6 \pm 3.9$	168 ± 10	100.8	0.53	Yu-1-49	$0.0217 \pm 0.0006$	0.167 ± 0.014	138.3 ± 3.8	157 ± 13	88.3	0.47
							Yu-1-50	+	+1	2035.7 ± 44.8	2088 ± 90	97.5	0.21
San	Sandstone of the lower part of the Yunoki Formation (Yu-1; 33° 42'	The Yunoki Formation	1 (Yu-1; 33° 42' 31.)	17" N, 133" 50" 0	2		Yu-1-51	#	#	$1679.1 \pm 37.0$	1747 ± 77	96.1	0.26
Vu-1-1	$0.0453 \pm 0.0015$	0.325 ± 0.015	9.4	286 ± 13	-	0.70	Yu-1-52	+	$0.148 \pm 0.017$	$132.6 \pm 4.2$		94.6	0.74
Yu-1-2	0,0232 ± 0,0009	0.223 ± 0.022	5,9	204 ± 20	72.4	0.59	Yu-1-53		#	$137.4 \pm 4.5$	149 ± 18	92.3	0.68
200	01000	2000							,				0.0
2-1-n.	0.0283 ± 0.0010	0.210 # 0.015	180.1 ± 6.3	198 ± 14		0.45	Yu-1-54	0.0195 ± 0.0006	0.129 ± 0.009	124.6 ± 3.6	123 ± 8	101.5	0.82

TABLE 1. (Continued)

Grain	Ω <sub>852</sub> /9d <sub>9062</sub>	U255/94710E	Coopb/238U age (Ma)	207Pb/235U age (Ma)	%conc	Th/U	Grain	$\Omega_{8E}/9d_{902}$	$^{207}{\rm Pb}/^{235}{\rm U}$	Pb/ U age (Ma)	(Ma)	%conc	Th/U
Yu-2-26		$0.236 \pm 0.024$	179.1 ± 5.0	215 ± 22	83.2	0.46	Yu-2-77	#	$0.480 \pm 0.074$	$379.4 \pm 13.5$	$398 \pm 61$	653	0.51
Yu-2-27	0.0301 ± 0.0014	0.360 ± 0.100	191.2 ± 8.9	# 1	2.79	1,41	Yu-2-78	#	+	$465.9 \pm 8.9$	453 ± 34	102.8	0.93
Yu-2-28	$0.0400 \pm 0.0012$	$0.269 \pm 0.035$	252.7 ± 7.3		104.5	0.30	Yu-2-79	#	#	+1	150 ± 15	86.8	0.99
Yu-2-29	0.0272 ± 0.0070	0.209 ± 0.054	173.1 ± 6.7	+1 .	89.8	0.63	Yu-2-80	11	# :	# 1	140 ± 21	81.7	1.23
Yu-2-30	0.0177 ± 0.0005	0.123 ± 0.018	113.0 ± 3.4		95.9	0.70	111-7-81	# .	41	176.0 ± 2.8	198 ± 12	88.8	0.42
Yu-2-31	$0.0468 \pm 0.0014$	0,338 ± 0.050	294.6 ± 9.1		2.66	0.56	Vu-2-82	0.0665 ± 0.0012	$0.490 \pm 0.036$	414.8 ± 7.8	405 ± 30	102,4	0.75
Yu-2-32	0.0239 ± 0.0008	0.171 ± 0.029	152.2 ± 4.9	160 ± 27	95.2	0.64	Yu-2-83	11 -	++ -	221.8 ± 4.2	205 ± 16	108.0	0.44
14-2-53	0.0293 ± 0.0011	0.498 ± 0.000	187.3 ± 7.0	410 = 54	42.7	0.71	Yu-2-84	# -	H -	458.9 ± 9.8	445 ± 38	103.1	0.70
FU-2-07	0.0502 ± 0.0008	0.216 ± 0.021	191.6 ± 5.1	199 ± 19	20.0	0.34	Tu-2-85	0.4526 ± 0.0073		2400.8 ± 39.0	2383 ± 103	0.101	0.00
CE-7-0X	0.0094 ± 0.0028	0.339 # 0.066		451 H 54	92.8	0.40	Tu-2-80	H -	# -	121.4 ± 2.9	125 ± 15	576	0.00
Yu-2-30	0.0727 = 0.0026	0.050 ± 0.050		11 -	17.6	0.71	Yu-2-8/	# -	0.197 ± 0.010	185.4 ± 5.0	183 ± 15	0,101	0.41
Yu-2-3/	0.0029 ± 0.0013	0.415 ± 0.052	207 6 ± 12.0	198 ± 29	77.0	0.02	Vo. 2 50	0.043/ ± 0.0015	0.306 ± 0.048	127.7 ± 9.4	205 + 14	8010	0.48
Va. 2.30	0,000 = 2,000	0.577 ± 0.000		4 4	910	0000	Va. 2.00	0.4	H 7	1916 4 4 360	1911 + 91	1003	1.40
04 C nA	0.0708 # 0.0025	0.567 + 0.050		4 3	0.70	0.70	Va 7 01	4.4	1 3	180 0 4 37	203 + 13	88.0	080
VII.2.41	0.0301 + 0.0011	0213 + 0.020		106 + 18	07.3	0.40	Vu-2.02	1 +	1 +	311 + 6196	745 + 48	1001	0.58
Vu-7-47	0.000 + 0.0000	0 348 + 0 056	2641 + 12.5		87.1	0.46	Vu-2-03	+	+	160.7 + 3.6	177 + 13	900	970
Yu-2-43	0.0347 ± 0.0007	0.249 ± 0.019		+	673	0.94	Yu-2-94	4	+	290.4 ± 7.2		95.7	0.41
Yu-2-44	$0.0344 \pm 0.0005$	$0.251 \pm 0.009$	218.3 ± 2.9	227 ± 8	0.96	0.89	Yu-2-95	+	+	1810.2 ± 34.3	1819 ± 72	99.5	06.0
Fu-2-45	0.0187 ± 0.0007	0.105 ± 0.020	119.2 ± 4.2	+	117.3	0.57	Yu-2-96	$0.0211 \pm 0.0006$	-9	134.6 ± 3.8	139 ± 16	1.96	0.59
Yu-2-46	$0.0384 \pm 0.0008$	0.286 ± 0.025	243.0 ± 5.3	+	95.2	0.62	Yu-2-97	4	+1	1655.3 ± 35.6	$1784 \pm 87$	92.8	0.13
Yu-2-47	0.0344 ± 0.0007	$0.274 \pm 0.022$	218.0 ± 4.5	246 ± 20	88.6	0.67	Yu-2-98	+	-44	239,4 ± 5.7	235 ± 21	101.9	0.18
Yu-2-48	$0.4062 \pm 0.0055$	7.337 ± 0.201	2197.6 ± 29.9	+	102.1	0.21	Yu-2-99	$0.3328 \pm 0.0060$	5.229 ± 0.165	1851.7 ± 33.6	1857 ± 59	7.66	0.29
Yu-2-49	$0.3779 \pm 0.0044$	7.013 ± 0.124	2066.5 ± 24.1	2113	8.76	0.46	Yu-2-100	$0.0286 \pm 0.0008$	$0.198 \pm 0.023$	181,5 ± 5.2	183 ± 21	6.86	0.93
Yu-2-50	$0.2893 \pm 0.0038$	4,471 ± 0,117	1637.8 ± 21.4	1726	676	0.23	Yu-2-101	.41	$0.512 \pm 0.036$	$430.5 \pm 9.7$	420 ± 30	102.6	0.92
Yu-2-51	$0.0197 \pm 0.0007$	$0.185 \pm 0.025$	125.6 ± 4.2	173	72.7	0.45	Yu-2-102	$0.0675 \pm 0.0016$	$0.489 \pm 0.040$	$421.2 \pm 10.1$	404 ± 33	104.1	0.85
Yu-2-52	$0.0272 \pm 0.0006$	0,189 ± 0.011	173.2 ± 3.7	176	98.4	0.30	Yu-2-103	+4	0.809 ± 0.078	279.1 ± 9.5	602 ± 58	40.4	0.18
14-2-53	$0.0357 \pm 0.0012$	$0.293 \pm 0.040$	226.1 ± 7.9		86.6	0.25	Yu-2-104	$0.0352 \pm 0.0008$	$0.243 \pm 0.016$	$223.3 \pm 4.8$	$221 \pm 15$	101.1	0.59
Yu-2-54	$0.0185 \pm 0.0006$	$0.119 \pm 0.016$	118.0 ± 3.8	114	103.6	0.28	Yu-2-105	#	$0.295 \pm 0.049$	$249.4 \pm 9.4$	262 ± 44	95.1	0.51
Fu-2-55	$0.0460 \pm 0.0023$	$1.682 \pm 0.191$	290.2 ± 14.3	1002	29.0	0.48	Yu-2-106	# .	$0.136 \pm 0.031$	121.3 ± 5.5	130 ± 29	93.4	0.81
Yu-2-56	$0.0280 \pm 0.0007$	$0.207 \pm 0.016$	177.8 ± 4.3		93.2	0.38	Yu-2-107	# .	+1 -	$220.9 \pm 4.2$	$234 \pm 10$	94.2	0.26
Yu-2-5/	0.0280 ± 0.0007	0.210 ± 0.018	178.3 = 4.6	193	92.2	0.20	Yu-2-108	41 -	0.181 ± 0.012	169.8 ± 4.0	10 = 691	100.6	0
N-2-17	0,09/8 ± 0,00/9	1.203 ± 0,047	601.8 = 11.9	030	(4.5	0.15	Yu-2-109	#	0.206 ± 0.017	1/5,0 = 4.7	190 ± 16	77.76	0.38
Vu-2-59	$0.31/4 \pm 0.0000$	4.970 ± 0.145	1777.3 = 55.4	# 6181	98.0	0.73	Yu-2-110	#	H. :	282.0 ± 10.0	# :	5000	0.48
09-7-nA	0.0441 ± 0.0011	0.532 ± 0.027	2/8.1 ± 0.9	167	0.00	100	Yu-2-111	н -	H :	193.3 ± 7.2	188 ± 50	103.0	0.55
10-7-01	0.0272 ± 0.0003	210.0 ± 0.000	1/3/2 # 3/1		9.00	0.00	711-7-117	0.0070 ± 0.0000	0.195 ± 0.020	174.3 ± 3.1	101 ± 191	# C6	0.44
7 n-2-02	0.0000 ± 0.0010	0.143 # 0.029	127.5 + 8.7	135	5.00	0.00	11-2-112 Vi 7 174	H. d	н н	25/17 + 10:3	252 ± 54	100	07.0
V. 2.64	0.0230 + 0.0005	1100 + 5110	1468 + 30	147	107.1	0.36	Va-7-115	1 +	+	153.1 + 71.7	1 +	77.3	0.77
Fu. 7.65	00372 + 00008	0.375 + 0.028	236.2 + 6.38	FCE	23.7	0.28	Vn-7-116	4	(d	1073+31	1	850	0.85
Vu-2-66	0.0433 ± 0.0015	0.288 ± 0.046	273.5 ± 9.6	1	106.4	0.37	Yu-2-117	1-11	1 -31	233.3 ± 6.7		80.4	0.47
Vu-2-67	$0.0267 \pm 0.0006$	0.180 ± 0.014	170.1 ± 3.6	-18	101.3	0.50	Vu-2-118	-	+	270.5 ± 10.3	+	1001	0.52
Yu-2-68	$0.0433 \pm 0.0014$	0,306 ± 0,030	273.2 ± 9.1		100.7	0.39	Yu-2-119	+	.4	1830.9 ± 42.7	1847 ± 64	1.66	0.7
Yu-2-69	$0.0735 \pm 0.0023$	0.612 ± 0.048	457.2 ± 14.4	485 ± 38	94.3	0.63	Yu-2-120	+	+	144	+	92.2	0.57
Yu-2-70	$0.0172 \pm 0.0006$	$0.127 \pm 0.014$	$109.7 \pm 3.9$	122 ± 14	90.2	0.48	Yu-2-121	$0.0686 \pm 0.0019$	+	427.6 ± 11.9	+	96.1	0.90
E4-2-71	0.0276 ± 0.0009	$0.223 \pm 0.020$	175.4 ± 5.8	204 ± 19	85.9	0.55	Yu-2-122	$0.0419 \pm 0.0018$	$0.322 \pm 0.056$	264.4 ± 11,4	284 ± 50	93.2	0.41
Yu-2-72	$0.0341 \pm 0.0010$	$0.239 \pm 0.011$	$216.4 \pm 6.0$	#	666	0.11	Yu-2-123	$0.0479 \pm 0.0014$	$0.339 \pm 0.036$	264.5 ± 8.6	+	89.3	0.46
Yu-2-73	$0.0343 \pm 0.0011$	0,268 ± 0.025	217.3 ± 7.3		500.5	0.67	Yu-2-124	+1	-81	523.1 ± 14.5	++	67.3	0.41
Yu-2-74	$0.0289 \pm 0.0009$	0.207 ± 0.016	$183.9 \pm 5.7$	+	6.96	0.44	Yu-2-125	$0.2967 \pm 0.0071$	4.615 ± 0.175	$1675.0 \pm 39.9$	$1752 \pm 67$	95.6	0.38
Yu-2-75	$0.0262 \pm 0.0008$	$0.183 \pm 0.013$	$166.5 \pm 5.1$	$171 \pm 12$	97.4	0.50							
Yu-2-76	$0.0335 \pm 0.0009$	$0.240 \pm 0.026$	212.5 ± 5.4	$219 \pm 24$	97.2	0.62							

Sundation of the Hilbher and the Hilbher control of Hilbher and the Hil	Standsmore of the Hibblen is Pounding (H-13) 47 (12.54 N. N. 13) 49 (13.24 P.)         Hil-3         0.0195 ± 0.0009         0.117 ± 0.013         Hil-3         0.0175 ± 0.0009         0.117 ± 0.021         0.018 ± 0.0009         0.117 ± 0.021         Hil-3         0.057 ± 0.0009         0.117 ± 0.0009         0.017 ± 0.0009         0.117 ± 0.018         1.11 ± 0.0009         0.017 ± 0.0009	Sundiction of the Hilbs of Part Service of the Hilbs of Part Service of the Hilbs of Collect and Collec	Grain	Ω852/9dy02	D552/9d_002	(Ma)	W.Pb/**3U age (Ma)	%conc	Th/U	Grain	Oxez/94,002	207Pb/235U	Pb/ U age (Ma)	(Ma)	%conc	Th/U
0.0187 ± 0.0009 0.131 ± 0.0021 11.17 ± 5.55 11.2 ± 27 0.148 0.65 11.17 ± 0.0009 0.131 ± 0.0018 11.17 ± 0.021 11.17	0.033 ± 0.009 0.131 ± 0.03 117 ± 0.03 117 ± 0.03 113 ± 0.03 111.5 ± 0.0175 ± 0.009 0.031 ± 0.009 0.0	0.0187 ± 0.0009 0.117 ± 0.021 0.0187 ± 0.0008 0.114 ± 0.021 0.0187 ± 0.0008 0.114 ± 0.021 0.0187 ± 0.0008 0.114 ± 0.021 0.0187 ± 0.0008 0.114 ± 0.021 0.017 ± 0.0008 0.114 ± 0.031 0.017 ± 0.0009 0.114 ± 0.031 0.017 ± 0.0009 0.114 ± 0.031 0.0187 ± 0.0008 0.113 ± 0.033 0.114 ± 0.031 0.0187 ± 0.0008 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.001 0.114 ± 0.031 0.0184 ± 0.0008 0.114 ± 0.001 0.114 ± 0		Sandstone of the Hibiha	ara Formation (Hi-1;	z	50, 34.28"			Hi-1-51	0.0197 ± 0.0009	+9	125.9 ± 5.9		85.0	0.43
0.0183 ± 0.0008 0.142 ± 0.007 11.70 ± 5.3 11.71 ± 1.7 34 0.155 11.8 16 0.055 11.8 10.007 0.0183 ± 0.0008 0.112 ± 0.018 0.0183 ± 0.0009 0.112 ± 0.018 0.018 ± 0.0009 0.112 ± 0.018 0.018 ± 0.0009 0.013 ±	0.0083 ± 0.0000 0.013 ± 0.000 0.013 ± 0.018 ± 0.000 0.013	0.0183 ± 0.0008	1-1-19	$0.0184 \pm 0.0009$	0.117 ± 0.021	117.4 ± 5.6	-81	104.8	0.62	Hi-1-52		#	$112.2 \pm 3.2$		92.0	1.09
0.0183 ± 0.0000 0.142 ± 0.029 17.7.2 ± 5.3 18 ± 19 8.6.4 0.5.3 Hi-1-55 0.0293 ± 0.0000 0.029 ± 0	0.003 ± 0.0000 0.112 ± 0.000 0	0.0183 ± 0.0008	H-1-2	$0.0187 \pm 0.0008$	0.133 ± 0.018	$119.2 \pm 5.3$		94.2	0.55	Hi-1-53	+	#	105.3 ± 4.1		83.3	0.38
0.0183 ± 0.0008 0.1112 ± 0.018 1   17.0 ± 5.5   10.8 ± 1   10.8   10.5   0.5   Hi-3-5   0.0298 ± 0.0000 0.209 ± 0.001	0.0151 ± 0.0000 0.0171 ± 0.018 0.018 0.018 0.056 0.019 0.0000 0.023 ± 0.019 0.023 ± 0.024 0.021 0.022 0.023	0.0491 ± 0.0000 0.112 ± 0.013	11-1-3	$0.0183 \pm 0.0008$	$0.142 \pm 0.020$	$116.7 \pm 5.2$	135 ± 79	86.4	0.53	Hi-1-54	$0.0179 \pm 0.0008$	+	114.4 ± 5.1	121 ± 24	94.1	0.62
0.04451 ± 0.00070 0.0371 ± 0.043 ± 0.045 1 ± 0.045 1 ± 0.045 1 ± 0.0008 0.044 ± 0.0008 0.034 ± 0.0008 0.031 ± 0.0008 0.032 ± 0.0008 0.033 ± 0.0008 0.033 ± 0.0008 0.033 ± 0.0008 0.033 ± 0.0008 0.033 ± 0.0008 0.033 ± 0	0.0019 = 0.0009	0.0391 ± 0.0020	H-1-4	$0.0183 \pm 0.0008$	$0.112 \pm 0.018$	$117.0 \pm 5.3$	$108 \pm 17$	108.7	0.56	Hi-1-55	$0.0928 \pm 0.0020$	#	$572.0 \pm 12.5$	610 ± 25	93.8	0.19
0.0419 ± 0.0009 0.112 ± 0.0018 1384 ± 59. 135 ± 11 102.3 0.35 HE1-35 0.0004 ± 0.0008 0.124 ± 0.0018 0.008 ± 0.0009 0.112 ± 0.0018 0.008 ± 0.0009 0.114 ± 0.0018 0.113 ± 0.017 0.21 11.0 ± 54 11.2 ± 10 10.7 0.95 HE1-39 0.0044 ± 0.0018 0.134 ± 0.0018 0.114 ± 0.0018 0.114 ± 0.0018 0.114 ± 0.0018 0.114 ± 0.002 0.11	0.0017 ± 0.0009 0.14.2 ± 0.018 134.4 ± 59 135 ± 17 102.3 0.24 14-15 0.0009 0.124 ± 0.0019 152.4 ± 6.3 117.4 ± 19 0.0019 ± 0.0019 0.124 ± 0.018 134.4 ± 59 135 ± 17 0.44 14-15 0.0019 ± 0.0009 0.124 ± 0.0021 17.2 ± 6.4 15 ± 6.4 ± 1.2 ± 1.0 ± 1	0.01/19 ± 0.0019         0.142 ± 0.0018         0.134 ± 15.0         135 ± 15.1         102.3         114-37         0.0200           0.01/9 ± 0.0018         0.013 ± 0.0018         0.013 ± 0.0018         0.013 ± 0.0018         0.013 ± 0.0018         0.014 ± 0.0018         0.014 ± 0.0018         0.014 ± 0.0018         0.019 ± 0.0009         0.019 ± 0.0009         0.019 ± 0.0009         0.019 ± 0.0009         0.019 ± 0.0009         0.019 ± 0.0009         0.017 ± 0.0012         1.02 ± 5.4         1.02 ± 0.01         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.017 ± 0.0009         0.018 ± 0.0009	1-1-5	$0.0451 \pm 0.0020$	$0.317 \pm 0.043$	284.5 ± 12.6	280 ± 38	8.101	99.0	Hi-1-56	+1	4	188,1 ± 4.5	193 ± 12	97.5	0.46
0.0199 ± 0.0018 0.013 ± 0.013 ± 0.044 ± 11.2 ± 0.04 ± 11.2 ± 0.04 ± 0.0018 0.013 ± 0.0008 0.017 ± 0.0008 0.017 ± 0.0009 0.014 ± 0.0018 0.017 ± 0.0009 0.014 ± 0.0018 0.017 ± 0.0009 0.014 ± 0.021 0.015 ± 0.022 ± 0.002 0.019 ± 0.0009 0.014 ± 0.021 0.015 ± 0.0009 0.014 ± 0.0018 0.017 ± 0.0009 0.014 ± 0.0018 0.013 ± 0.0009 0.017 ± 0.0009 0.014 ± 0.0018 0.013 ± 0.0009 0.017 ± 0.0009 0.011 ± 0.0009 0.011 ± 0.0009 0.011 ± 0.0009 0.011 ± 0.0009 0.011 ± 0.0009 0.011 ± 0.0009 0	0.018 = 0.000         0.013 = 0.001         0.013 = 0.001         0.013 = 0.001         0.013 = 0.001         0.013 = 0.001         110 = 4.1         1	0.0419 ± 0.0008	9-1-iF	$0.0217 \pm 0.0009$	0.142 ± 0.018	138.4 ± 5.9	135 ± 17	102.5	0.53	Hi-1-57	+	+1	132.5 ± 4.8	$117 \pm 19$	113.7	0.58
0.0199 ± 0.0009 0.119 ± 0.002 1122 ± 6 1 95 ± 1 123 ± 0 0.45 Hill-1-69 0.0063 ± 0.0021 0.1032 ± 0.003 0.109 ± 0.0009 0.119 ± 0.002 1126 ± 5.5 112 ± 10 0.9 4 0.065 Hill-1-69 0.0063 ± 0.0021 0.103 ± 0.003 0.119 ± 0.003 0.119 ± 0.013 1.123 ± 0.13 1.133 ± 0.13 1.133 ±	0.0198 ± 0.0000 0.0184 ± 0.0017 12.0 ± 5.4 11.0 ± 1.0 19.3 He-1-60 0.0063 ± 0.0012 0.022 ± 0.019 2.2 2.8 ± 3.5 ± 5.0 0.0198 ± 0.0000 0.0194 ± 0.0017 12.0 ± 5.4 11.0 ± 1.0 19.3 He-1-60 0.0063 ± 0.0012 0.022 ± 0.019 1.1 ± 1.2 ± 0.019 1.1 ± 0.019 1.	0.0198 ± 0.0009	Ii-1-7	$0.0419 \pm 0.0018$	$0.313 \pm 0.037$	264.4 ± 11.2	276 ± 32	95.7	0.43	Hi-1-58	+	+	$110.6 \pm 4.1$	$119 \pm 14$	93.1	0.48
0.01998 # 0.00099	0.0198 ± 0.0000 0.10.1 ± 0.0021 12.6.5 ± 5.5 13.2 ± 10.0 ±	0.0198 ± 0.0009 0.1147 ± 0.017 1216 ± 5.4 112 ± 16 107.7 0.33 Hf-1-60 0.0052 to 0.0199 to 0.0299 to 0.0199 to 0.0299	1i-1-8	$0.0187 \pm 0.0010$	$0.098 \pm 0.023$		95 ± 22	125.7	0.45	Hi-1-59	*	+1	$273.7 \pm 9.2$	$283 \pm 26$	1.96	0.5
0.0195 # 0.0099	0.0198 ±0.0000 0.114 ±0.0015 11.78 ±4.53 113 ±2.0 54,1 0.44	0.01999 ± 0.00009 0.140 ± 0.021 12.62 ± 45.5 113 ± 20 95.1 0.41 Hill-1-64 0.00175 ± 0.00009 0.140 ± 0.021 11.23 ± 5.5 112 ± 21 101.9 0.47 Hill-1-64 0.0175 ± 0.00008 0.112 ± 0.017 11.21 ± 4.8 11.01 11.2 ± 2.1 101.9 0.47 Hill-1-64 0.0175 ± 0.0008 0.112 ± 0.017 11.21 ± 4.8 1.01 11.2 ± 2.1 101.9 0.47 Hill-1-64 0.0175 ± 0.0008 0.112 ± 0.017 11.21 ± 4.8 1.07 ± 1.06 0.089 Hill-1-64 0.0189 ± 0.0008 0.112 ± 0.017 11.21 ± 4.8 1.07 ± 1.06 0.089 Hill-1-65 0.0189 ± 0.0008 0.112 ± 0.017 11.21 ± 4.8 1.07 ± 1.06 0.089 Hill-1-69 0.0189 ± 0.0008 0.129 ± 0.007 11.21 ± 4.8 1.07 ± 1.24 ± 1.24 0.07 11.21 ± 4.8 1.07 ± 0.04 1.05 ± 0.0009 0.129 ± 0.016 1.05 ± 0.02 ± 0.000 0.129 ± 0.016 1.17.2 ± 2.3 12.2 ± 1.6 95.4 0.05 Hill-1-69 0.0179 ± 0.0188 ± 0.0009 0.129 ± 0.016 1.17.2 ± 2.3 12.2 ± 1.6 95.4 0.05 Hill-1-73 0.0189 ± 0.019 0.129 ± 0.019 1.15.2 ± 2.3 12.2 ± 1.6 95.4 0.05 Hill-1-73 0.0189 ± 0.010 0.129 ± 0.019 1.15.2 ± 2.3 12.2 ± 1.6 95.4 0.15 0.0189 ± 0.010 0.129 ± 0.010 1.17.2 ± 2.3 12.2 ± 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	6-1-9	$0.0190 \pm 0.0008$	$0.117 \pm 0.017$		$112 \pm 16$	107.7	0.93	Hi-1-60	$0.0625 \pm 0.0021$	#	$391.1 \pm 12.9$	$407 \pm 34$	96.2	6.0
0.0199 ± 0.0009 0.117 ± 0.002 113 ± 4.6 123 ± 19 044 0.65 H1-64 0.0017 0.0189 ± 0.0008 0.124 ± 0.007 124 ± 0.002 113 ± 0.002 1.018 ± 15 1019 0.47 H1-64 0.0018 ± 0.0008 0.124 ± 0.007 0.124 ± 0.002 1.024 ± 0.002 1.	0.0199 ±0.0009 0.117 ±0.022 1143 ± 53. 1123 ± 14 045 046 146 146 00009 0.123 ± 0.0009 0.113 ± 0.0019 1143 ± 53. 1124 ± 15 0105 0.81 H1-65 0.0175 ± 0.0009 0.123 ± 0.000 10.22 ± 45 105 ± 1000 0.0175 ± 0.0009 0.124 ± 0.001 1143 ± 45. 1143 ± 45. 1124 ± 45 1075 ± 0.0019 ± 0.0007 0.101 ± 0.0019 0.0124 ± 0.0019 0.0135 ± 0.0007 0.101 ± 0.0019 0.0135 ± 0.0009 0.135 ± 0.0009 0.013 ± 0.0019 ± 0.0009 0.013 ± 0.0019 0.0135 ± 0.0009 0.013 ± 0.0019 0.0135 ± 0.0009 0.013 ± 0.0019 0.0135 ± 0.0009 0.0135 ± 0.0009 0.0135 ± 0.0009 0.0135 ± 0.0019 0.0135 ±	0.0195 ± 0.0007 0.113 ± 0.015 117.8 ± 4.6 112.8 ± 14 0.45 181-6.7 0.0174 ± 0.0019 0.0179 ± 0.0009 0.117 ± 0.0122 1145.2 ± 5.5 112.8 ± 15 101.9 0.47 181-16.5 0.0185 ± 0.0009 0.117 ± 0.012 114.8 ± 5.5 112.8 ± 16 105.0 0.81 181-16.5 0.0189 ± 0.0175 ± 0.0008 0.111 ± 0.017 112.1 ± 4.8 10.1 112.4 ± 16 105.0 0.81 181-16.5 0.0189 ± 0.0175 ± 0.0008 0.111 ± 0.017 112.1 ± 4.8 10.1 174 ± 16 105.0 0.81 181-16.5 0.0189 ± 0.0018 ± 0.0008 0.111 ± 0.017 112.1 ± 4.8 10.1 124 ± 16 105.0 0.81 181-16.5 0.0189 ± 0.0018 ± 0.0008 0.112 ± 0.017 112.1 ± 4.8 10.1 124 ± 16 105.0 0.81 181-16.9 0.0189 ± 0.0019 0.117 ± 0.0199 ± 0.017 ± 0.0189 ± 0.0008 0.117 ± 0.0199 ± 0.017 ± 0.018 ± 0.0009 0.117 ± 0.0199 ± 0.017 ± 0.019 ± 0.017 ± 0.019 ± 0.017 ± 0.019 ± 0.017 ± 0.019 ±	3-1-10	$0.0198 \pm 0.0009$	$0.140 \pm 0.021$	-11	-11	95.1	0,41	Hi-1-61	+1	+	114.0 ± 4.7	+	114.3	0.46
0.0079	0.0199 ± 0.0000 0.1119 ± 0.022 11   13 ± 5 ± 5   11   13 ± 1   10   10   10   10   10   10   10	0.0199 ± 0.00009 0.117 ± 0.022 1145.2 ± 55. 112 ± 21 101.9 0.47 H1-1-65 0.01054 to 0.0189 ± 0.00008 0.144 ± 0.0017 112.1 ± 4.8 107 ± 16 105.4 0.51 H1-1-64 0.0195 to 0.0186 ± 0.00008 0.114 ± 0.017 112.1 ± 4.8 107 ± 16 105.4 0.81 H1-1-65 0.0186 ± 0.00008 0.130 ± 0.017 ± 0.017 ± 16 0.0187 ± 0.0188 ± 0.00008 0.130 ± 0.017 ± 0.017 ± 16 0.018 ± 0.00008 0.130 ± 0.017 ± 0.017 ± 16 0.018 ± 0.00008 0.130 ± 0.017 ± 0.019 ± 17.2 ± 5.3 18 ± 1.2 ± 0.000 0.017 ± 0.019 ± 0.0000 0.017 ± 0.010 ± 0.0000 0.	11-1-1	$0.0184 \pm 0.0007$	0.131 ± 0.015	-11	125 ± 14	94.4	0.65	Hi-1-62	+1	+8	111.4 ± 5.1	135 ± 22	82.2	1,25
0.0195 ± 0.0008	0.0196 ± 0.0008 0.121 ± 0.017 1 182 ± 5 0.017 1 18 ± 6 0.015 ± 0.0007 0.102 ± 0.0007 1 18 ± 5 1 18 ± 1 18 ± 1 18 ± 1 0.0007 0.019 ± 0.0007 0.102 ± 0.0007 1 18 ± 1 18 ± 1 18 ± 1 0.0007 0.019 ± 0.0007 0.102 ± 0.0007 0.	0.0196 ± 0.00008 0,124 ± 0.017 124.4 ± 5.1 118 ± 16 1054 0,51 H1-1-64 0,0186 ± 0.00008 0,146 ± 0.0027 112.1 ± 4.8 107 ± 16 105.0 0,81 H1-1-64 0,0186 ± 0.00008 0,019 ± 0.0207 ± 0.0208 ± 0.0207 ± 0.0018 ± 0.00008 0,019 ± 0.0207 ± 0.020 ± 0.027 ± 0.0208 ± 0.0019 ± 0.0018 ± 0.00008 0,019 ± 0.020 ± 0.027 ± 0.0018 ± 0.0018 ± 0.00008 0,019 ± 0.020 ± 0.027 ± 0.0018 ± 0.0019 ± 0.0018 ± 0.00008 0,019 ± 0.002 ± 0.	5-1-12	$0.0179 \pm 0.0009$	0.117 ± 0.022	**	+	101.9	0.47	Hi-1-63	4	+	$111.8 \pm 4.9$	$117 \pm 19$	95.2	0.62
0.00188 ± 0.00008 0.14 = 0.022   112.1 ± 4.8   197 ± 16   165.0   04.9   Hi-1-65   0.0169 ± 0.00070   0.132 ± 0.017   0.0175 ± 0.0008   0.017 ± 0.014   10.0 ± 4.9   17.8 ± 1.3   198 ± 2.9   0.24   0.028   Hi-1-67   0.0194 ± 0.0007   0.132 ± 0.018   0.0038 ± 0.0008   0.172 ± 0.014   10.0 ± 4.9   12.4 ± 16   0.56   0.68   Hi-1-69   0.0177 ± 0.0009   0.172 ± 0.014   10.0 ± 4.9   0.027 ± 0.000   0.017 ± 0.014   10.0 ± 4.9   0.0 ± 4.0   0.000   0.	0.0188 ± 0.0008         0.146 ± 0.0008         0.146 ± 0.0009         0.146 ± 0.0009         0.149 ± 0.0009         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.249 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.173 ± 0.0019         0.174	0.0175 ± 0.0008	11-1-13	$0.0196 \pm 0.0008$	$0.124 \pm 0.017$	- 11	118 ± 16	105.4	0.51	Hi-1-64	4	Ħ	$102.0 \pm 4.8$	106 ± 19	96.2	0.44
0.0183 ± 0.0008 0.112 ± 4.5 16 ± 15 0.5 0.8 11.4.4.6 0.017 ± 0.0009 0.112 ± 0.0009 0.139 ± 0.0008 0.139 ± 0.007 1.200 ± 4.9 124 ± 16 96.4 0.66 11.4.68 0.0173 ± 0.0009 0.129 ± 0.017 1.200 ± 4.9 124 ± 16 96.4 0.66 11.4.68 0.0173 ± 0.0009 0.129 ± 0.016 11.79 ± 5.3 124 ± 16 95.4 0.66 11.4.68 0.0173 ± 0.0009 0.129 ± 0.016 11.79 ± 5.3 124 ± 16 95.4 0.65 11.4.68 0.0173 ± 0.0009 0.129 ± 0.016 11.79 ± 5.3 124 ± 1.7 92.3 1.7 11.1.7 0.0127 ± 0.0109 0.129 ± 0.016 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.029 0.129 ± 0.020 0.123 ± 0.029 0.129 ± 0.020 0.123 ± 0.029 0.129 ± 0.020 0.123 ± 0.029 0.129 ± 0.020 0.123 ± 0.029 0.129 ± 0.020 0.123 ± 0.029 0.123 ± 0.029 0.123 ± 0.029 0.123 ± 0.029 0.123 ±	0.0758 ± 0.0008 0.111 ± 0.007 11.11 ± 1.15 10.15 10.15 10.15 10.15 10.008 0.013 ± 0.0009 0.102 ± 0.0009 0.103 ± 0.0017 11.12 ± 4.5 10.15 ± 1.15 0.004 0.007 0.102 ± 0.0019 0.103 ± 0.0019	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	F-1-14	0.0186 ± 0.0008	$0.146 \pm 0.022$		$138 \pm 21$	86.0	0.49	Hi-1-65	- 81	स	118.6 ± 4.7	115 ± 16	102.9	0.41
0.0188 ± 0.0008         0.296 ± 0.026         17.8 ± 5.3         189 ± 24         6.24         0.78         Hi-1-57         0.0194 ± 0.0006         0.123 ± 0.016           0.0188 ± 0.0008         0.130 ± 0.037         1.120 ± 4.9         1.124 ± 16         96.4         0.65         Hi-1-68         0.0173 ± 0.0006         0.123 ± 0.018           0.0254 ± 0.0008         0.177 ± 0.004         1.172 ± 5.3         1.18 ± 6.00         0.172 ± 0.0006         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.018 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.172 ± 0.00         0.173 ± 0.00         0.018 ± 0.00         0.173 ± 0.00         0.173 ± 0.00         0.174 ± 0.00         0.018 ± 0.00         0.174	0.0038 ± 0.0038	$0.0189 \pm 0.0008 \qquad 0.1305 \pm 0.075 \qquad 11728 \pm 5.3 \qquad 189 \pm 24 \qquad 62.4 \qquad 62.8 \qquad 611-67 \qquad 0.0194 \pm 0.0008 \qquad 0.0130 \pm 0.0017 \qquad 1200 \pm 4.9 \qquad 124 \pm 16 \qquad 96.4 \qquad 62.8 \qquad 611-68 \qquad 0.0018 \pm 0.0008 \qquad 0.0130 \pm 0.017 \qquad 1200 \pm 4.9 \qquad 164 \pm 16 \qquad 95.6 \qquad 0.03 \qquad 141-70 \qquad 0.0227 \pm 0.0018 \pm 0.0008 \qquad 0.129 \pm 0.0105 \qquad 115.2 \pm 16 \qquad 95.6 \qquad 0.03 \qquad 141-70 \qquad 0.0227 \pm 0.0018 \pm 0.0009 \qquad 0.129 \pm 0.0105 \qquad 145.8 \pm 5.8 \qquad 151.2 \pm 16 \qquad 95.8 \qquad 0.03 \qquad 141-70 \qquad 0.0227 \pm 0.0018 \pm 0.0018 \qquad 1.0018 \pm 0.0019 \qquad 0.0018 \pm 0.0018 \qquad 1.0018 \pm 0.0019 \qquad 0.0018 \pm 0.0018 \qquad 1.0018 \pm 0.0019 \qquad 0.0018 \pm 0.0019 \qquad 0.0018 \pm 0.0019 \qquad 0.0018 \pm 0.0019 \qquad 0.0018 \pm 0.0019 \qquad 0.0019 \pm 0.002 \qquad 1.0018 \pm 0.0019 \qquad 0.0019 \pm 0.002 \qquad 0.0019 \pm 0.0019 \qquad 0.0019 \pm 0.002 \qquad 0$	ii-1-15	$0.0175 \pm 0.0008$	0.111 ± 0.017	141	107 ± 16	105.0	0.81	Hi-1-66	+	++	182.5 ± 5.8	+	81.0	0.45
0.0353 ± 0.0008 0.139 ± 0.007 1210.0 ± 49 124 ± 16 96.4 0.65 Hi-l-80 0.0473 ± 0.0006 0.135 ± 0.016 0.0354 ± 0.0009 0.137 ± 0.0016 1.179 ± 5.5 16.4 ± 13 ± 16 91.6 0.31 Hi-l-77 0.0227 ± 0.0016 0.135 ± 0.016 0.035 ± 0.0006 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0016 0.135 ± 0.0017 0.135 ± 0.0016 0.135 ± 0.0017 0.135 ± 0.0	0.0254 ± 0.0008	0.0188 ± 0.0008         0.130 ± 0.017         1.200 ± 49         124 ± 16         96.4         0.65         Hi-1-68         0.0173           0.0185 ± 0.0008         0.137 ± 0.016         1.15.0 ± 5.3         16.5 ± 15         97.6         0.60         Hi-1-69         0.4179 ± 0.019           0.0185 ± 0.0008         0.235 ± 0.019         1.039 ± 0.016         1.15.8 ± 5.8         1.25 ± 17         97.6         0.60         Hi-1-71         0.0227 ± 0.019           0.0234 ± 0.0109         4.235 ± 0.035         1.65 ± 5.8         1.95 ± 77         92.3         0.41         Hi-1-72         0.0178 ± 0.019           0.0234 ± 0.0109         0.197 ± 0.028         1.86 ± 6.9         1.84 ± 6.9         1.84 ± 6.9         1.84 ± 7.7         0.0178 ± 0.019           0.0174 ± 0.0009         0.110 ± 0.021         1.115 ± 5.7         1.84 ± 6.9         1.84 ± 4.1         0.0178 ± 0.019         0.0178 ± 0.000         0.0179 ± 0.011         1.84 ± 4.1         1.00.8         0.83         Hi-1-74         0.0182 ± 0.019         0.0178 ± 0.022         1.84 ± 4.1         1.77 ± 10         0.75         Hi-1-74         0.0182 ± 0.019         0.0178 ± 0.022         1.84 ± 4.2         1.85 ± 2.9         8.35         0.40         Hi-1-74         0.0182 ± 0.019         0.0178 ± 0.022         1.84 ± 4.1         1.72	91-1-16	0.0184 ± 0.0008	0.205 ± 0.026			62.4	0.78	Hi-1-67	-11	+	123.7 ± 4.8	126 ± 18	5'86	0.48
0.0254 ± 0.0000 0.117 ± 0.014   161.6 ± 5.5   166 ± 13   97.6   0.60   H5-1-60   0.4179 ± 0.0116   8.973 ± 0.322   0.4181 ± 0.0000   0.129 ± 0.016   11.5 ± 5.8   123 ± 17   93.5   0.4181 ± 0.0000   0.236 ± 0.039   H5-1-73   0.0185 ± 0.0000   0.128 ± 0.013   0.0254 ± 0.0010   4.111 ± 0.188   17.74 ± 5.6   16.5 ± 17   91.5   95.5   94.5   H5-1-73   0.0185 ± 0.0000   0.128 ± 0.013   0.0254 ± 0.0010   4.111 ± 0.188   17.74 ± 5.6   16.5 ± 17   91.5   95.5   94.5   H5-1-73   0.0185 ± 0.0000   0.128 ± 0.013   0.0254 ± 0.0000   0.129 ± 0.012   0.0174 ± 0.0000   0.129 ± 0.023   11.2 ± 5.7   11.5 ± 2.0   1	0.0254 ± 0.0010 0.177 ± 0.0044   61.16 ± 6.5   166 ± 16   9.56   0.64   Hi-l-70   0.4179 ± 0.0016   0.2254 ± 0.0009   0.127 ± 0.0010   0.177 ± 0.0049   0.125 ± 0.0016   11.19 ± 5.8   125 ± 15   9.56   0.31   Hi-l-77   0.0252 ± 0.0009   0.125 ± 0.001   11.15 ± 1.2   0.2554 ± 0.0010   0.125 ± 0.001   11.2 ± 1.2   0.2554 ± 0.0010   0.125 ± 0.001   11.2 ± 1.2   0.2554 ± 0.0010   0.127 ± 0.0010   0.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-17	$0.0188 \pm 0.0008$	$0.130 \pm 0.017$		$124 \pm 16$	96.4	0.65	Hi-1-68	#	+	$110.3 \pm 4.2$		0.06	0.47
0.0185 ± 0.0000 0.236 ± 0.036 1179 ± 53 123 ± 16 956 0.31 Hi-77 0.0229 ± 0.0000 0.236 ± 0.019 0.0237 ± 0.036 0.031 Hi-77 0.0239 ± 0.0000 0.236 ± 0.036 0.031 Hi-77 0.0178 ± 0.0000 0.128 ± 0.013 0.0324 ± 0.0100 0.0234 ± 0.035 156.2 ± 56 165 ± 733 0.43 Hi-77 0.0178 ± 0.0006 0.128 ± 0.011 0.0128 ± 0.010 0.0234 ± 0.0100 0.129 ± 0.020 0.0304 ± 0.011 0.197 ± 0.025 1.022 ± 0.020 0.0324 ± 0.011 0.197 ± 0.025 1.022 ± 0.020 0.0324 ± 0.0010 0.129 ± 0.020 0.0324 ± 0.0010 0.129 ± 0.020 0.0324 ± 0.0010 0.129 ± 0.022 0.0324 ± 0.0010 0.129 ± 0.022 0.120 ± 0.020 0.0324 ± 0.0010 0.129 ± 0.022 0.120 ± 0.022 0.0324 ± 0.0010 0.129 ± 0.022 0.120 ± 0.022 0.0324 ± 0.0010 0.120 ± 0.022 0.120 ± 0.022 0.0324 ± 0.0010 0.120 ± 0.022 0.120 ± 0.022 0.0324 ± 0.0010 0.120 ± 0.022 0.120 ± 0.022 0.0324 ± 0.0010 0.120 ± 0.022 0.120 ± 0.022 0.0324 ± 0.0010 0.120 ± 0.022 0.120 ± 0.022 0.0324 ± 0.0000 0.120 ± 0.011 ± 0.011 ± 0.011 1.022 ± 0.022	0.00183 ± 0.0008	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3-1-18	$0.0254 \pm 0.0010$	$0.177 \pm 0.014$	-#	166 ± 13	97.6	09.0	Hi-1-69	4	+	$2250.8 \pm 62.6$		96.4	0.48
0.2354 ± 0.009         0.1356 ± 0.639         115.8 ± 5.8         215 ± 27         53.8         0.35         Hh-173         0.0178 ± 0.0000         0.198 ± 0.000           0.2554 ± 0.0103         4.111 ± 0.188         157.1 ± 5.8         1656 ± 77         9.16         0.89         Hh-174         0.0178 ± 0.000         0.117 ± 0.011           0.2554 ± 0.0101         4.111 ± 0.188         157.1 ± 5.9         15.3         0.49         Hh-174         0.0182 ± 0.0000         0.117 ± 0.018           0.0254 ± 0.0010         4.111 ± 0.188         15.7         15.2         0.45         Hh-174         0.0182 ± 0.0000         0.177 ± 0.018           0.0174 ± 0.0009         0.129 ± 0.020         111.2 ± 5.7         118 ± 20         75.3         0.40         Hh-1.75         0.0170 ± 0.0000         0.175 ± 0.0009         0.175 ± 0.0009         0.175 ± 0.0009         0.175 ± 0.0009         0.175 ± 0.0009         0.175 ± 0.0009         0.175 ± 0.0009         0.0170 ± 0.0009         0.175 ± 0.0009         0.0170 ± 0.0009         0.175 ± 0.0009         0.0170 ± 0.0009         0.175 ± 0.0018         0.0259 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009         0.0170 ± 0.0009 <td< td=""><td>0.0248 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.000         0.138 ± 0.000         0.138 ± 0.001         <th< td=""><td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td><td>61-1-1</td><td><math>0.0185 \pm 0.0008</math></td><td><math>0.129 \pm 0.016</math></td><td>-11</td><td>123 ± 16</td><td>95.6</td><td>0.31</td><td>Hi-1-70</td><td>-91</td><td>4</td><td>144.8 ± 4.9</td><td></td><td>6.69</td><td>0.55</td></th<></td></td<>	0.0248 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.0009         0.138 ± 0.000         0.138 ± 0.000         0.138 ± 0.001 <th< td=""><td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td><td>61-1-1</td><td><math>0.0185 \pm 0.0008</math></td><td><math>0.129 \pm 0.016</math></td><td>-11</td><td>123 ± 16</td><td>95.6</td><td>0.31</td><td>Hi-1-70</td><td>-91</td><td>4</td><td>144.8 ± 4.9</td><td></td><td>6.69</td><td>0.55</td></th<>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	61-1-1	$0.0185 \pm 0.0008$	$0.129 \pm 0.016$	-11	123 ± 16	95.6	0.31	Hi-1-70	-91	4	144.8 ± 4.9		6.69	0.55
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0254 ± 0.0103 4,1929 ± 0.195   156.2 ± 173 0,195   11.75 0,0018 ± 0.0006 0,117 ± 0.011   1076 ± 5.3 0,12 ± 1.2 0,00254 ± 0.0010 0,120 ± 0.0224 ± 0.0101   10.75 ± 5.3 0,40   11.12 ± 1.7 0,0018 ± 0.0007   0.117 ± 0.011   10.75 ± 1.2 1,12 ± 1.1 0,00254 ± 0.0007   0.129 ± 0.025   130.2 ± 0.2 1,12 ± 1.2 0,221 ± 1.0 0,000 0,120 ± 0.020   11.12 ± 5.7 1,15 ± 2.0 0,42   11.12 ± 5.0 0,42   11.12 ± 5.0 0,42   11.12 ± 5.0 0,42   11.12 ± 1.2 0,42   11.12 ±	0.2554 ± 0.0103	1-1-20	$0.0181 \pm 0.0009$	$0.236 \pm 0.030$	+1	$215 \pm 27$	53.8	0.35	Hr-1-71	+1	#	146.2 ± 6.0	+	80.6	0.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.02554 ± 0.0100	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	F1-21	$0.2742 \pm 0.0103$	4.293 ± 0.195	1562.1 ± 58.6	1692 ± 77	92.3	0.41	Hi-1-72	4	$0.128 \pm 0.013$	113,5 ± 3,9		93.2	0,56
0.0254 ± 0.0011         0.235 ± 0.0021         0.024 ± 0.0005         0.12 ± 0.018         0.12 ± 0.018           0.0244 ± 0.0010         0.132 ± 0.025         13.02 ± 0.02         18.3 ± 2.3         71.2         6.75         HE1-75         0.0170 ± 0.0000         0.173 ± 0.018           0.0244 ± 0.0000         0.192 ± 0.0025         13.2 ± 0.2         83.5         0.48         HE1-77         0.0170 ± 0.0000         0.159 ± 0.017           0.0240 ± 0.0000         0.143 ± 0.033         13.2 ± 2.2         83.5         0.48         HE1-77         0.0170 ± 0.0000         0.159 ± 0.017           0.0240 ± 0.0007         0.178 ± 0.015         16.7 ± 4.3         16.6 ± 1.4         99.7         0.68         HE1-78         0.0295 ± 0.000         0.153 ± 0.019           0.0281 ± 0.0007         0.178 ± 0.015         16.7 ± 4.3         16.6 ± 1.4         99.7         0.68         HE1-78         0.0400         0.153 ± 0.019           0.0281 ± 0.0007         0.178 ± 0.0018         1.030 ± 0.018         1.0018         1.0018         0.029         0.019         0.019         0.019           0.0281 ± 0.0007         0.178 ± 0.0009         0.178 ± 0.009         0.178 ± 0.009         0.159 ± 0.019         0.019         0.019         0.015         0.015         0.015         0.019         0.00	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0253 ± 0.0011         0.235 ± 0.025 $I6IA \pm 6.9$ $I3IA \pm 2.0$ $I3A \pm 2.0$ $I3A \pm 3.0$ </td <td>1-1-22</td> <td><math>0.2654 \pm 0.0100</math></td> <td><math>4.111 \pm 0.188</math></td> <td>1517.4 ± 56.9</td> <td>1656 ± 76</td> <td>916</td> <td>68.0</td> <td>Hi-1-73</td> <td>+</td> <td><math>0.117 \pm 0.011</math></td> <td><math>107.6 \pm 3.5</math></td> <td><math>112 \pm 11</math></td> <td>8.56</td> <td>1.05</td>	1-1-22	$0.2654 \pm 0.0100$	$4.111 \pm 0.188$	1517.4 ± 56.9	1656 ± 76	916	68.0	Hi-1-73	+	$0.117 \pm 0.011$	$107.6 \pm 3.5$	$112 \pm 11$	8.56	1.05
0.0173 ± 0.0010 0.197 ± 0.023   130.2 ± 6.2   115 ± 20   95.8   0.82   Hi-1-75   0.0251 ± 0.0009   0.115 ± 0.021   0.0174 ± 0.0009   0.113 ± 4.023   111.2 ± 5.7   115 ± 2.0   95.8   0.82   Hi-1-75   0.0170 ± 0.0006   0.155 ± 0.0170   0.0170 ± 0.0009   0.143 ± 0.023   113.4 ± 5.9   135 ± 4.2   155 ± 4.2   100.8   0.83   Hi-1-78   0.0170 ± 0.0009   0.153 ± 0.018   0.0281 ± 0.0007   0.178 ± 0.013   113.4 ± 4.4   177 ± 10   100.6   0.72   Hi-1-79   0.0170 ± 0.0009   0.123 ± 0.018   0.0280 ± 0.0007   0.178 ± 0.013   173.2 ± 4.2   155 ± 1   100.6   0.72   Hi-1-79   0.0297 ± 0.0008   0.123 ± 0.018   0.0280 ± 0.0007   0.178 ± 0.019   0.0189 ± 0.0017   0.178 ± 0.001   0.0189 ± 0.0007   0.178 ± 0.013   117.3 ± 3.4   117 ± 12   100.5   0.82   Hi-1-81   0.0209 ± 0.0007   0.122 ± 0.013   117.3 ± 3.4   117 ± 12   100.5   0.82   Hi-1-81   0.0290 ± 0.0007   0.158 ± 0.019   0.0189 ± 0.0006   0.121 ± 0.015   118.7 ± 3.8   118 ± 15   0.082   Hi-1-84   0.0187 ± 0.0007   0.128 ± 0.019   0.0189 ± 0.0006   0.121 ± 0.015   115.0 ± 3.7   118 ± 15   0.05   Hi-1-84   0.0187 ± 0.0009   0.0189 ± 0.0000   0.0121 ± 0.015   120.7 ± 3.5   118 ± 15   0.05   Hi-1-84   0.0187 ± 0.0009   0.0189 ± 0.0000   0.0121 ± 0.015   0.0280 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0281 ± 0.0000   0.0291 ± 0.00	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0204 ± 0.0001         0.197 ± 0.025         130.2 ± 6.2         183 ± 23         71.2         0.75         Hi-1-76         0.0251 ± 0.025           0.0174 ± 0.0009         0.120 ± 0.020         111.2 ± 5.7         115 ± 20         96.8         0.82         Hi-1-76         0.0170 ± 0.0170           0.0174 ± 0.0009         0.131 ± 0.012         153.2 ± 42         152 ± 14         100.8         0.83         Hi-1-76         0.0170 ± 0.0170           0.0240 ± 0.0007         0.161 ± 0.015         165.2 ± 42         152.2 ± 14         100.8         0.83         Hi-1-78         0.0355 ± 0.019           0.0250 ± 0.0007         0.178 ± 0.015         165.7 ± 43         166 ± 14         90.7         0.68         Hi-1-80         0.0209 ± 0.0209           0.0184 ± 0.0005         0.178 ± 0.013         117.3 ± 3.4         117 ± 12         100.5         0.82         Hi-1-87         0.0209 ± 0.0209           0.0184 ± 0.0005         0.122 ± 0.016         116.7 ± 3.8         117 ± 12         100.5         0.82         Hi-1-87         0.0209 ± 0.0209           0.0185 ± 0.0006         0.122 ± 0.016         116.7 ± 3.8         116 ± 14         98.7         0.64         Hi-1-87         0.0169 ± 0.0209           0.0189 ± 0.0000         0.122 ± 0.016         115.7 ± 3.8         116 ± 14<	1-1-23	$0.0253 \pm 0.0011$	$0.235 \pm 0.022$	161.4 ± 6.9.	214 ± 20	75.3	0.40	Hi-1-74	+1	$0.127 \pm 0.018$	116.3 ± 4.5	121 ± 17	6.56	9.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0777 ± 0.0009 0.129 ± 0.020 1112 ± 5.7 115 ± 2.9 0.88 Hil-75 0.0177 ± 0.0006 0.156 ± 0.007 112 ± 5.7 115 ± 5.7 115 ± 5.9 0.88 Hil-75 0.0177 ± 0.0006 0.159 ± 0.007 129 ± 1.0 100.00 0.0204 ± 0.0007 0.151 ± 0.013 112 ± 5.7 122 ± 4.3 100.88 0.83 Hil-75 0.0209 ± 0.0008 0.232 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0294 ± 0.009 0.0299 ± 0.009 0.0399 ± 0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-24	0.0204 ± 0.0010	$0.197 \pm 0.025$	130,2 ± 6,2	$183 \pm 23$	71.2	0.75	Hi-1-75	.41	$\overline{H}$	159.6 ± 5.8	164 ± 20	97.4	0.59
$0.0277 \pm 0.0009 \qquad 0.143 \pm 0.023 \qquad 113.4 \pm 3.9 \qquad 13.6 \pm 2.2 \qquad 83.5 \qquad 0.48 \qquad Hil-77 \qquad 0.0196 \pm 0.0006 \qquad 0.159 \pm 0.019 \qquad 0.0181 \pm 0.0023 \qquad 113.4 \pm 3.9 \qquad 13.6 \pm 2.2 \qquad 83.5 \qquad 0.48 \qquad Hil-77 \qquad 0.0196 \pm 0.0006 \qquad 0.159 \pm 0.019 \qquad 0.0231 \pm 0.018 \qquad 0.0231 \pm 0.018 \qquad 0.0232 \pm 0.018 \qquad 0.018 \pm 0.0006 \qquad 0.123 \pm 0.013 \qquad 117.3 \pm 3.4 \qquad 117.2 \pm 1.2 \qquad 0.048 \qquad 11184 \qquad 0.0232 \pm 0.019 \qquad 0.0219 \pm 0.010 \qquad 0.0232 \pm 0.019 \qquad 0.0242 \pm 0.0019 \qquad 0.$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	i-1-25	$0.0174 \pm 0.0009$	0.120 ± 0.020		$115 \pm 20$	8.96	0.82	Hi-1-76	44	++	108.7 ± 3.6	129 ± 16	84.0	0.69
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0240 ± 0.0007         0.161 ± 0.015         153.2 ± 4.2         152.2 ± 14.2         100.8         0.83         Hi-1-78         0.3656 ± 0.0078         7.337 ± 0.209         200.99 ± 43.0         0.153 ± 0.209         200.99 ± 43.0         0.0259 ± 4.000         0.0294 ± 0.000         0.018 ± 0.001         0.018 ± 0.001         0.0295 ± 4.000         0.0297 ± 0.009         0.0297 ± 0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-36		$0.143 \pm 0.023$		$136 \pm 22$	83.5	0.48	Hi-1-77	+4	+	124.9 ± 4.1	150 ± 18	83.4	0.34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-27	$0.0240 \pm 0.0007$	0.161 ± 0.015		$152 \pm 14$	100.8	0.83	Hi-1-78	41	#	$2008.9 \pm 43.0$	$2153 \pm 61$	93.3	0.46
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	i-1-28	$0.0281 \pm 0.0006$	$0.191 \pm 0.011$		$177 \pm 10$	100.6	0.72	Hi-1-79	++	+1	$188.7 \pm 5.1$	$204 \pm 17$	92.4	0.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-29	$0.0260 \pm 0.0007$	$0.178 \pm 0.015$	44	166 ± 14	7.66	89.0	Hi-1-80	41	#	256.2 ± 7.1	303 ± 25	84.6	0.69
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-1-30	$0.0185 \pm 0.0007$	$0.099 \pm 0.018$	118.0 ± 4.6	$2I \mp 96$	122.7	0.56	H6-1-81	#	+	$133.6 \pm 4.8$	147 ± 21	912	0.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-31	$0.0184 \pm 0.0005$	$0.122 \pm 0.013$		$117 \pm 12$	100.5	0.82	Hi-1-82	+1	+1	$107.0 \pm 3.9$	132 ± 18	81.3	1.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-32	0.0186 ± 0.0006	$0.150 \pm 0.015$	118.5 ± 3.6	142 ± 14	83.7	0.44	Hi-1-83	+1	#	117.8 ± 4.3	$418 \pm 35$	28.2	9'0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-33	$0.0183 \pm 0.0006$	$0.123 \pm 0.016$	$116.7 \pm 3.8$	118 ± 15	8.86	0.62	Hi-1-84	#	+1.	1752,4 ± 45,4	$1784 \pm 62$	98.2	0.15
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-34	$0.0189 \pm 0.0005$	0.128 ± 0.013		122 ± 12	7.86	99.0	Hi-1-85	40	+1	179.7 ± 6.1	308 ± 27	58.3	0.63
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-35	$0.0180 \pm 0.0006$	$0.121 \pm 0.015$		116 ± 14	6.86	0.59	Hi-1-86	44	#	156.0 ± 5.5	223 ± 24	6.69	0.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-36	$0.0368 \pm 0.0013$	$0.268 \pm 0.040$		241 ± 36	7.96	0.53	Hi-1-87	#	+	$453.5 \pm 14.1$	497 ± 41	91.2	0.74
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-37		$0.285 \pm 0.046$		255 ± 41	57.4	0.75	Hi-1-88	#	-11	191.8 ± 7.9		62.8	0.82
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-38		$0.300 \pm 0.032$		267 ± 29	64.6	0.50	Hi-1-89	#	+1	$144.6 \pm 5.9$		98.4	0.63
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-39	$0.3341 \pm 0.0076$	$6.370 \pm 0.242$		2028 ± 77	91.6	95.0	Hi-1-90	#	+	125.5 ± 4.0		83.2	0.92
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	05-1-1	$0.0201 \pm 0.0007$	$0.219 \pm 0.023$		$201 \pm 21$	63.8	0.65	Hi-1-91	#	#	$115.6 \pm 4.3$		92.1	0.83
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1p-I-1	$0.0195 \pm 0.0010$	$0.146 \pm 0.030$		$138 \pm 29$	8.68	0.54	Hi-1-92	+	4.	$120.4 \pm 5.5$	$132 \pm 23$	91.4	0.4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	i-1-42	$0.0178 \pm 0.0008$	$0.109 \pm 0.022$	#	$105 \pm 21$	9'201	0.48	Hi-1-93	+1	#	$266.2 \pm 11.4$	+	101.2	0.55
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-43	$0.0204 \pm 0.0008$	$0.132 \pm 0.021$	#	126 ± 20	103.5	89.0	Hi-1-94	+	#	$113.0 \pm 4.7$		65.7	0.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$0.0301 \pm 0.0010 \qquad 0.0209 \pm 0.020 \qquad 191.3 \pm 6.1 \qquad 193 \pm 18 \qquad 99.1 \qquad 0.49 \qquad Hi-1-96 \qquad 0.0175 \pm 0.0008 \qquad 0.201 \pm 0.029 \qquad 112.1 \pm 5.2 \qquad 186 \pm 26$ $0.0205 \pm 0.0010 \qquad 0.176 \pm 0.031 \qquad 131.0 \pm 6.1 \qquad 164 \pm 29 \qquad 79.8 \qquad 0.43 \qquad Hi-1-97 \qquad 0.0175 \pm 0.0008 \qquad 0.163 \pm 0.028 \qquad 111.7 \pm 5.4 \qquad 154 \pm 27$ $0.0183 \pm 0.0007 \qquad 0.147 \pm 0.017 \qquad 117.0 \pm 4.2 \qquad 139 \pm 16 \qquad 84.2 \qquad 0.45 \qquad 141.1-98 \qquad 0.0177 \pm 0.0005 \qquad 0.111 \pm 0.011 \qquad 113.2 \pm 3.0 \qquad 107 \pm 10 \qquad 107 \pm 17 \qquad 107 \qquad 107 \pm 17 \qquad 107 \pm 17 \qquad 107 + 17 \qquad 107 + 17 \qquad 107 \qquad 107 \pm 17 $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-44	$0.0179 \pm 0.0007$	$0.114 \pm 0.018$	#	$110 \pm 17$	104.1	0.80	Hi-1-95	+	#	115.7 ± 4.9		98.2	0.48
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$0.0205 \pm 0.0010 \qquad 0.176 \pm 0.031 \qquad 131.0 \pm 6.1 \qquad 164 \pm 29 \qquad 79.8 \qquad 0.53 \qquad Hi-1-97 \qquad 0.0175 \pm 0.0008 \qquad 0.163 \pm 0.028 \qquad 111.7 \pm 5.4 \qquad 154 \pm 27 \qquad 0.0183 \pm 0.0007 \qquad 0.147 \pm 0.017 \qquad 117.0 \pm 4.2 \qquad 139 \pm 16 \qquad 84.2 \qquad 0.52 \qquad \text{Hi-1-98} \qquad 0.0177 \pm 0.0005 \qquad 0.111 \pm 0.011 \qquad 113.2 \pm 3.0 \qquad 107 \pm 10 \qquad 107 \pm 10 \qquad 0.0176 \pm 0.0007 \qquad 0.118 \pm 0.017 \qquad 112.7 \pm 4.2 \qquad 114 \pm 16 \qquad 89.0 \qquad 0.73 \qquad Hi-1-99 \qquad 0.0194 \pm 0.0006 \qquad 0.191 \pm 0.016 \qquad 112.5 \pm 4.2 \qquad 114 \pm 16 \qquad 99.0 \qquad 0.73 \qquad Hi-1-100 \qquad 0.0271 \pm 0.0005 \qquad 0.212 \pm 0.016 \qquad 172.4 \pm 4.2 \qquad 195 \pm 14 \qquad 0.018 \pm 0.007 \qquad 0.018 \pm 0.010 \qquad 112.5 \pm 4.2 \qquad 114 \pm 10 \qquad 0.018 \pm 0.0007 \qquad 0.018 \pm 0.010 \qquad 112.5 \pm 4.2 \qquad 114 \pm 10 \qquad 0.018 \pm 0.0007 \qquad 0.0191 \pm 0.019 \qquad 0.0191 \pm 0.0010 \qquad 0.0191 \pm 0.0010 \qquad 0.0191 \pm 0.0191 \qquad 0.0181 \qquad 0.0181 \pm 0.0191 \qquad 0.0181 \pm 0.0191 \qquad 0.0181 \pm 0.0191 \qquad 0.0181 + 0.0191 \qquad 0.0181 \pm 0.0$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-45	$0.0301 \pm 0.0010$	0.209 ± 0.020	34	$193 \pm 18$	99.1	0.49	96-1-11	#	41	112.1 ±-5.2		4.09	0.62
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	F-1-46	$0.0205 \pm 0.0010$	$0.176 \pm 0.031$			8.62	0.53	Hi-1-97	+	+	$111.7 \pm 5.4$		72.8	0.6
0.0175 ± 0.0007 0.135 ± 0.017 1122 ± 4.42 129 ± 16 88.4 0.87 H-1-1-99 0.0194 ± 0.0006 0.141 ± 0.016 1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$0.0176 \pm 0.0007$ $0.135 \pm 0.017$ $112.7 \pm 4.2$ $129 \pm 16$ $87.4$ $0.87$ Hi-1-99 $0.0194 \pm 0.0176 \pm 0.0007$ $0.118 \pm 0.016$ $112.5 \pm 4.2$ $114 \pm 16$ $99.0$ $0.73$ $Hi-1-100$ $0.0271 \pm 0.0271 \pm 0.0180 \pm 0.0007$ $0.120 \pm 0.020$ $115.0 \pm 4.5$ $115 \pm 19$ $100.3$ $0.40$ $Hi-1-101$ $0.0186 \pm 0.0180$	1-1-47	0,0183 ± 0.0007	$0.147 \pm 0.017$	100		84.2	0.52	Hi-1-98	-91	#	$113.2 \pm 3.0$		106.0	0,76
CATHE CANADA CATE CALL AND THE LAST THE LAST CALL CALL CALL CALL CALL CALL CALL CAL	$0.0176 \pm 0.0007$ $0.118 \pm 0.016$ $112.5 \pm 4.2$ $114 \pm 16$ $99.0$ $0.73$ $Hi.J.100$ $0.0271 \pm 0.0007$ $0.212 \pm 0.016$ $172.4 \pm 4.2$ $195 \pm 14$ $0.0188 \pm 0.0007$ $0.130 \pm 0.020$ $1150 \pm 0.05$ $115 \pm 10$ $100.3$ $0.40$ $Hi.J.101$ $0.0188 \pm 0.0005$ $0.141 \pm 0.014$ $1185 \pm 3.3$ $134 \pm 13$	0.0176 $\pm$ 0.0007 0.118 $\pm$ 0.016 112.5 $\pm$ 4.2 114 $\pm$ 16 99.0 0.73 $\pm$ 16.1-100 0.0271 $\pm$ 0.0180 $\pm$ 0.0007 0.120 $\pm$ 0.020 115.0 $\pm$ 4.5 115 $\pm$ 19 100.3 0.40 $\pm$ 16.1-101 0.0186 $\pm$	1-1-48	$0.0176 \pm 0.0007$	$0.135 \pm 0.017$	41	$129 \pm 16$	87.4	0.87	Hi-1-99	#	+1	$124.1 \pm 3.7$		92.9	0.73
$0.0176 \pm 0.0007$ $0.118 \pm 0.016$ $112.5 \pm 4.2$ $114 \pm 16$ $99.0$ $0.73$ $16.4-100$ $0.0271 \pm 0.0007$ $0.212 \pm 0.016$	0.0180 + 0.0007 0.190 + 0.00 1150 + 45 115 + 19 100 3 0.40 HILLIO 0.0186 + 0.0005 0.141 + 0.014 1185 + 3.3 134 + 13	$0.0180 \pm 0.0007$ $0.120 \pm 0.020$ $115.0 \pm 4.5$ $115 \pm 19$ $100.3$ $0.40$ $HeJ-10I$ $0.0186 \pm 0.0180$	1-1-49	$0.0176 \pm 0.0007$	$0.118 \pm 0.016$	+	$114 \pm 16$	0.66	0.73	Hi-1-100	46	#	172.4 ± 4.2		88.2	0.40

0.0058 ± 0.0070 0.131 ± 0.007 0.131 ± 1.0 2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2		1188 ± 0.0007 1764 ± 0.0004 1266 ± 0.0006 1171 ± 0.0005 3013 ± 0.0058	D <sub>552</sub> /9d <sub>105</sub>	(Ma)	W.Pb/ess U age (Ma)	%conc	Th/U	Grain	D867/9dd902	207Pb/235U	(Ma)	(Ma)	%cone	Th/U
0.0054 ± 0.0040         0.155 ± 0.0040         0.105 ± 0.0040         0.155		$1.164 \pm 0.0004$ $1266 \pm 0.0006$ $1171 \pm 0.0005$ $3013 \pm 0.0058$ $1294 \pm 0.0014$	0.131 ± 0.019	119,9 ± 4,3	125 ± 18	5.96	0.41	Hi-1-153	0.0185 ± 0.0006	$0.136 \pm 0.012$	118,0 ± 4.1	129 ± 11	91.2	0.64
0.0015 = 0.0005		)266 ± 0.0006 )171 ± 0.0005 3013 ± 0.0058 )294 ± 0.0014	0.124 ± 0.010	104.6 ± 2.6	119 ± 9	88.2	0.00	Hi-1-154	$0.0208 \pm 0.0008$	$0.152 \pm 0.016$	$132.6 \pm 4.9$	144 ± 15	92.3	6.0
0.00171 ± 0.00005		$1171 \pm 0.0005$ $3013 \pm 0.0058$ $1294 \pm 0.0014$	$0.196 \pm 0.013$	$169.2 \pm 3.9$	182 ± 12	93.2	0.50							
0.0313 ± 0.0009		5013 ± 0.0058 7294 ± 0.0014	$0.115 \pm 0.013$	109.0 ± 3.1	111 ± 12	98.5	68.0	Sand	stone of the lower part	10	ion (Bi-1; 33" 38" 5	4	\$2.38" E)	
0.0079 ± 0.0070		1294 ± 0.0014	$4.735 \pm 0.148$	1697.9 ± 32.4	1773 ± 55	95.7	0.16	Bi-1-1	$0.0426 \pm 0.0010$	$0.332 \pm 0.031$	$269.2 \pm 6.5$	291 ± 27	92.5	0.51
0.079 = 0.079         0.079 = 0.079         0.070         0.070         0.070         0.070         0.070         0.070         0.070         0.070         0.071         0.071         0.071         0.071         0.071         0.071         0.071         0.071         0.071         0.071         0.072         0.073         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072         0.072<			$0.615 \pm 0.064$	186.8 ± 9.1	$487 \pm 51$	38.4	0,52	Bi-1-2	$0.0264 \pm 0.0005$	$0.180 \pm 0.013$	$168.1 \pm 3.2$	$168 \pm 12$	100.1	1,11
0.0029 ± 0.0070 0.159 ± 0.017 185.0 ± 75 181 ± 16 0.20 0.04 bit-14 0.0002 ± 0.0009 0.245 ± 0.017 ± 0.0009 0.159 ± 0.017 185.0 ± 0.04 ± 0.000 0.159 ± 0.017 185.0 ± 0.04 ± 0.000 0.159 ± 0.0001 0.151 ± 0.017 185.0 ± 0.000 0.151 ±		190 ± 0.0009	$0.155 \pm 0.023$	121.5 ± 6.0	146 ± 22	83.0	0.37	Bi-1-3	$0.0301 \pm 0.0006$	+	191,5 ± 3.7	$203 \pm 14$	94.2	0.4
0.023 ± 0.001		1185 ± 0.0008	$0.139 \pm 0.014$	$118.2 \pm 5.0$	$133 \pm 13$	89.2	69.0	Bi-1-4	++	+	1692.2 ± 22.7	1756 ± 52	96.4	0.3
0.0224 0.0000 0.1154 0.021		$9291 \pm 0.0012$	$0.196 \pm 0.017$	185.0 ± 7.5	181 ± 16	102.0	0.37	Bi-1-5	-11	#	209.7 ± 5.6	$301 \pm 28$	9.69	0.8
0.0277 ± 0.0070 0.113 ± 0.007 0.113 ± 0.013 1 104.5 0.147 0.0232 ± 0.0000 0.103 ± 0.017 1 ± 0.007 0.113 ± 0.007 0.		1272 ± 0.0011	$0.213 \pm 0.018$	172.8 ± 7.0		88.1	0.56	9-1-18	-94	#	267.1 ± 5.3	$308 \pm 20$	86.7	0.9
0.0127 ± 0.0012 0.1515 ± 0.002 1 150 ± 15 9.7 0.2 0.2 0.2 0.2 0.0 0.2 0.2 0.0 0.0 0.2 0.0 0.0		$9171 \pm 0.0009$	$0.113 \pm 0.021$	$109.4 \pm 5.9$	$108 \pm 20$	100.9	0.57	Bi-1-7	-#	+	$207.3 \pm 5.9$	$217 \pm 19$	7.56	0.9
0.0193 ± 0.0000         0.115 ± 0.0000         0.115 ± 0.001         1.01 ±		$0.0000 \pm 0.0012$	0.215 ± 0.017		197 ± 16	7.56	0.52	Bi-1-8	+1	-#1	149,9 ± 3.6	154 ± 9	576	0,5
0.0199 ± 0.0001         0.1194 ± 0.0001         0.1194 ± 0.0001         0.1194 ± 0.0001         0.0192 ± 0.0000         0.0192 ± 0		1182 ± 0.0009	0.136 ± 0.019	116.1 ± 5.5	130 ± 18	89.5	0.57	Bi-1-9	4	#	1902.7 ± 42.2	1870 ± 58	101.7	0.7
0.0039 ± 0.0070		0100'0 ± 0610	0.154 ± 0.024	121.1 ± 6.2	145 ± 23	83.4	0.63	Bi-1-10	*	#	172.9 ± 5.0	212 ± 18	81.4	0.0
0.0281 ± 0.0000         0.028 ± 0.0000         1.02.3 ± 8.8         1.04.2         8.6.7         1.0.001 ± 0.0000         4.0.3         1.0.1.1         0.0.001         1.0.1.2         ±5.8.4         1.0.2.3         1.0.1.1         0.0.008         4.0.00         1.0.1.2         1.0.2.3         ±8.0.00         1.0.1.2         1.0.2.3         ±8.0.00         1.0.1.2         ±8.4         1.0.2.3         ±8.0.00         1.0.1.2         ±8.4         1.0.2         1.0.2.2         ±8.0.00         1.0.2.2         ±8.0.00         1.0.2.2         ±8.4         0.0.2         ±8.1.1.8         0.0.29         ±0.00.1         1.0.1.2         ±8.0.2         ±8.2.4         £8.2.4<		$7195 \pm 0.0007$	$0.127 \pm 0.020$	124.2 ± 4.4	122 ± 19	102.0	0.65	Bi-1-11	.91	31	$261.9 \pm 6.5$	267 ± 17	98.1	0,0
0.0099 ± 0.0007		319 ± 0.0009	$0.336 \pm 0.031$	202.3 ± 5.8	294 ± 27	6.89	0.57	Bi-1-12	+1	$0.208 \pm 0.013$	197.7 ± 4.9	$192 \pm 12$	103.1	0,6
0.01999 ± 0.0007 0.1199 ± 0.0007 0.119		$7281 \pm 0.0007$	0.206 ± 0.019	178.7 ± 4.8	190 ± 18	94.1	0.31	Bi-1-13	-91	$4.281 \pm 0.136$	1570.3 ± 35.0	1690 ± 54	92.9	0.3
0.0.1999 ± 0.00070         0.135 ± 0.001         137.0 ± 4.50         1.16 ± 2.002         0.42         Bi-1-15         0.0399 ± 0.0007         0.136 ± 0.002         0.136 ± 0.002         0.031 ± 0.002         0.031 ± 0.002         0.031 ± 0.002         0.034 ± 0.0001         0.034 ± 0.000 <td></td> <td>187 ± 0.0005</td> <td><math>0.106 \pm 0.013</math></td> <td>119.3 ± 3.4</td> <td><math>102 \pm 12</math></td> <td>116.4</td> <td>0.62</td> <td>Bi-1-14</td> <td>4</td> <td>141</td> <td>1488.9 ± 32.8</td> <td>1628 ± 49</td> <td>5.16</td> <td>0.0</td>		187 ± 0.0005	$0.106 \pm 0.013$	119.3 ± 3.4	$102 \pm 12$	116.4	0.62	Bi-1-14	4	141	1488.9 ± 32.8	1628 ± 49	5.16	0.0
0.0349 ± 0.0009         0.139 ± 0.004         0.139		$7000.0 \pm 9910$	$0.130 \pm 0.021$	$127.0 \pm 4.5$	$124 \pm 20$	102.2	0.42	Bi-1-15	$0.0399 \pm 0.0011$	-31	$252.4 \pm 6.7$	$279 \pm 20$	5.06	0.7
0.0020 ± 0.0020 0.153 ± 0.004 1178 ± 5.7 1 46 ± 17 80.5 0.56 Bi-1.17 0.0337 ± 0.0009 0.257 ± 0.017 0.0237 ± 0.000 0.025 ± 0.002 0.153 ± 0.004 0.155 ± 0.004		1241 ± 0.0009	$0.139 \pm 0.026$	153,5 ± 5.7	132 ± 24	116.3	0.65	Bi-1-16	+	-11	$1920.3 \pm 49.9$	1888 ± 60	101.7	0.4
0.0034 p.0000 0.155 p.0020 1133 p.03 5.04 Bi-1-18 0.0354 p.0088 5.517 p.0180 1955 p.018 100.5 0.0018 p.0000 0.155 p.0020 1173 p.0020 p.0020 p.0020 1173 p.0020 p.0020 1173 p.0020 1173 p.0020 1173 p.0020 1173 p.0020 p.0020 1173 p.0020 p.0020 1173 p.0020 p.0020 1173 p.0020		1184 ± 0.0009	$0.155 \pm 0.018$	117.8 ± 5.7	$146 \pm 17$	80.5	92.0	Bi-1-17	-41	0,257 ± 0,022	205.6 ± 6.5	$232 \pm 20$	88.6	0.4
0.01934 ± 0.0000         0.175 ± 0.02         11.2 ± 5.9         0.434 ± 0.0000         5.571 ± 0.016         195.3 ± 6.1         10.1           0.018 ± 0.0010         5.520 ± 0.30         1.02 ± 0.0010         5.531 ± 0.016         193.7 ± 9.9         10.1           0.018 ± 0.0010         5.520 ± 0.30         1.02 ± 0.0010         0.038 ± 0.0017         0.037 ± 0.0017         2.05 ± 6.5         3.38 ± 14         7.17           0.0324 ± 0.0010         0.125 ± 0.023         1.023 ± 0.0017         0.042 ± 0.0017         0.042 ± 0.0017         2.05 ± 6.5         3.88 ± 14         7.17           0.0234 ± 0.0011         0.179 ± 0.022         1.025 ± 0.022         1.025 ± 0.023         1.0022         0.0017         2.0017 <td></td> <td>0.00000000000000000000000000000000000</td> <td><math>0.137 \pm 0.013</math></td> <td>128.3 ± 5.8</td> <td>130 ± 13</td> <td>98.5</td> <td>89.0</td> <td>Bi-1-18</td> <td>+</td> <td><math>5.224 \pm 0.172</math></td> <td>1865.9 ± 48.8</td> <td><math>1826 \pm 61</math></td> <td>100.5</td> <td>0,3</td>		0.00000000000000000000000000000000000	$0.137 \pm 0.013$	128.3 ± 5.8	130 ± 13	98.5	89.0	Bi-1-18	+	$5.224 \pm 0.172$	1865.9 ± 48.8	$1826 \pm 61$	100.5	0,3
0.0354 ± 0.0010		1184 ± 0.0009	$0.150 \pm 0.020$	$117.3 \pm 5.9$	$142 \pm 19$	82.0	0.85	Bi-1-19	44	$5.517 \pm 0.180$	$1953.8 \pm 51.0$	1903 ± 62	102.7	0.7
0.0323 ± 0.0146         5.620 ± 0.340         1873 ± 0.0146         5.620 ± 0.034         1871 ±		$0181 \pm 0.0010$	$0.126 \pm 0.022$	$115.4 \pm 6.3$	120 ± 21	96.1	1.12	Bi-1-20	44	#	1943.7 ± 49.9	1912 ± 55	101.7	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$3423 \pm 0.0146$	5.620 ± 0.340	1897.9 ± 80.8	1919 ± 116	6.86	0.27	Bi-1-21	40	+1	242.6 ± 6.5	338 ± 14	71.7	0.65
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$0432 \pm 0.0019$	$0.328 \pm 0.023$	$272.5 \pm 11.8$	288 ± 20	94.5	0.44	Bi-1-22	42	#4	269.7 ± 7.4	$278 \pm 15$	97.1	0.5
0.0199 ± 0.0010 0.147 ± 0.020 1.15.3 ± 6.5 139 ± 19 91.6 0.50 B B1-24 0.03373 ± 0.0006 5.347 ± 0.021 18.6 ± 2.4 11.2 ± 0.2373 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.047 ± 0.0010 0.048 ± 0.0010 0.049		1234 ± 0.0011	$0.196 \pm 0.023$	149.0 ± 7.2	182 ± 22	82.0	0.62	Bi-1-23	+1.	+	2428.6 ± 62,4	2436 ± 69	2.66	0.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$9200 \pm 0.0010$	0.147 ± 0.020	$127.5 \pm 6.5$	139 ± 19	9.16	69.0	Bi-1-24	41	# .	$1873.7 \pm 48.0$	1876 ± 54	6.66	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		07007 = 07010	0.176 ± 0.022	128.5 ± 6.5	165 ± 21	78.0	0.34	BI-1-25	# -	+1 -	1816.9 ± 54.1	1838 ± 80	6.86	2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		0199 ± 0.0012	0.141 ± 0.035	126.8 ± 7.5	134 ± 34	4.4	0.46	81-1-20	# -	H -	190.3 ± 3.9	219 ± 12	89.5	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		200 0 = 0.0015	0.131 ± 0.039	114,0 ± 8,0	125 ± 5/	91.4	1,03	17-1-19	H :	+1 -	1/2,3 ± 5.3	200 ± 13	0.70	0.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		1200 ± 0.0024	0.110 ± 0.070	120.7 = 13.0	111 # 13	0.01	0.30	07-1-19	H -	н	509 ± 6.605	01 ± 707	90.3	5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			# -	119.1 = 7.0	142 ± 50	65.9	0.00	67-1-19	44	#1 5	165,4 ± 5.6	CI = 691	90.4	0 0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			H :	160.1 = 7.4	332 ± 20	0.70	0.07	Bi-1-30	н -	H. 5	204.2 ± 8.2	11 = 0/2	98.0	3 6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			0.442 ± 0.003	2040 ± 78	3/2 ± 33	1003	0.54	Di-1-31	Н 4	н з	170 A ± 5.77	220 ± 13	0,000	3 6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		2100 ± 0200	0.106 ± 0.002	102.0 ± 4.0	162 ± 30	9001	0.53	Di 1 33	4 4	0.328 + 0.018	107 5 + 71	51 ± 001	01.1	200
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		2000 + 0,000	0.175 + 0.018	1275 + 43		707	P\$ 0	Bi-1-34	1 +	0.108 + 0.018	1016 + 72	181 + 17	104.6	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		3199 ± 0.0006	0.133 ± 0.014	127.1 ± 4.0		6 66	0.47	Bi-1-35	-41	5 092 + 0 205	1636.7 ± 54.2	1835 ± 74	89.2	0.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		3201 ± 0.0008	$0.144 \pm 0.020$	128.2 ± 4.8	137 ± 19	93.8	0.61	Bi-1-36	-44	+	2181.4 ± 72.7	2265 ± 94	96.3	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$3200 \pm 0.0007$	$0.138 \pm 0.018$	127.9 ± 4.6	131 ± 17	97.4	0.53	Bi-1-37	- 11	+	200.0 ± 7.4	270 ± 21	74.0	0.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$3609 \pm 0.0087$	5.594 ± 0.208	1986.5 ± 48.1	1915 ± 71	103.7	0.34	Bi-1-38	+1	+1	188.5 ± 6.5	252 ± 14	74.7	0.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			$0.213 \pm 0.019$	157.6 ± 4.9	196 ± 18	80.3	0.59	Bi-1-39	#	+	$1776.6 \pm 58.9$	1819 ± 74	7.76	0.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			111	218.8 ± 8.2	273 ± 34	80.4	0.73	Bi-1-40	+	+1	344.1 ± 12.4	512 ± 33	67.3	0.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			$0.200 \pm 0.027$	154.5 ± 5.9	185 ± 25	83.3	0.40	Bi-1-41	*	+#	266.7 ± 9.5	321 ± 22	83.0	0.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		7263 ± 0.0011	$0.208 \pm 0.027$	167.4 ± 6.9	192 ± 25	87.1	0.55	Bi-1-42	#	#	$1853.5 \pm 41.3$	1857 ± 65	8.66	0.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	$9226 \pm 0.0008$	$0.157 \pm 0.013$	143.8 ± 4.9	$148 \pm 12$	97.1	0.74	Bi-1-43	+1	+8	313.8 ± 8.4	358 ± 27	87.6	0.0
$0.0357 \pm 0.0012 \qquad 0.264 \pm 0.021 \qquad 226.1 \pm 7.7 \qquad 238 \pm 19 \qquad 94.9 \qquad 0.48 \qquad Bi-1-45 \qquad 0.5027 \pm 0.0112 \qquad 11.657 \pm 0.406 \qquad 2625.2 \pm 58.7 \qquad 2577 \pm 90 \qquad 101.9 \\ 0.0299 \pm 0.0011 \qquad 0.236 \pm 0.020 \qquad 190.0 \pm 6.7 \qquad 215 \pm 18 \qquad 88.2 \qquad 1.06 \qquad Bi-1-46 \qquad 0.0396 \pm 0.0012 \qquad 0.433 \pm 0.038 \qquad 250.3 \pm 7.6 \qquad 36.5 \pm 3.2 \qquad 68.6 \qquad 0.0399 \pm 0.0012 \qquad 0.433 \pm 0.038 \qquad 250.3 \pm 7.6 \qquad 36.5 \pm 3.2 \qquad 68.6 \qquad 0.0399 \pm 0.0012 \qquad 0.0433 \pm 0.038 \qquad 0.0499 \pm 0.0012 \qquad 0.0499 \pm 0.001$		$0420 \pm 0.0014$	0,312 ± 0,020	265.4 ± 8.6	276 ± 17	96.2	0.39	Bi-1-44	+1	-81	244.5 ± 6.8	288 ± 23	85.0	0.6
$0.0299 \pm 0.0001$ $0.236 \pm 0.020$ $190.0 \pm 6.7$ $215 \pm 18$ $88.2$ $1.06$ $Bi-1.46$ $0.0396 \pm 0.0012$ $0.433 \pm 0.038$ $250.3 \pm 7.6$ $365 \pm 3.2$ $68.6$		$0357 \pm 0.0012$	$0.264 \pm 0.021$	226.1 ± 7.7		6.46	0.48	Bi-1-45		#	2625.2 ± 58.7	2577 ± 90	101.9	1,35
一 一		1299 ± 0.0011	$0.236 \pm 0.020$	190.0 ± 6.7	$215 \pm 18$	88.2	1.06	Bi-1-46		+	250.3 ± 7.6	$365 \pm 32$	9.89	0

0.0299 ± 0.0009	Grain	$\Omega_{852}/9d_{902}$	Usez/94/oc	200Pb/23sU age (Ma)	<sup>207</sup> Pb/ <sup>235</sup> U age (Ma)	%conc	Th/U	Grain	.0%EP/93%U	$\Omega_{512}/4d_{105}$	206pb/23fU age (Ma)	<sup>207</sup> Pb/ <sup>225</sup> U age (Ma)	%conc	Th/U
0.0392 ± 0.0019	84-7-48	$0.0445 \pm 0.0012$	$0.419 \pm 0.032$	280,5 ± 7,8	356 ± 27	6.82	0.49	Bi-1-99	$0.0337 \pm 0.0006$	$0.255 \pm 0.013$	213.9 ± 3.8	$230 \pm 12$	92.8	0.46
0.0239 ± 0.0000	64-1-4	0.0392 ± 0.0010	$0.356 \pm 0.024$	247.9 ± 6.5		80.3	0.54	Bi-1-100	#	#	1851,1 ± 28,2	1861 ± 45	5.66	0.80
0.0257 ± 0.0000 0.235 ± 0.0000 0.255	11-1-50	0.0389 ± 0.0009	$0.343 \pm 0.017$	245.9 ± 5.8		82.2	0.45	Bi-1-101	+	+	207.5 ± 3.8	234 ± 12	88.8	0.32
0.0235 ± 0.0007 0.246 ± 0.002 18.6.4 ± 4.7 197 ± 18 0.28 0.78 0.78 0.2106 ± 0.0007 0.0024 ± 0.0007 0.0024 ± 0.0007 0.0024 ± 0.0007 0.0024 ± 0.000 0.0024 ± 0.0007 0.0024 ± 0.000 0.0024 ±	15-1-11	$0.0273 \pm 0.0006$	$0.239 \pm 0.017$	173.4 ± 4.0	$218 \pm 15$	79.5	82.0	Bi-1-102	$0.2598 \pm 0.0042$	1	$1489.0 \pm 23.8$	1646 ± 47	5.06	0.25
0.0353 ± 0.0010 0.465 ± 0.002 0.315 ± 6.3 389 ± 35 55.7 107 B1-1104 0.0358 ± 0.0036 0.0035 ± 0.0010 0.455 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.003 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.002 0.0035 ± 0.003 0.003 0.0035 ± 0.003 0.003 0.0035 ± 0.003 0.003 0.003 0.003 0.003	11-1-52	$0.0288 \pm 0.0005$	$0.273 \pm 0.012$	183.0 ± 3.5	245 ± 11	74.8	0.38	Bi-1-103	$0.0281 \pm 0.0007$	41	178.5 ± 4.3	205 ± 18	87.0	0.62
0.0035 ± 0.0007 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0035 ± 0.0004 0.0030 ± 0.000	11-1-53	$0.0342 \pm 0.0010$	$0.466 \pm 0.042$	216.5 ± 6.5	389 ± 35	55.7	1.07	Bi-1-104	$0.3768 \pm 0.0036$		$2061.3 \pm 19.7$		104.5	0.27
0.0237 ± 0.0005	81-1-54	$0.0287 \pm 0.0007$	0,214 ± 0,020	182.4 ± 4.7		92.8	0.78	Bi-1-105	0.2106 ± 0.0024	+1	1231.8 ± 14.0		84.9	0.3
0.0339 ± 0.0005 0.0349 ± 0.0005 0.0349 ± 0.0005 0.0349 ± 0.0005 0.0349 ± 0.0005 0.0349 ± 0.0005 0.0349 ± 0.0005 0.0349 ± 0.0007 0.0350 ± 0.0007 0.0350 ± 0.0007 0.0350 ± 0.0007 0.0370 ± 0.000	8-1-55	$0.0635 \pm 0.0012$	$0.492 \pm 0.024$	397.2 ± 7.7	406 ± 20	8.76	0.50	Bi-1-106	0.0406 ± 0.0009	+	256.6 ± 5.8	295 ± 28	86.9	0.7
0.63494 ± 0.00002	9-1-18	$0.0277 \pm 0.0006$	$0.198 \pm 0.012$	176.4 ± 3.7	183 ± 11	6.96	95.0	Bi-1-107	$0.0282 \pm 0.0004$	++	179.3 ± 2.2	178 ± 9	100.8	0
0.0349 ± 0.0007	0-1-57	$0.3494 \pm 0.0062$	5.578 ± 0.179	$1932.0 \pm 34.3$	$1913 \pm 61$	101.0	0.30	Bi-1-108	$0.0396 \pm 0.0004$	+	250.1 ± 2.8	287 ± 12	87.3	0
0.0336 ± 0.0007 0.221 ± 0.0014 0.2112 ± 4,1 227 ± 15 97,5 d.2 Bi-1-110 0.0335 ± 0.0003 0.0330 ± 0.0005 0.221 ± 0.0014 0.0071 0.0214 ± 0.019 0.0032 ± 0.0005 0.0330 ± 0.0005 0.0214 ± 0.019 0.0032 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0001 0.0321 ± 0.0005 0.0330 ± 0.0005 0.0330 ± 0.0003 0.0322 ± 0.0006 0.037 ± 0.0010 0.0322 ± 0.0000 0.0322 ± 0.0010 0.0322 ± 0.0001 0.0322 ± 0.0010 0.0322 ± 0.0003 0.0320 ± 0.0010 0.0320 ± 0.0003 0.0320 ± 0.0003 0.0320 ± 0.0000 0.0320 ± 0.0003 0.03	F-1-58	0.0342 ± 0.0008	$0.368 \pm 0.023$	216.6 ± 4.9	$318 \pm 20$	1.89	0.59	Bi-1-109	$0.3639 \pm 0.0032$	$5.726 \pm 0.164$	$2000.7 \pm 17.8$	$1935 \pm 55$	103.4	0.57
0.0332 ± 0.0005 0.221 ± 0.000 1907.1 ± 3.5 0.22 ± 9 974 0.65 Bi-1-111 0.0381 ± 0.0005 0.231 ± 0.0005 0.231 ± 0.0005 0.231 ± 0.0005 0.231 ± 0.0005 0.231 ± 0.0005 0.231 ± 0.0005 0.231 ± 0.0005 0.237 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0005 0.230 ± 0.0007 0.230 ± 0.0005 0.230 ± 0.	9-1-59	$0.0349 \pm 0.0007$	0,250 ± 0,014	221.2 ± 4.1	227 ± 12	5.76	0.42	Bi-1-110	$0.3355 \pm 0.0031$	5.347 ± 0.160	$1865.0 \pm 17.4$	1876 ± 56	99.4	0,23
0.00000 0.0007 0.214 ± 0.019 0.000 0.0000 0.	9-1-60	$0.0310 \pm 0.0005$	$0.221 \pm 0.010$	197.1 ± 3.5	202 ± 9	97.4	0.65	Bi-1-111	$0.0381 \pm 0.0005$	#	$241.0 \pm 2.9$	256 ± 12	94.2	0
0.3332 ± 0.0055 5.153 ± 0.166 1849, ± 3.07 1845 ± 59 1002 0.83 81-113 0.0394 ± 0.0012 0.0332 ± 0.0063 5.313 ± 0.148 1841.5 ± 2.94 1841 ± 53 100.0 0.88 81-113 0.0394 ± 0.0012 0.0333 ± 0.0005 0.202 ± 0.0101 0.0333 ± 0.0005 0.202 ± 0.0010 0.0334 ± 0.0005 0.202 ± 0.0010 0.0335 ± 0.0003 0.0202 ± 0.0011 0.0333 ± 0.0005 0.202 ± 0.0011 1861.5 ± 2.94 0.95 186 ± 1.18 0.0394 ± 0.0010 0.0252 ± 0.0004 0.0252 ± 0.0004 0.0252 ± 0.0011 181.5 ± 2.3 186 ± 1.0 0.025 181-113 0.0334 ± 0.0010 0.0252 ± 0.0004 0.0252 ± 0.0004 0.0252 ± 0.0004 0.0252 ± 0.0004 0.0252 ± 0.0004 0.0252 ± 0.0004 0.0252 ± 0.0004 0.0252 ± 0.0004 0.0252 ± 0.0005 0.	19-1-6	0.0300 ± 0.0007	$0.214 \pm 0.019$	190.6 ± 4.7	197 ± 18	8.96	0.49	Bi-1-112		0.269 ± 0.022	206.0 ± 4.0	242 ± 20	85.3	0
0.0233 ± 0.00053 5.311 ± 0.148 1841.5 ± 294 1841 ± 53 100.0 0.88 16.1-114 0.3194 ± 0.00052 0.0279 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0234 ± 0.0016 0.0235 ± 0.0003 0.0235 ± 0.0003 0.0235 ± 0.0003 0.0235 ± 0.0016 0.0235 ± 0.0017 0.0236 ± 0.0006 0.0236 ± 0.0017 0.0236 ± 0.0006 0.0232 ± 0.0017 0.0236 ± 0.0006 0.0232 ± 0.0017 0.0	6-1-62	0.3322 ± 0.0055	5.153 ± 0.166	1849.1 ± 30.7	1845 ± 59	100.2	0.38	Bi-1-113	0.0364 ± 0.0012	計	230.2 ± 7.8	258 ± 22	1.68	0.57
$0.0233 \pm 0.0006 \qquad 0.299 \pm 0.0106 \qquad 2045 \pm 4.0 \qquad 264 \pm 14 \qquad 77.4 \qquad 6.90 \qquad Bi-1-15 \qquad 0.0239 \pm 0.0015 \\ 0.0233 \pm 0.0003 \qquad 5.302 \pm 0.151 \qquad 1864.3 \pm 9.0 \qquad 26.9 \qquad Bi-1-16 \qquad 0.0279 \pm 0.0010 \\ 0.0255 \pm 0.0043 \qquad 5.302 \pm 0.151 \qquad 1864.3 \pm 9.9 \qquad 1869.4 \pm 9.9 \qquad 9.4 \qquad 0.92 \qquad Bi-1-17 \qquad 0.0279 \pm 0.0010 \\ 0.0255 \pm 0.0043 \qquad 6.316 \pm 0.019 \qquad 180.4 \pm 3.9 \qquad 6.017 \qquad 181.1 \qquad 0.0279 \pm 0.0010 \\ 0.0256 \pm 0.0046 \qquad 0.316 \pm 0.019 \qquad 181.5 \pm 3.2 \qquad 189 \pm 1.0 \qquad 9.7 \qquad 0.37 \qquad Bi-1-18 \qquad 0.0059 \pm 0.0010 \\ 0.0256 \pm 0.0045 \qquad 6.202 \pm 0.011 \qquad 181.5 \pm 3.2 \qquad 187 \pm 10 \qquad 9.7 \qquad 0.32 \qquad Bi-1-12 \qquad 0.0219 \pm 0.0010 \\ 0.0256 \pm 0.0045 \qquad 6.202 \pm 0.011 \qquad 181.5 \pm 3.2 \qquad 187 \pm 10 \qquad 9.7 \qquad 0.35 \qquad Bi-1-12 \qquad 0.0319 \pm 0.0010 \\ 0.0256 \pm 0.0005 \qquad 5.553 \pm 0.190 \qquad 1956.3 \pm 5.0 \qquad 1999 \pm 5.7 \qquad 9.5 \qquad Bi-1-12 \qquad 0.0329 \pm 0.0010 \\ 0.0454 \pm 0.0005 \qquad 6.0531 \pm 0.019 \qquad 2.956 \pm 5.2 \qquad 3.06 \pm 17 \qquad 9.5 \qquad Bi-1-12 \qquad 0.0329 \pm 0.0000 \\ 0.0454 \pm 0.0012 \qquad 0.521 \pm 0.030 \qquad 419.7 \pm 7.8 \qquad 3.06 \pm 17 \qquad 9.5 \qquad 4.8 \qquad Bi-1-12 \qquad 0.0329 \pm 0.0000 \\ 0.0453 \pm 0.0010 \qquad 0.521 \pm 0.003 \qquad 419.7 \pm 7.8 \qquad 3.06 \pm 1.7 \qquad 9.5 \qquad 0.38 \qquad Bi-1-12 \qquad 0.0334 \pm 0.0005 \\ 0.0453 \pm 0.0010 \qquad 0.521 \pm 0.003 \qquad 419.7 \pm 7.8 \qquad 3.06 \pm 1.7 \qquad 9.5 \qquad 0.38 \qquad Bi-1-12 \qquad 0.0334 \pm 0.0005 \\ 0.0453 \pm 0.0010 \qquad 0.521 \pm 0.003 \qquad 449.7 \pm 7.8 \qquad 3.06 \pm 1.7 \qquad 9.5 \qquad 0.39 \qquad Bi-1-12 \qquad 0.0329 \pm 0.0000 \\ 0.0453 \pm 0.0010 \qquad 0.521 \pm 0.003 \qquad 2.242 \pm 1.3 \qquad 80.8 \qquad 1.0 \qquad 0.39 \qquad Bi-1-12 \qquad 0.0239 \pm 0.0000 \\ 0.0453 \pm 0.0010 \qquad 0.529 \pm 0.004 \qquad 2.552 \pm 9.3 \qquad 3.78 \pm 3.7 \qquad 3.72 \pm 1.3 \qquad 8.8 \qquad 0.049 \qquad Bi-1-12 \qquad 0.0239 \pm 0.0000 \\ 0.0453 \pm 0.0017 \qquad 0.529 \pm 0.004 \qquad 2.552 \pm 9.3 \qquad 3.72 \pm 1.1 \qquad 8.3 \qquad 0.39 \qquad Bi-1-12 \qquad 0.0329 \pm 0.0000 \\ 0.0453 \pm 0.0017 \qquad 0.529 \pm 0.004 \qquad 2.502 \pm 0.004 \qquad 2.502 \pm 0.001 \qquad 0.0238 \pm 0.001 \qquad 0.0239 \pm 0.0000 \\ 0.0453 \pm 0.0017 \qquad 0.239 \pm 0.023 \qquad 2.242 \pm 11 \qquad 3.94 \pm 14 \qquad 8.92 \qquad 0.35 \qquad Bi-2-2 \qquad 0.0239 \pm 0.0000 \\ 0.0253 \pm 0.0010 \qquad 0.229 \pm 0.012 \qquad 2.202 \pm 2.7 \pm 11 \qquad 3.94 \pm 10 \qquad 0.329 \qquad 0.0209 \pm 0.0000 \\ 0.0253 \pm 0.0010 \qquad 0.229 \pm 0.012 \qquad 2.202 \pm 2.7 \pm 11 \qquad 3.94 \pm 10 \qquad 0.329 \qquad 0.0209 \\ 0.0295 \pm 0.0000 \qquad 0.229 \pm 0.012 \qquad 2.242 \pm 11 \qquad 3.94 \pm 11 \qquad 3.94 \qquad 0.35 \qquad Bi-2-1 \qquad 0.02$	6-1-63	$0.3307 \pm 0.0053$	5.131 ± 0.148	1841.5 ± 29.4	1841 ± 53	100.0	0.85	Bi-1-114	$0.3194 \pm 0.0095$	$5.031 \pm 0.192$	$1786.8 \pm 52.9$	1825 ± 69	6.76	0.30
0.0233 ± 0.0005 0.207 ± 0.010 188.1 ± 3.2 191 ± 9 94.4 0.92 81-7.17 0.0279 ± 0.0010 0.0235 ± 0.0033 3.920 ± 0.1211 186.2 ± 2.97 186.9 ± 5.97 0.25 81-1.17 0.0279 ± 0.0010 0.0235 ± 0.0043 3.920 ± 0.121 186.2 ± 2.97 186.9 ± 5.97 0.25 81-1.19 0.0311 ± 0.0010 0.0235 ± 0.0040 0.0235 ± 0.0040 0.0235 ± 0.0040 0.0235 ± 0.0040 0.0235 ± 0.0040 0.0235 ± 0.0041 181.5 ± 3.2 179 ± 5.7 9.5 9 0.27 81-1.19 0.0311 ± 0.0010 0.0235 ± 0.0045 0.0235 ± 0.0045 0.0235 ± 0.0045 0.0235 ± 0.0045 0.0355 ± 0.0045 0.0355 ± 0.0045 0.0355 ± 0.0045 0.0355 ± 0.0045 0.0355 ± 0.0045 0.0355 ± 0.0040 0.0351 ± 0.0010 0.0252 ± 0.004 0.0351 ± 0.0010 0.0252 ± 0.0045 0.0352 ± 0.0045 0.0352 ± 0.0045 0.0352 ± 0.0045 0.0352 ± 0.0045 0.0352 ± 0.0045 0.0352 ± 0.0045 0.0352 ± 0.0045 0.0052 0.034 ± 0.0010 0.0522 ± 0.0047 0.0522 ± 0.0047 0.0052 ± 0.0040 0.0052 ± 0.0040	1-1-64	0.0322 ± 0.0006	0.297 ± 0.016	204.3 ± 4.0	264 ± 14	77.4	0.00	Bi-1-115	$0.0394 \pm 0.0012$	$0.311 \pm 0.016$	249,2 ± 7.6	275 ± 14	906	0
0.0353 ± 0.0063 5.590 ± 0.151 $  8642 \pm 297   899 \pm 53 997   0.36   Bi-1-17 0.0209 \pm 0.0000 0.0226 \pm 0.00043 0.0043   0.316 \pm 0.018   0.0043   0.320 \pm 0.018   0.018 \pm 30 - 0.018   0.316 \pm 0.018   0.018 \pm 30 - 0.018   0.316 \pm 0.018   0.018 \pm 30 - 0.018   0.018 \pm 0.0005   0.320 \pm 0.011   0.010   0.0000   0.000   0.0000   0.0000   0.0$	6-1-65	0.0283 ± 0.0005	$0.207 \pm 0.010$	180.1 ± 3.2	6 ± 161	94.4	0.92	Bi-1-116	0.0435 ± 0.0015		274.4 ± 9.7	316 ± 29	86.7	0.45
0.0255 ± 0.0005 0.025 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0006 0.0256 ± 0.0007 0.0257 ± 0.0007 0.0257 ± 0.0007 0.0257 ± 0.0007 0.0257 ± 0.0007 0.0252 ± 0.0006 0.0258 ± 0.0006 0.0258 ± 0.0006 0.0258 ± 0.0007 0.0258 ± 0.0007 0.0258 ± 0.0007 0.0258 ± 0.0007 0.0259 ± 0.0006 0.0250 ± 0.0006 0.0250 ± 0.0006 0.0250 ± 0.0006 0.0250 ± 0.0006 0.0250 ± 0.0006	99-1-19	$0.3353 \pm 0.0053$	5.302 ± 0.151	1864.2 ± 29.7	1869 ± 53	7.66	0.36	Bi-1-117	$0.0279 \pm 0.0010$	#	177.4 ± 6.4	191 ± 20	92.9	0
$0.0325 \pm 0.0006 \qquad 0.316 \pm 0.018 \qquad 2076 \pm 3.9 \qquad 279 \pm 16 \qquad 74.5 \qquad 0.51 \qquad Bi-i-i19 \qquad 0.0331 \pm 0.0001 \\ 0.02956 \pm 0.0005 \qquad 0.0202 \pm 0.011 \qquad 181,5 \pm 2.5 \qquad 187 \pm 10 \qquad 97.2 \qquad 0.35 \qquad Bi-i-i20 \qquad 0.02396 \pm 0.0000 \\ 0.02956 \pm 0.0005 \qquad 0.0351 \pm 0.019 \qquad 195.3 \pm 3.04 \qquad 1909 \pm 65 \qquad 101.4 \qquad 0.85 \qquad Bi-i-i21 \qquad 0.03246 \pm 0.0005 \\ 0.0363 \pm 0.0006 \qquad 0.0351 \pm 0.019 \qquad 195.3 \pm 3.04 \qquad 1909 \pm 65 \qquad 101.4 \qquad 0.85 \qquad Bi-i-i21 \qquad 0.0326 \pm 0.0005 \\ 0.04540 \pm 0.00070 \qquad 0.0521 \pm 0.019 \qquad 291.6 \pm 5.2 \qquad 306 \pm 17 \qquad 95.4 \qquad 0.81 \qquad Bi-i-i22 \qquad 0.0320 \pm 0.0005 \\ 0.0673 \pm 0.00070 \qquad 0.0521 \pm 0.019 \qquad 291.6 \pm 5.2 \qquad 306 \pm 17 \qquad 95.4 \qquad 0.81 \qquad Bi-i-i22 \qquad 0.0320 \pm 0.0005 \\ 0.0673 \pm 0.00070 \qquad 0.0521 \pm 0.019 \qquad 291.6 \pm 5.2 \qquad 306.2 \pm 3.3 \qquad 37.8 \pm 3.3 \qquad 70.2 \qquad Bi-i-i25 \qquad 0.0299 \pm 0.0005 \\ 0.0673 \pm 0.0010 \qquad 0.0521 \pm 0.003 \qquad 419.7 \pm 7.8 \qquad 2.020 \pm 2.5 \qquad 98.6 \qquad 0.78 \qquad Bi-i-i25 \qquad 0.0320 \pm 0.0005 \\ 0.0450 \pm 0.00070 \qquad 0.459 \pm 0.029 \qquad 2.056 \pm 9.3 \qquad 3.78 \pm 3.3 \qquad 70.2 \qquad Bi-i-i25 \qquad 0.0299 \pm 0.0005 \\ 0.0450 \pm 0.0010 \qquad 0.459 \pm 0.029 \qquad 2.059 \pm 5.5 \qquad 1809 \pm 7.8 \qquad 10.24 \qquad 0.259 \qquad Bi-i-i25 \qquad 0.0299 \pm 0.0005 \\ 0.0450 \pm 0.0010 \qquad 0.459 \pm 0.022 \qquad 2.089 \pm 8.56 \qquad 1809 \pm 7.8 \qquad 10.24 \qquad 0.279 \qquad Bi-i-i25 \qquad 0.0299 \pm 0.0005 \\ 0.0450 \pm 0.0017 \qquad 0.528 \pm 0.032 \qquad 2.089 \pm 8.5 \qquad 10.24 \pm 1.8 \qquad 10.24 \qquad 0.279 \qquad Bi-i-i25 \qquad 0.0391 \pm 0.0005 \\ 0.0450 \pm 0.0017 \qquad 0.528 \pm 0.032 \qquad 2.089 \pm 8.5 \qquad 10.24 \qquad 1.8 \qquad 8.9 \qquad 0.259 \qquad Bi-i-i25 \qquad 0.0291 \pm 0.0005 \\ 0.0460 \pm 0.0017 \qquad 0.528 \pm 0.032 \qquad 2.091 \pm 0.6 \qquad 3.9 \qquad 3.12 \pm 1.4 \qquad 4.9 \pm 2.3 \qquad 3.20 \qquad 1.9 \qquad 3.12 \pm 1.4 \qquad 4.9 \pm 2.3 \qquad 3.20 \qquad 1.9 \qquad 3.20 \qquad 3.20$	19-1-19	$0.2626 \pm 0.0043$	3.920 ± 0.121	1503.1 ± 24.5	1618 ± 50	92.9	0.27	Bi-1-118	$0.0509 \pm 0.0020$	+	$320.2 \pm 12.8$	325 ± 42	98.4	0.57
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	89-1-1	0.0327 ± 0.0006	$0.316 \pm 0.018$	207.6 ± 3.9	$279 \pm 16$	74.5	0.51	Bi-1-119	$0.0311 \pm 0.0010$	-41	$197.6 \pm 6.4$	199 ± 15	99.2	0
0.2952 ± 0.0045	69-1-9	$0.0286 \pm 0.0005$	$0.202 \pm 0.011$	181.5 = 3.2	187 ± 10	97.2	0.32	Bi-1-120	$0.0280 \pm 0.0009$	-44	178,1 ± 5.7	189 ± 13	94,4	0
0.4554 ± 0.0055 5.553 ± 0.190 1936.3 ± 30.4 1909 ± 65 101.4 0.85 Bi-1-122 0.3260 ± 0.0055 0.4645.2 ± 0.0008 8.552 ± 0.219 10.45 ± 2.2 29.6 ± 1.7 95.4 0.81 Bi-1-123 0.334 ± 0.0058 0.4540 ± 0.0070 8.552 ± 0.239 14.2 2.2 24.5 ± 2.5 98.6 ± 1.7 95.4 0.81 Bi-1-124 0.799 ± 0.0058 0.4530 ± 0.0071 ± 0.0072 ± 0.0030 1.9 19.7 ± 1.8 1.2 1.3 0.344 ± 0.0058 0.3821 ± 0.0005 0.521 ± 0.030 1.9 19.7 ± 1.8 1.2 1.3 0.344 ± 0.0058 0.3821 ± 0.0005 0.521 ± 0.030 1.9 19.2 ± 2.5 10.4 1.3 0.19 Bi-1-125 0.0290 ± 0.0006 0.0351 ± 0.001 0.265 ± 0.049 1.9 19.2 ± 3.5 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	11-1-70	$0.2952 \pm 0.0045$	4.546 ± 0.149	1667.5 ± 25.6	1739 ± 57	656	0.35	Bi-1-121	$0.3216 \pm 0.0055$	44	1797.6 ± 30.5	$1861 \pm 55$	9.96	0.34
0.0463 $\pm$ 0.0008 0.351 $\pm$ 0.019 291,6 $\pm$ 5.2 366 $\pm$ 17 95,4 0.81 Bi-1-123 0.3344 $\pm$ 0.0058 0.4540 $\pm$ 0.0007 0.551 $\pm$ 0.019 211 $\pm$ 37.0 2292 $\pm$ 73 105.3 0.39 Bi-1-124 0.1793 $\pm$ 0.0036 0.0451 $\pm$ 0.0007 0.551 $\pm$ 0.021 $\pm$ 0.020 $\pm$ 0.0006 0.0521 $\pm$ 0.0007 0.0522 $\pm$ 0.0007 0.0529 $\pm$ 0.0009 0.0529 $\pm$ 0.00	17-1-6	0.3504 ± 0.0055	5.553 ± 0.190	1936.3 ± 30.4	1909 ± 65	101.4	0.85	Bi-1-122	0.3260 ± 0.0055	941	$1818.8 \pm 30.6$	1830 ± 53	99.4	0.25
$0.4540 \pm 0.0070 \qquad 8.562 \pm 0.273 \qquad 2413.1 \pm 37.0 \qquad 2292 \pm 77 \qquad 105.3 \qquad 0.39 \qquad Bi-i-j24 \qquad 0.1793 \pm 0.0030 \\ 0.0573 \pm 0.0012 \qquad 0.0221 \pm 0.030 \qquad 4197.3 \pm 37.0 \qquad 2292 \pm 77 \qquad 105.3 \qquad 0.39 \qquad Bi-i-j24 \qquad 0.1793 \pm 0.0000 \\ 0.03821 \pm 0.0012 \qquad 0.0221 \pm 0.030 \qquad 4197.3 \pm 37.5 \qquad 2401 \pm 6.5 \qquad 0.019 \qquad Bi-i-j27 \qquad 0.0239 \pm 0.0000 \\ 0.03821 \pm 0.0005 \qquad 0.0452 \pm 0.0040 \qquad 265.5 \pm 9.3 \qquad 3.78 \pm 33 \qquad 70.2 \qquad 0.59 \qquad Bi-i-j27 \qquad 0.0299 \pm 0.0000 \\ 0.0421 \pm 0.0015 \qquad 0.452 \pm 0.0040 \qquad 265.5 \pm 9.3 \qquad 3.78 \pm 33 \qquad 70.2 \qquad 0.59 \qquad Bi-i-j27 \qquad 0.0299 \pm 0.0000 \\ 0.04510 \pm 0.0010 \qquad 0.452 \pm 0.0040 \qquad 265.5 \pm 9.3 \qquad 3.78 \pm 33 \qquad 70.2 \qquad 0.59 \qquad Bi-i-j27 \qquad 0.0299 \pm 0.0000 \\ 0.04510 \pm 0.0010 \qquad 0.452 \pm 0.0040 \qquad 265.5 \pm 9.3 \qquad 3.78 \pm 33 \qquad 70.2 \qquad 0.59 \qquad Bi-i-j27 \qquad 0.0299 \pm 0.0000 \\ 0.0527 \pm 0.0017 \qquad 0.538 \pm 0.024 \qquad 3.913 \pm 1.04 \qquad 4.91 \pm 28 \qquad 77.0 \qquad 0.78 \qquad Bi-i-j \qquad 0.03873 \pm 0.0005 \\ 0.0353 \pm 0.0017 \qquad 0.311 \pm 0.017 \qquad 230.2 \pm 6.9 \qquad 275 \pm 1.5 \qquad 83.8 \qquad 83.8 \qquad 83.9 \qquad 23.7 \pm 0.0005 \\ 0.0459 \pm 0.0017 \qquad 0.311 \pm 0.017 \qquad 230.1 \pm 9.6 \qquad 3.92 \pm 1.8 \qquad 0.028 & 0.0000 \\ 0.0459 \pm 0.0017 \qquad 0.311 \pm 0.0017 \qquad 230.1 \pm 9.6 \qquad 0.028 & 0.0005 \\ 0.0459 \pm 0.0010 \qquad 0.252 \pm 0.017 \qquad 242 \pm 11 \qquad 89.9 \qquad 0.33 \qquad Bi-i-j \qquad 0.0298 \pm 0.0005 \\ 0.0291 \pm 0.0010 \qquad 0.2291 \pm 0.012 \qquad 177.9 \pm 1.4 \qquad 0.0009 \\ 0.0292 \pm 0.0000 \qquad 0.2218 \pm 0.012 \qquad 177.9 \pm 3.4 \qquad 14 \qquad 89.9 \qquad 0.37 \qquad Bi-i-j \qquad 0.0297 \pm 0.0009 \\ 0.0293 \pm 0.0000 \qquad 0.2218 \pm 0.012 \qquad 177.1 \pm 4.0 \qquad 2011 \pm 11 \qquad 9.3.5 \qquad 0.227 \equiv 0.0009 \\ 0.0293 \pm 0.0000 \qquad 0.218 \pm 0.012 \qquad 187.1 \pm 3.6 \qquad 162 \pm 8 \qquad 0.039 \qquad Bi-i-j \qquad 0.0297 \pm 0.0009 \\ 0.0293 \pm 0.0000 \qquad 0.211 \pm 0.014 \qquad 186.4 \pm 4.3 \qquad 194 \pm 13 \qquad 95.9 \qquad 0.39 \qquad Bi-i-j \qquad 0.0294 \pm 0.0005 \\ 0.0293 \pm 0.0000 \qquad 0.211 \pm 0.014 \qquad 186.4 \pm 4.3 \qquad 194 \pm 13 \qquad 95.9 \qquad 0.35 \qquad Bi-i-j \qquad 0.0294 \pm 0.0006 \\ 0.0293 \pm 0.0000 \qquad 0.211 \pm 0.014 \qquad 186.4 \pm 3.3 \qquad 194 \pm 13 \qquad 95.3 \qquad 0.35 \qquad Bi-i-j \qquad 0.0294 \pm 0.0009 \\ 0.0293 \pm 0.0000 \qquad 0.211 \pm 0.014 \qquad 185.4 \pm 3.3 \qquad 3.41 \pm 10 \qquad 2.35 \qquad 1.34 \qquad 1.05 \qquad 3.34 \qquad 3.34 \qquad 3.34 \qquad 3.34 \qquad 3.34 \qquad 3.34 $	1-1-72	$0.0463 \pm 0.0008$	0.351 ± 0.019	291,6 ± 5.2	306 ± 17	95.4	0.81	Bi-1-123	0.3344 ± 0.0058	Ŧ	$1859.6 \pm 32.0$	Ŧ	1.66	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	i-1-73	$0.4540 \pm 0.0070$	8.562 ± 0.273	2413.1 ± 37.0	2292 ± 73	105.3	0.39	Bi-1-124	$0.1793 \pm 0.0030$	+	$1063.0 \pm 17.9$	$1303 \pm 38$	81.6	0.20
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-74	$0.0673 \pm 0.0012$	$0.521 \pm 0.030$	419.7 ± 7.8	426 ± 25	986	0.78	Bi-1-125	+4		212.7 ± 5.4	333 ± 26	63.8	0,72
$0.0338 \pm 0.0006 \qquad 0.259 \pm 0.014 \qquad 195.3 \pm 3.5 \qquad 2.42 \pm 13 \qquad 80.8 \qquad 0.60 \qquad Bi-1-127 \qquad 0.0298 \pm 0.0006 \\ 0.0421 \pm 0.00101 \qquad 0.265 \pm 0.0224 \qquad 2.655 \pm 9.3 \qquad 3.78 \pm 33 \qquad 70.2 \qquad 0.359 \qquad Bi-1-128 \qquad 0.0224 \pm 0.0005 \\ 0.0450 \pm 0.00101 \qquad 0.597 \pm 0.0225 \qquad 2.83.9 \pm 8.7 \qquad 4170 \pm 24 \qquad 68.2 \qquad 1.29 \qquad Sandstone of the middle part of 0.3699 \pm 0.0101 \qquad 5.899 \pm 0.251 \qquad 2.028.8 \pm 58.6 \qquad 1961 \pm 83 \qquad 103.5 \qquad 0.26 \qquad Bi-2-1 \qquad 0.3873 \pm 0.0065 \\ 0.0537 \pm 0.0017 \qquad 0.538 \pm 0.034 \qquad 2.0218 \pm 10.4 \qquad 430 \pm 2.8 \qquad 7.70 \qquad 0.78 \qquad Bi-2-2 \qquad 0.03294 \pm 0.0005 \\ 0.0537 \pm 0.0017 \qquad 0.538 \pm 0.034 \qquad 2.90.1 \pm 9.6 \qquad 2.75 \pm 15 \qquad 8.38 \qquad 0.38 \qquad Bi-2-2 \qquad 0.03294 \pm 0.0005 \\ 0.0533 \pm 0.0017 \qquad 0.311 \pm 0.013 \qquad 2.90.1 \pm 9.6 \qquad 2.75 \pm 15 \qquad 8.38 \qquad 0.38 \qquad Bi-2-2 \qquad 0.03294 \pm 0.0005 \\ 0.0231 \pm 0.0017 \qquad 0.311 \pm 0.013 \qquad 2.90.1 \pm 9.6 \qquad 3.94 \pm 14 \qquad 8.99 \qquad 0.35 \qquad Bi-2-4 \qquad 0.0211 \pm 0.0005 \\ 0.0231 \pm 0.0010 \qquad 0.229 \pm 0.012 \qquad 1.793.2 \pm 52.4 \qquad 1837 \pm 8.2 \qquad 9.76 \qquad 0.62 \qquad Bi-2-4 \qquad 0.0211 \pm 0.0005 \\ 0.0233 \pm 0.0000 \qquad 0.229 \pm 0.012 \qquad 1.793.2 \pm 52.4 \qquad 1837 \pm 8.2 \qquad 9.76 \qquad 0.62 \qquad Bi-2-6 \qquad 0.0278 \pm 0.0005 \\ 0.0291 \pm 0.0010 \qquad 0.229 \pm 0.012 \qquad 1641.8 \pm 31.8 \qquad 1.752 \pm 4.7 \qquad 93.6 \qquad 0.35 \qquad Bi-2-8 \qquad 0.0373 \pm 0.0005 \\ 0.0295 \pm 0.0000 \qquad 0.208 \pm 0.012 \qquad 184.1 \pm 4.0 \qquad 2.01 \pm 11 \qquad 93.3 \qquad 0.27 \qquad Bi-2-1 \qquad 0.0379 \pm 0.0005 \\ 0.0298 \pm 0.0000 \qquad 0.208 \pm 0.012 \qquad 184.1 \pm 5.2 \qquad 2.62 \pm 11 \qquad 98.5 \qquad 0.21 \qquad Bi-2-1 \qquad 0.0234 \pm 0.0005 \\ 0.0293 \pm 0.0000 \qquad 0.211 \pm 0.014 \qquad 186.4 \pm 4.3 \qquad 1.94 \pm 13 \qquad 95.9 \qquad 0.35 \qquad Bi-2-15 \qquad 0.0345 \pm 0.0006 \\ 0.0408 \pm 0.0000 \qquad 0.211 \pm 0.014 \qquad 186.4 \pm 4.3 \qquad 1.94 \pm 13 \qquad 95.9 \qquad 0.35 \qquad Bi-2-15 \qquad 0.0345 \pm 0.0006 \\ 0.0408 \pm 0.0000 \qquad 0.211 \pm 0.014 \qquad 186.4 \pm 4.3 \qquad 1.94 \pm 13 \qquad 95.9 \qquad 0.35 \qquad Bi-2-15 \qquad 0.0345 \pm 0.0006 \\ 0.0493 \pm 0.0000 \qquad 0.217 \pm 0.0009 \qquad 1.94 \pm 3.8 \qquad 1.94 \pm 13 \qquad 95.9 \qquad 0.35 \qquad Bi-2-17 \qquad 0.0345 \pm 0.0006 \\ 0.0493 \pm 0.0000 \qquad 0.217 \pm 0.0012 \qquad 1.94 \pm 13 \qquad 2.41 \pm 10 \qquad 75.5 \qquad 0.30 \qquad Bi-2-17 \qquad 0.0345 \pm 0.0005 \\ 0.0493 \pm 0.0000 \qquad 0.217 \pm 0.0012 \qquad 2.41 \pm 10 \qquad 2.51 \pm 0.0217 \qquad 0.0345 \pm 0.0006 \\ 0.0493 \pm 0.0000 \qquad 0.217 \pm 0.0012 \qquad 2.41 \pm 10 \qquad 2.41 \pm 10 \qquad 2.41 \pm 10 \qquad 2.41 \pm 10 \qquad 2.41 \pm 0.0012 \qquad 2.4$	1-1-75	$0.3821 \pm 0.0058$	$6.174 \pm 0.193$	2086.2 ± 31.5	$2001 \pm 63$	104.3	0.19	Bi-1-126	$0.0290 \pm 0.0006$	+	184,4 ± 3.7	203 ± 12	8'06	0.48
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	P-1-76	$0.0308 \pm 0.0006$	0.269 ± 0.014	195.3 ± 3.5	$242 \pm 13$	80.8	090	Bi-1-127	0.0298 = 0.0006	$0.279 \pm 0.014$	$189.0 \pm 3.7$	$250 \pm 12$	75.6	1.15
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-17	$0.0421 \pm 0.0015$	$0.452 \pm 0.040$	265.5 ± 9.3	$378 \pm 33$	20.2	0.59	Bi-1-128	$0.0224 \pm 0.0005$	$0.312 \pm 0.020$	142.9 ± 3.4	276 ± 18	51.8	0
0.0459 ± 0.00014 0.507 ± 0.029 283.9 ± 8.7 417 ± 24 68.2 1.29 Sandstone of the middle part of 0.0569 ± 0.0107 5.899 ± 0.0213 ± 0.034 31.3 ± 10.4 450 ± 28 7 10.3 0.26 Bi-2-1 0.3873 ± 0.0065 0.0587 ± 0.0017 0.538 ± 0.034 31.3 ± 10.4 450 ± 28 7 7.0 0.78 Bi-2-2 0.0384 ± 0.0007 0.0537 ± 0.0017 0.311 ± 0.017 230.2 ± 6.9 275 ± 15 83.8 0.38 Bi-2-3 0.0292 ± 0.0009 0.2046 ± 0.0011 0.311 ± 0.017 230.2 ± 6.9 275 ± 15 83.8 0.38 Bi-2-3 0.0292 ± 0.0009 0.207 ± 0.0009 0.207 ± 0.0009 0.207 ± 0.0009 0.208 ± 0.017 230.2 ± 5.2 4 2 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1-1-78	$0.3503 \pm 0.0101$	5,434 ± 0,225	1935.9 ± 55.6	82 ± 0681	102,4	0.27					A STATE OF THE STA		
$0.3699 \pm 0.0107 \qquad 5.899 \pm 0.251 \qquad 2028.8 \pm 5.86 \qquad 1961 \pm 83 \qquad 1035 \qquad 0.26 \qquad Bi-2-1 \qquad 0.3873 \pm 0.0065 \qquad 6.645 \pm 0.0357 \pm 0.00107 \qquad 0.3528 \pm 0.037 \pm 0.0017 \qquad 0.3528 \pm 0.037 \pm 0.0017 \qquad 0.3528 \pm 0.037 \equiv 0.0017 \qquad 0.3528 \pm 0.0017 \qquad 0.3528 \pm 0.0017 \qquad 0.3528 \pm 0.0017 \qquad 0.3529 \pm 0.0017 \qquad 0.3529 \pm 0.0017 \qquad 0.3529 \pm 0.0017 \qquad 0.371 \pm 0.0017 \qquad 0.371 \pm 0.0017 \qquad 0.3529 \pm 0.0017 \qquad 0.029 \pm 0.0019 \qquad 0.0299 \pm 0.0019 \qquad 0.2599 \pm 0.017 \qquad 0.0291 \pm 0.0009 \qquad 0.14 \pm 0.0019 \qquad 0.259 \pm 0.0119 \qquad 0.0291 \pm 0.00019 \qquad 0.259 \pm 0.012 \qquad 0.248 \pm 1.0019 \qquad 0.2591 \pm 0.0019 \qquad 0.2591 \pm 0.0019 \qquad 0.248 \pm 1.0019 \qquad 0.2591 \pm 0.0019 \qquad 0.248 \pm 1.0019 \qquad 0.2591 \pm 0.0019 \qquad 0.248 \pm 1.0019 \qquad 0.248 \pm 0.0019 \qquad 0.249 \pm 0.0009 \qquad 0.249 \pm 0.0019 \qquad $	1-1-19	$0.0450 \pm 0.0014$	$0.507 \pm 0.029$	283.9 ± 8.7	417 ± 24	68.2	1.29	Sand	stone of the middle par	of	Sec.	55.66" N, 133 48' 07.93" E	07.93" E)	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	08-1-9	$0.3699 \pm 0.0107$	5.899 ± 0.251	2028.8 ± 58.6	1961 ± 83	103.5	0.26	Bi-2-1	$0.3873 \pm 0.0065$	+1	2110,2 ± 35,3	2065 ± 58	102.2	0.36
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	18-1-1			331.3 ± 10.4	430 ± 28	77.0	0.78	Bi-2-2	$0.0384 \pm 0.0007$	111	$242.8 \pm 4.6$	$238 \pm 13$	101.9	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-82	0.0363 ± 0.0011	0.311 ± 0.017	230.2 ± 6.9	275 ± 1.5	83.8	0.38	Bi-2-3	$0.0292 \pm 0.0009$	+1	185.5 ± 5.6	193 ± 24	96.1	-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-83	0.0460 ± 0.0075	$0.411 \pm 0.033$	290.1 ± 9.6	349 ± 28	83.0	0.56	Bi-2-4	$0.0211 \pm 0.0005$	$0.155 \pm 0.012$	$134.8 \pm 3.0$	146 ± 12	92.0	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-84	$0.3207 \pm 0.0094$	5.103 ± 0.228	$1793.2 \pm 52.4$	1837 ± 82	97.6	0.62	BI-2-5	$0.0268 \pm 0.0006$	+1	170,4 ± 4.1	180 ± 16	94.4	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-85	$0.0331 \pm 0.0010$	$0.259 \pm 0.015$	$210.0 \pm 6.3$	234 ± 14	6.68	0.37	Bi-2-6	0.0270 ± 0.0005	#	171.9 ± 3.5	225 ± 12	16.4	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-80	$0.0283 \pm 0.0006$	$0.269 \pm 0.012$	$179.9 \pm 3.7$	$242 \pm 11$	74.4	0.63	Bi-2-7	$0.3079 \pm 0.0035$	+1	1730.4 ± 19.7	$1773 \pm 42$	9.76	o'
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1-1-87	$0.2901 \pm 0.0056$	$4.630 \pm 0.124$	1641.8 ± 31.8	1755 ± 47	93.6	0.35	Bi-2-8	$0.0373 \pm 0.0009$	-11	235.8 ± 5.4	$237 \pm 23$	1.66	0
0.0389 ± 0.0010 0.285 ± 0.026 246.3 ± 6.6 255 ± 23 96.7 0,79 Bi;2-10 0.0302 ± 0.0005 0.202 ± 0.0005 0.174 ± 0.009 171.3 ± 3.6 16.2 ± 8 105.4 0.43 Bi;2-11 0.3425 ± 0.0049 5.372 ± 0.0048 ± 0.0008 0.295 ± 0.012 258.1 ± 5.2 26.2 ± 11 98.5 0.21 Bi;2-13 0.2834 ± 0.0032 4.472 ± 0.0048 ± 0.0048 ± 0.0041 186.4 ± 4.3 194 ± 48 96.5 0.20 Bi;2-14 0.0255 ± 0.0006 0.216 ± 0.0004 0.207 ± 0.0009 0.275 ± 0.0006 0.217 ± 0.009 187.5 ± 3.8 1921 ± 48 96.5 0.26 Bi;2-14 0.0271 ± 0.0004 0.207 ± 0.0004 0.207 ± 0.0009 0.278 ± 0.025 ± 0.0006 0.217 ± 0.009 187.5 ± 3.8 199 ± 8 94.2 0.35 Bi;2-15 0.1513 ± 0.007 2.732 ± 0.0483 ± 0.0009 0.378 ± 0.022 303.9 ± 5.8 326 ± 19 93.3 0.81 Bi;2-15 0.0346 ± 0.0008 0.260 ± 0.0285 ± 0.0009 0.278 ± 0.001 181.5 ± 3.1 241 ± 10 75.5 0.30 Bi;2-17 0.3154 ± 0.0055 4.963 ± 0.0009	98-1-9	$0.0295 \pm 0.0006$	$0.218 \pm 0.012$	$187.1 \pm 4.0$	201 ± 11	93.3	0.27	Bi-2-9	$0.0297 \pm 0.0005$	$0.204 \pm 0.013$	$188.8 \pm 3.2$	189 ± 12	100.2	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	68-1-9	$0.0389 \pm 0.0010$	$0.285 \pm 0.026$	246.3 = 6.6	255 ± 23	2.96	0.79	Bi-2-10	$0.0302 \pm 0.0005$	+1	$191.9 \pm 3.4$	$187 \pm 13$	102.7	0.42
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	06-1-0	$0.0269 \pm 0.0006$	0.174 ± 0.009	171.3 ± 3.6	162 ± 8	105.4	0.43	Bi-2-11	0.3425 ± 0.0040	# 1	1898.8 ± 22.0	# .	101.0	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16-1-8	$0.0408 \pm 0.0008$	$0.295 \pm 0.012$	258.1 ± 5.2	262 ± 11	686	0.21	Bi-2-12	+1.	$4.472 \pm 0.107$	$1608.4 \pm 18.4$	1726 ± 41	93.2	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	8-1-92	$0.0293 \pm 0.0007$	0.211 ± 0.014	186.4 ± 4.3	194 ± 13	95.9	0.39	Bi-2-13	#	44	168.8 ± 3.6	198 ± 17	85.0	0.75
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11-1-93	$0.3334 \pm 0.0064$	5.635 ± 0.140	$1855.1 \pm 35.8$	1921 ± 48	6.96	0.26	Bi-2-14	91	#	$172.3 \pm 2.2$	191 ± 7	90.1	0
$0.0483 \pm 0.0009 \qquad 0.378 \pm 0.022 \qquad 303.9 \pm 5.8 \qquad 326 \pm 19 \qquad 93.3 \qquad 0.81 \qquad \text{Bi-2-16} \qquad 0.0346 \pm 0.0008 \qquad 0.266 \pm 0.0008 \qquad 0.0266 \pm 0.0009 \qquad 0.0266 \pm 0.0009 \qquad 0.0267 \pm 0.011 \qquad 1.81.5 \pm 3.1 \qquad 2.41 \pm 10 \qquad 75.5 \qquad 0.30 \qquad \text{Bi-2-17} \qquad 0.3154 \pm 0.0055 \qquad 4.963 \pm 0.0059 \qquad 0.00009 \qquad 0$	1-1-94	$0.0295 \pm 0.0006$	$0.217 \pm 0.009$	187.6 ± 3.8	199 ± 8	94.2	0.35	Bi-2-15	++	+	908.2 ± 10.4	$1337 \pm 32$	67.9	0
$0.0286 \pm 0.0005$ $0.267 \pm 0.011$ $181.5 \pm 3.1$ $2.41 \pm 10$ $75.5$ $0.30$ $18.2-17$ $0.3154 \pm 0.0055$ $4.963 \pm 0.005$	31-1-95	$0.0483 \pm 0.0009$	0.378 ± 0.022	303.9 ± 5.8		93.3	0.81	Bi-2-16	$0.0346 \pm 0.0008$	#	$219.1 \pm 5.0$	235 ± 18	93.4	0.56
	96-1-1	$0.0286 \pm 0.0005$	$0.267 \pm 0.011$	181.5 ± 3.1		75.5	0.30	Bi-2-17	$0.3154 \pm 0.0055$	+1	$1767.2 \pm 30.7$	#	97.5	Ö
0.0288 ± 0.0005 0.251 ± 0.011 182.8 ± 3.1 227 ± 10 80.5 0.63 Bi-2-18 0.0309 ± 0.0010 0.221 ±	Bi-1-97	$0.0288 \pm 0.0005$	$0.251 \pm 0.011$	44		80.5	0.63	Bi-2-18	$0.0309 \pm 0.0010$	1.0	$196.2 \pm 6.2$	$203 \pm 27$	9.96	0
	06-1-10	0.0000 = 0.0000	10.00 to 10.00 to 10.00	13 LO H 4.0		- The same of the								

Bi-2-20	Ω <sub>852</sub> /9d <sub>902</sub>	O 552/9d Lot	206Pb/238U age (Ma)	20'Pb/235U age (Ma)	%conc	Th/U	Grain	$\Omega_{8E}/4d_{500}$	107Pb/235U	Ma)	(Ma)	%conc	Th/U
1000	$0.3020 \pm 0.0051$	4.687 ± 0,115	1701.0 ± 28.5	+0.	96,4	0.74	Bi-2-71	#	$0.163 \pm 0.014$	41	+	101.0	0.70
17-7-1	$0.2818 \pm 0.0047$	$4.367 \pm 0.105$	$1600.6 \pm 26.7$		93.8	0.21	Bi-2-72	#	#	#	150 ± 14	91.8	0.67
Bi-2-22	$0.0300 \pm 0.0008$	$0.231 \pm 0.021$	$190.9 \pm 4.8$	211 ± 19	506	69.0	Bi-2-73	#	$0.181 \pm 0.021$	$172.7 \pm 6.8$	#	102,0	0.45
Bi-2-23	0.0304 ± 0.0007	0.204 ± 0.016	192.8 ± 4.3	189 ± 15	102.1	1.16	Bi-2-74	#	Ħ.	173.0 ± 5.8	179 ± 10	96.5	0.35
Bi-2-24	$0.0306 \pm 0.0007$	$0.195 \pm 0.017$	194.3 ± 4.6		97.01	0.56	Bi-2-75	#	+	174.4 ± 6.1	+1	666	0.41
Bi-2-25	$0.0230 \pm 0.0005$	$0.175 \pm 0.014$	146.9 ± 3.5		868	0.97	Bi-2-76	+1	41	135.1 ± 4.7	+1	108.0	0.52
81-2-26	$0.1873 \pm 0.0032$	#	1107.0 ± 19.1		80.1	0.37	Bi-2-77	41	+	#	2208 ± 90	8.66	0.49
Bi-2-27	$0.0299 \pm 0.0007$	$0.381 \pm 0.022$	189.9 ± 4.1	+	57.9	0.58	Bi-2-78	#	#	$174.7 \pm 6.0$	# .	94.9	0.42
Bi-2-28	$0.3355 \pm 0.0055$	$5.226 \pm 0.127$	$1864.9 \pm 30.7$		100.4	0.12	Bi-2-79	-11	#	#	$232 \pm 20$	84.2	0.96
Bi-2-29	$0.0384 \pm 0.0008$	$0.266 \pm 0.019$	242,9 ± 5.3		101.5	0.67	Bi-2-80	#	#	$175.2 \pm 6.1$	169 ± 12	103.5	0.53
Bi-2-30	$0.0309 \pm 0.0007$	$0.221 \pm 0.015$	$196.1 \pm 4.2$	$203 \pm 14$	6.7	0.24	Bi-2-81	+	$0.190 \pm 0.019$	$172.9 \pm 6.5$	$177 \pm 18$	6.79	0,12
Bi-2-31	$0.0489 \pm 0.0019$	$0.346 \pm 0.061$	$308.0 \pm 11.9$	-8	102.0	0.53	Bi-2-82	+1	#	$249,3 \pm 8.9$	$257 \pm 23$	97.1	0.65
Bi-2-32	$0.3479 \pm 0.0061$	5.425 ± 0.171	1924.7 ± 33.9	1889 ± 60	6.101	0.41	Bi-2-83	+6	+0	$173.4 \pm 5.5$	309 ± 15	26.1	0.37
Bi-2-33	0.0282 ± 0.0007	$0.203 \pm 0.012$	179.3 ± 4.6	188 ± 11	95.4	0.45	Bi-2-84	$0.0274 \pm 0.0009$	$0.193 \pm 0.013$	174.3 ± 5.8	179 ± 12	97.3	0.43
Bi-2-34	$0.3596 \pm 0.0088$	5.560 ± 0.212	1980.4 ± 48.3	1910 ± 73	103.7	0.42	Bi-2-85	41	31	177.5 ± 5.7	195 ± 11	6'06	0.7
Bi-2-35	$0.0285 \pm 0.0007$	0.193 ± 0.012	181.3 ± 4.7	$179 \pm 11$	101.2	0.37	Bi-2-86	$0.3338 \pm 0.0107$	+	$1856.9 \pm 59.8$	1857 ± 88	100.0	0.79
Bi-2-36	$0.0504 \pm 0.0019$	0.381 ± 0.052	316.8 ± 11.9	328 ± 45	7.96	080	Bi-2-87	0.0381 ± 0.0013	-11	241.0 ± 8.1	315 ± 21	76.5	0.48
Bi-2-37	$0.4079 \pm 0.0095$	8.678 ± 0.268	2205.2 ± 51.6	2305 ± 71	7.56	0.50	Bi-2-88	$0.0294 \pm 0.0010$	40	$187.1 \pm 6.3$	$190 \pm 14$	98.6	0
Bi-2-38	$0.0322 \pm 0.0009$	$0.284 \pm 0.021$	204.3 ± 5.8	254 ± 19	80.5	99.0	Bi-2-89	$0.0279 \pm 0.0009$	4	$177.3 \pm 5.8$	185 ± 11	1.96	0.33
Bi-2-39	$0.4530 \pm 0.0109$	$9.845 \pm 0.336$	2408.6 ± 57.8	2420 ± 83	99.5	0.52	Bi-2-90	$0.0329 \pm 0.0014$	4	208.4 ± 8.8	237 ± 26	88.0	0.75
Bi-2-40	$0.3437 \pm 0.0081$	5,367 ± 0.174	1904.2 ± 44.9	1880 ± 61	101.3	0.29	Bi-2-91	$0.0272 \pm 0.0010$	4	$172.8 \pm 6.4$	177 ± 12	9.7.6	0.59
Bi-2-41	$0.3268 \pm 0.0078$	5,163 ± 0,174	1822.6 ± 43.3	1846 ± 62	7.86	0,23	Bi-2-92	$0.2588 \pm 0.0092$	$4.131 \pm 0.180$	1483.8 ± 52.8	1660 ± 72	4.68	0.31
Bi-2-42	$0.3579 \pm 0.0059$	$5.660 \pm 0.177$	1972.0 ± 32.4		102.4	0.10	Bi-2-93	#	$0.247 \pm 0.018$	222.1 ± 8.3	$224 \pm 16$	1.66	0.60
Bi-2-43	$0.2143 \pm 0.0036$	3.250 ± 0.108	1251.6 ± 21.0	1469 ± 49	85.2	0.13	Bi-2-94	$0.0259 \pm 0.0010$	$0.176 \pm 0.013$	$164.7 \pm 6.2$	164 ± 12	100.3	0.39
Bi-2-44	$0.0238 \pm 0.0005$	$0.154 \pm 0.010$	$151.6 \pm 3.0$	146 ± 9	104.0	0.33	Bi-2-95	$0.0282 \pm 0.0010$	$0.198 \pm 0.013$	$179.5 \pm 6.6$	184 ± 12	9.76	0.30
Bi-2-45	$0.4489 \pm 0.0074$	$9.610 \pm 0.300$	$2390.2 \pm 39.5$	2398 ± 75	7.66	0.24	Bi-2-96	$0.0268 \pm 0.0008$	$0.189 \pm 0.013$	$170.8 \pm 5.3$	$176 \pm 12$	0.7.0	0.71
Bi-2-46	$0.3456 \pm 0.0057$	5,421 ± 0.173	1913.6 ± 31.7	1888 ± 60	1013	0.54	Bi-2-97	+1	$0.149 \pm 0.018$	128,1 ± 4.7	141 ± 17	91.1	1,12
Bi-2-47	$0.0291 \pm 0.0006$	$0.224 \pm 0.013$	$185.2 \pm 3.7$	+1	500	0.37	Bi-2-98	44.	$0.277 \pm 0.015$	254.9 ± 7.5	$248 \pm 14$	102.6	0.12
Bi-2-48	$0.3198 \pm 0.0053$	5.010 ± 0.158	$1789.0 \pm 29.5$	1821 ± 57	98.2	0.12	Bi-2-99	#	13.250 ± 0.488	2535.3 ± 72.2	2698 ± 99	94.0	0.36
Bi-2-49	$0.0285 \pm 0.0007$	$0.194 \pm 0.016$	181.3 ± 4.2		100.7	0.45	Bi-2-100	#	$0.234 \pm 0.015$	$221.7 \pm 6.7$	213 ± 14	103.9	0.3
Bi-2-50	$0.0212 \pm 0.0005$	$0.159 \pm 0.014$	$135.5 \pm 3.4$	+	90.2	0.65	Bi-2-101	41	+1 -	$163.1 \pm 4.9$	$156 \pm 10$	104.2	0.40
Bi-2-51	$0.0287 \pm 0.0010$	$0.211 \pm 0.019$	$182.2 \pm 6.5$	+11	93.7	0,45	Bi-2-102	+1	41	$172.1 \pm 5.4$	185 ± 14	92.9	0.31
Bi-2-52	0.1944 ± 0.0062	2.915 ± 0,136	1145.0 ± 36.4		82.6	0.57	Bi-2-103	+1	#	1827.3 ± 51.6	$1848 \pm 67$	6.86	0.23
Bi-2-53	$0.2714 \pm 0.0085$	4.238 ± 0.181	1548.1 ± 48.5	+	92.1	0.48	Bi-2-104	#	$0.178 \pm 0.010$	164.0 ± 4.8	6 = 991	986	0
Bi-2-54	$0.2984 \pm 0.0093$	4.684 ± 0.191	1683.2 ± 52.3	#	95.4	0.12	Bi-2-105	#	$0.155 \pm 0.016$	140.0 ± 5.2	147 ± 15	95.5	0.38
Bi-2-55	$0.0460 \pm 0.0018$	$0.346 \pm 0.043$	$289.8 \pm 11.5$	302 ± 37	96.1	0.56	Bi-2-106	#	+1	$173.8 \pm 6.5$	$61 \pm 681$	92.1	0.51
Bi-2-56		$0.199 \pm 0.012$	$188.2 \pm 6.1$	+1	102,2	0.24	Bi-2-107	+#	0,240 ± 0.017	137.2 ± 4.8	219 ± 15	62.7	0.99
Bi-2-57	$0.1748 \pm 0.0057$	$2.492 \pm 0.130$	1038,5 ± 33.8	1270 ± 66	81.8	0.38	Bi-2-108	#	$0.173 \pm 0.014$	$172.8 \pm 6.0$	162 ± 13	8'901	0.45
Bi-2-58	$0.0286 \pm 0.0013$	$0.189 \pm 0.017$	$181.6 \pm 8.2$	$176 \pm 16$	103.3	0.42	Bi-2-109	#	$0.139 \pm 0.015$	$139.4 \pm 5.2$	132 ± 14	105.2	0.47
Bi-2-59	$0.4931 \pm 0.0208$	11.868 ± 0.576	2584.3 ± 109.2	#	9.66	0.53	Bi-2-110	#	# .	$137.5 \pm 5.3$	#	106.1	0.59
Bi-2-60		$3.724 \pm 0.189$	1405.5 ± 59.7		89.2	0.22	Bi-2-111	# .	#	$161.0 \pm 4.7$	$182 \pm 10$	88.3	0.2
Bi-2-61	0.2503 ± 0.0106	$3.851 \pm 0.194$	1440.1 ± 61.1	# -	89.8	0.63	Bi-2-112	+ -	# .	# .	149 ± 21	97.5	0.61
Bi-2-62	$0.3067 \pm 0.0130$	4.786 ± 0.235	1724.3 ± 72.9		1.96	0.43	Bi-2-113	#1 -	#	41	2092 ± 63	7.68	0.32
B1-2-63	$0.0290 \pm 0.0013$	$0.204 \pm 0.014$	$184.3 \pm 8.0$		67.6	0.65	Bi-2-114	#	#	$250.4 \pm 7.7$	245 ± 18	102.0	1.0
Bi-2-64	0.0340 ± 0.0015	0.235 ± 0.021	215.7 ± 9.7		100.7	0.61	Bi-2-115	# .	# :	44	1898 ± 64	0.101	0.0
Bi-2-65	$0.0299 \pm 0.0013$	$0.215 \pm 0.013$	$190.0 \pm 8.1$		0.96	0.21	Bi-2-116	91	#(	$177.0 \pm 5.4$	182 ± 12	97.3	0.47
Bi-2-66	$0.0217 \pm 0.0009$	$0.150 \pm 0.012$	$138.5 \pm 5.7$	142 ± 11	9.7.6	0.36	Bi-2-117	+1.	#	#1	$199 \pm 15$	92.8	0.51
B)-2-67	$0.0274 \pm 0.0011$	0.187 ± 0.017	174.0 ± 7.3		100.2	0.34	Bi-2-118	+1	#		1622 ± 59	93.0	0
B1-2-68	0.3358 ± 0.0130	5.337 ± 0.245	1866.5 ± 72.4	++ -	9.66	0.12	Bi-2-119	#	# .	44 .	2623 ± 87	66.3	0.54
Bi-2-69	$0.0264 \pm 0.0011$	$0.177 \pm 0.011$	$168.2 \pm 6.7$	166 ± 11	101.5	0.17	Bi-2-120	$0.2562 \pm 0.0044$	4.019 ± 0.140	1470.2 ± 25.1	1638 ± 57	88.8	0.37

TABLE 1. (Continued)

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0.3091 ± 0.00044		~	Ö	8.96	50.8 1803 ± 61 96.8
0.0466 $\pm$ 0.0020         0.419 $\pm$ 0.050         29.3 $\pm$ 12.8           0.0588 $\pm$ 0.0014         0.679 $\pm$ 0.056         20.36         3.8.8           0.0440 $\pm$ 0.0014         0.679 $\pm$ 0.035         277.5 $\pm$ 9.5           0.0440 $\pm$ 0.0019         0.344 $\pm$ 0.035         277.5 $\pm$ 9.5           0.0440 $\pm$ 0.0019         0.344 $\pm$ 0.035         277.5 $\pm$ 9.5           0.0482 $\pm$ 0.0019         0.344 $\pm$ 0.036         277.5 $\pm$ 9.5           0.0482 $\pm$ 0.0019         0.344 $\pm$ 0.030         272.6 $\pm$ 1.219           0.0482 $\pm$ 0.0010         0.234 $\pm$ 0.03         204.2 $\pm$ 1.219           0.0482 $\pm$ 0.0011         0.344 $\pm$ 0.03         30.2 $\pm$ 1.14           0.0522 $\pm$ 0.0010         0.234 $\pm$ 0.05         30.2 $\pm$ 1.14           0.0252 $\pm$ 0.0010         0.244 $\pm$ 0.03         30.2 $\pm$ 1.14           0.0254 $\pm$ 0.0017         0.344 $\pm$ 0.03         30.2 $\pm$ 1.14           0.0258 $\pm$ 0.0000         0.310 $\pm$ 0.03         20.4 $\pm$ 1.5           0.0480 $\pm$ 0.0012         0.347 $\pm$ 0.016         0.347 $\pm$ 0.03         20.3 $\pm$ 2.1           0.0480 $\pm$ 0.0013         0.327 $\pm$ 0.02         20.3 $\pm$ 2.8 $\pm$ 3.7           0.0426 $\pm$ 0.0016         0.320 $\pm$ 0.02         20.3 $\pm$ 2.8 $\pm$ 3.7           0.0426 $\pm$ 0.0019         0.320 $\pm$ 0.02         20.23		9		± 32 98.4	11.5 295 ± 32 98.4
$0.0588 \pm 0.0014 \qquad 0.679 \pm 0.036 \qquad 36.83 \pm 8.8 \\ 0.04401 \pm 0.00174 \qquad 0.366 \pm 0.035 \qquad 277.78 \pm 9.1 \\ 0.04401 \pm 0.00174 \qquad 0.366 \pm 0.035 \qquad 277.78 \pm 9.1 \\ 0.04473 \pm 0.00194 \qquad 0.394 \pm 0.035 \qquad 277.56 \pm 8.3 \\ 0.0452 \pm 0.0019 \qquad 0.394 \pm 0.046 \qquad 297.9 \pm 12.0 \\ 0.0432 \pm 0.00013 \qquad 0.341 \pm 0.033 \qquad 272.6 \pm 8.3 \\ 0.0491 \pm 0.0017 \qquad 0.364 \pm 0.064 \qquad 309.2 \pm 10.4 \\ 0.0292 \pm 0.0000 \qquad 0.224 \pm 0.063 \qquad 204.2 \pm 6.7 \\ 0.0491 \pm 0.0017 \qquad 0.364 \pm 0.064 \qquad 309.2 \pm 10.4 \\ 0.0295 \pm 0.0000 \qquad 0.214 \pm 0.078 \qquad 302.4 \pm 15.5 \\ 0.0398 \pm 0.0000 \qquad 0.310 \pm 0.076 \qquad 302.4 \pm 15.5 \\ 0.0480 \pm 0.0017 \qquad 0.367 \pm 0.076 \qquad 302.4 \pm 15.5 \\ 0.0487 \pm 0.0012 \qquad 0.310 \pm 0.027 \qquad 226.9 \pm 9.3 \\ 0.0459 \pm 0.0013 \qquad 0.310 \pm 0.027 \qquad 226.9 \pm 9.3 \\ 0.0459 \pm 0.0019 \qquad 0.310 \pm 0.027 \qquad 226.3 \pm 7.7 \\ 0.0459 \pm 0.0013 \qquad 0.329 \pm 0.020 \qquad 289.3 \pm 8.3 \\ 0.0459 \pm 0.0019 \qquad 0.329 \pm 0.020 \qquad 289.3 \pm 8.3 \\ 0.0459 \pm 0.0019 \qquad 0.375 \pm 0.029 \qquad 229.76 \pm 8.9 \\ 0.0459 \pm 0.0019 \qquad 0.375 \pm 0.029 \qquad 2245.2 \pm 57.5 \\ 0.0471 \pm 0.0014 \qquad 0.375 \pm 0.029 \qquad 435.4 \pm 12.1 \\ 0.0436 \pm 0.0019 \qquad 0.375 \pm 0.029 \qquad 249.76 \pm 0.00 \\ 0.0448 \pm 0.0011 \qquad 0.311 \pm 0.031 \qquad 1788.0 \pm 27.6 \\ 0.0418 \pm 0.0011 \qquad 0.296 \pm 0.029 \qquad 224.3 \pm 6.7 \\ 0.0418 \pm 0.0011 \qquad 0.296 \pm 0.029 \qquad 224.3 \pm 6.7 \\ 0.0418 \pm 0.0011 \qquad 0.296 \pm 0.029 \qquad 224.3 \pm 6.7 \\ 0.0418 \pm 0.0011 \qquad 0.296 \pm 0.029 \qquad 224.3 \pm 6.7 \\ 0.0418 \pm 0.0011 \qquad 0.296 \pm 0.029 \qquad 1980.7 \pm 48.6 \\ 0.04418 \pm 0.0011 \qquad 0.296 \pm 0.029 \qquad 1980.7 \pm 48.6 \\ 0.04419 \pm 0.0011 \qquad 0.342 \pm 0.029 \qquad 224.3 \pm 6.7 \\ 0.04419 \pm 0.0011 \qquad 0.342 \pm 0.029 \qquad 224.3 \pm 6.7 \\ 0.04419 \pm 0.0011 \qquad 0.342 \pm 0.033 \qquad 224.3 \pm 8.8 \\ 0.04419 \pm 0.0014 \qquad 0.342 \pm 0.033 \qquad 224.3 \pm 8.8 \\ 0.0431 \pm 0.0014 \qquad 0.347 \pm 0.033 \qquad 224.2 \pm 8.8 \\ 0.0431 \pm 0.0014 \qquad 0.347 \pm 0.033 \qquad 222.2 \pm 8.8 \\ 0.0431 \pm 0.0014 \qquad 0.327 \pm 0.033 \qquad 222.2 \pm 8.8 \\ 0.0431 \pm 0.0014 \qquad 0.327 \pm 0.033 \qquad 222.2 \pm 8.8 \\ 0.0431 \pm 0.0014 \qquad 0.0231 \pm 0.033 \qquad 222.2 \pm 8.8 \\ 0.0431 \pm 0.0014 \qquad 0.0232 \qquad 222.2 \pm 8.8 \\ 0.0431 \pm 0.0014 \qquad 0.0232 \qquad 222.2 \pm 2.2 \\ 0.0449 \pm 0.0014 \qquad 0.0232 \qquad 222.2 \pm 2.2 \\ 0.0449 \pm 0.0014 \qquad 0.0232 \qquad 222.2 \pm 2.2 \\ 0.0449 \pm 0.0014 \qquad 0.0232 \qquad 222.2 \pm 2.2 \\ 0.0449 \pm 0.0014 \qquad 0.0232 \qquad 22$		9	Ē	± 16 104.1	9,3 264 ± 16 104,1
0.0440 ± 0.0014 0.366 ± 0.035 2778 ± 9.1 0.0440 ± 0.0015 0.344 ± 0.035 2777.5 ± 9.5 0.0446 ± 0.0019 0.344 ± 0.035 2777.5 ± 9.5 0.0446 ± 0.0019 0.341 ± 0.035 277.5 ± 9.5 0.0482 ± 0.0019 0.341 ± 0.030 277.5 ± 9.5 0.0482 ± 0.0013 0.344 ± 0.046 297.9 ± 12.0 0.0480 ± 0.0035 0.342 ± 0.067 302.1 ± 21.9 0.0425 ± 0.0010 0.334 ± 0.067 302.1 ± 21.9 0.0425 ± 0.0001 0.324 ± 0.054 309.2 ± 10.4 0.0255 ± 0.0009 0.316 ± 0.075 10.0480 ± 0.0029 0.3492 ± 0.0010 0.324 ± 0.075 21.8 ± 5.7 0.0480 ± 0.0011 0.387 ± 0.035 286.9 ± 9.3 0.0426 ± 0.0015 0.380 ± 0.025 286.9 ± 9.3 0.0426 ± 0.0015 0.320 ± 0.027 286.9 ± 9.3 0.0426 ± 0.0011 0.327 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.0424 ± 0.0012 0.320 ± 0.037 286.9 ± 9.3 0.043 ± 0.0010 0.331 ± 0.031 128.0 ± 8.9 0.043 ± 0.0010 0.331 ± 0.031 128.0 ± 8.9 0.043 ± 0.0010 0.341 ± 0.036 ± 0.020 0.344 ± 0.0016 0.344 ± 0.036 0.344 ± 0.0016 0.344 ± 0.036 0.344 ± 0.006 0.341 ± 0.006 0.344 ± 0.006 0.341 ± 0.006 0.344 ± 0.009 0.341 ± 0.006 0.341 ± 0.006 0.344 ± 0.0011 0.356 ± 0.039 0.341 ± 0.035 0.341 ± 0.035 0.341 ± 0.035 0.341 ± 0.035 0.341 ± 0.035 0.341 ± 0.035 0.341 ± 0.035 0.341 ± 0.006 0.341 ± 0.0014 0.337 ± 0.033 0.332 0.322 ± 8.8 0.0433 ± 0.0014 0.3337 ± 0.033 0.322 ± 0.033 0.332 0.322 ± 0.033 0.332 0.322 ± 0.033 0.332 0.0433 ± 0.0014 0.3337 ± 0.033 0.322 ± 0.033 0.332 0.0433 ± 0.0014 0.3337 ± 0.033 0.322 ± 0.033 0.332 0.0433 ± 0.0014 0.3337 ± 0.033 0.322 ± 0.033 0.332 0.0433 0.0014 0.3337 ± 0.033 0.332 0.322 ± 0.033 0.332 0.0433 0.0014 0.3337 ± 0.033 0.332 0.322 ± 0.033 0.332 0.0433 0.0014 0.3337 ± 0.033 0.332 0.322 ± 0.033 0.332 0.322 ± 0.033 0.332 0.332 0.332 0.332 0.332 0.332 0.332 0.333 0.3333 0.3333 0.3333 0.3333 0.3333 0.3333 0.3333 0.33		-	9	± 24 101.2	9.9 264 ± 24 101.2
0.0440 ± 0.0015 0.344 ± 0.035 277.5 ± 9.5 0.4554 ± 0.0019 10.005 ± 0.427 242.5 ± 15.0 0.0432 ± 0.0019 0.344 ± 0.035 277.5 ± 8.3 0.0432 ± 0.0019 0.344 ± 0.036 272.5 ± 8.3 0.0480 ± 0.0019 0.341 ± 0.030 272.5 ± 8.3 0.0480 ± 0.0010 0.234 ± 0.023 244.2 ± 6.7 0.0481 ± 0.0011 0.234 ± 0.023 244.2 ± 6.7 0.0481 ± 0.0017 0.234 ± 0.023 244.2 ± 6.7 0.0480 ± 0.0021 0.387 ± 0.076 302.4 ± 10.4 0.0295 ± 0.0009 0.310 ± 0.027 251.8 ± 5.7 0.0480 ± 0.0021 0.387 ± 0.035 288.9 ± 9.3 0.0426 ± 0.0015 0.387 ± 0.035 288.9 ± 9.3 0.0426 ± 0.0015 0.387 ± 0.035 288.9 ± 9.3 0.0426 ± 0.0015 0.389 ± 0.039 ± 0.0107 257.5 ± 7.5 0.0426 ± 0.0015 0.329 ± 0.027 288.3 ± 8.3 0.0426 ± 0.0019 0.329 ± 0.029 288.3 ± 8.3 0.0426 ± 0.0019 0.329 ± 0.039 24.5 ± 12.1 0.0426 ± 0.0019 0.375 ± 0.039 24.5 ± 12.1 0.0426 ± 0.0019 0.375 ± 0.039 24.5 ± 12.1 0.0426 ± 0.0019 0.375 ± 0.039 24.5 ± 12.1 0.0426 ± 0.0019 0.375 ± 0.039 24.5 ± 12.1 0.0426 ± 0.0019 0.375 ± 0.039 24.5 ± 12.1 0.0430 ± 0.0019 0.340 ± 0.031 1.0 0.015 1.0 0.338 ± 0.039 0.0441 ± 0.016 0.341 ± 0.016 0.341 ± 0.016 0.341 ± 0.039 0	D.47 F	~	101.8	± 17 101.8	197 ± 17 101.8
0.04564 ± 0.0104		-	٩	± 25 101.8	10.7 287 ± 25 101.8
0.04473 ± 0.001/9 0.394 ± 0.046 297.9 ± 12.0 0.04432 ± 0.0031 0.344 ± 0.030 272.6 ± 8.3 0.0482 ± 0.0031 0.344 ± 0.030 272.6 ± 8.3 0.0480 ± 0.0031 0.342 ± 0.063 20.42 ± 6.7 0.0480 ± 0.0017 0.364 ± 0.054 309.2 ± 10.4 0.0295 ± 0.0006 0.224 ± 0.054 309.2 ± 10.4 0.0295 ± 0.0004 0.234 ± 0.076 34.2 ± 6.7 0.0480 ± 0.0021 0.387 ± 0.076 30.24 ± 15.5 0.0480 ± 0.0001 0.387 ± 0.076 30.24 ± 15.5 0.0480 ± 0.0010 0.297 ± 0.035 26.8 ± 9.3 0.0450 ± 0.0010 0.207 ± 0.032 26.8 ± 9.3 0.0450 ± 0.0010 0.300 ± 0.030 26.8 ± 9.3 0.0450 ± 0.0010 0.320 ± 0.030 26.8 ± 9.3 0.0450 ± 0.0010 0.320 ± 0.030 26.017 267.5 ± 7.5 0.0450 ± 0.0010 0.320 ± 0.030 26.017 267.5 ± 7.5 0.0450 ± 0.0010 0.357 ± 0.039 20.017 267.5 ± 7.5 0.0450 ± 0.0010 0.375 ± 0.039 20.017 267.5 ± 7.5 0.0450 ± 0.0010 0.375 ± 0.039 20.010 0.375 ± 0.039 0.010 0.375 ± 0.039 0.010 0.375 ± 0.039 0.010 0.375 ± 0.039 0.010 0.375 ± 0.039 0.010 0.310 ± 0.311 ± 0.031 1.788 0 ± 2.76 0.0340 ± 0.0010 0.311 ± 0.031 1.788 0 ± 2.76 0.0340 ± 0.0010 0.341 ± 0.015 0.344 ± 0.015 0.344 ± 0.001 0.344 ± 0.0011 0.360 ± 0.039 11.89 0 ± 46.4 0.3587 ± 0.0039 0.344 ± 0.039 0.344 ± 0.0031 0.344 ± 0.039 0.344 ± 0.039 0.344 ± 0.0041 0.396 ± 0.039 0.344 ± 0.039 0.344 ± 0.031 0.344 ± 0.0011 0.364 ± 0.039 0.344 ± 0.039 0.344 ± 0.0011 0.344 ± 0.035 0.344 ± 0.039 0.344 ± 0.031 0.344 ± 0.031 0.344 ± 0.031 0.344 ± 0.031 0.344 ± 0.031 0.344 ± 0.031 0.344 ± 0.039 0.344 ±		~	9	± 32 107,7	16.5 433 ± 32 107,7
0.0432 ± 0.0013				± 16 103.3	7,4 200 ± 16 103.3
0.0480 ± 0.0035		9		± 26 106.6	10.9 272 ± 26 106.6
0.0432 ± 0.0010 0.234 ± 0.023 204.2 ± 6.7 0.0491 ± 0.0017 0.364 ± 0.054 309.2 ± 10.4 0.0255 ± 0.0004 0.212 ± 0.018 190.9 ± 26.9 0.0480 ± 0.0021 0.387 ± 0.076 30.2.4 ± 13.5 0.0480 ± 0.0021 0.387 ± 0.027 251.8 ± 5.7 0.0426 ± 0.0012 0.287 ± 0.035 268.9 ± 9.3 0.0426 ± 0.0013 0.389 ± 0.035 268.9 ± 9.3 0.0426 ± 0.0013 0.389 ± 0.030 268.6 ± 9.8 0.0426 ± 0.0013 0.389 ± 0.030 268.6 ± 9.8 0.0426 ± 0.0013 0.399 ± 0.017 267.5 ± 7.5 0.0428 ± 0.0010 0.399 ± 0.017 267.5 ± 7.5 0.0429 ± 0.0010 0.399 ± 0.034 300.4 ± 9.7 0.0699 ± 0.0019 0.375 ± 0.029 435.4 ± 12.1 0.0699 ± 0.0019 0.375 ± 0.029 435.4 ± 12.1 0.0491 ± 0.0019 0.375 ± 0.029 435.4 ± 12.1 0.0492 ± 0.0001 0.311 ± 0.031 1788.0 ± 27.6 0.0418 ± 0.0011 0.266 ± 0.230 11788.0 ± 27.6 0.0418 ± 0.0011 0.266 ± 0.029 264.3 ± 6.7 0.0418 ± 0.0011 0.266 ± 0.039 189.0 ± 46.4 0.3597 ± 0.0088 5.860 ± 0.036 1980.7 ± 48.6 0.0449 ± 0.0013 0.345 ± 0.035 264.3 ± 6.7 0.0494 ± 0.0013 0.345 ± 0.035 264.3 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 264.5 ± 8.8 0.0431 ± 0.0014 0.337 ± 0.033 204.5 ± 8.8 0.0431 ± 0.0014 0.0313 ± 0.035 27.2 ± 8.8		0		± 115 98.8	106.6 2185 ± 115 98.8
0.0491 ± 0.0017		_		± 23 95.9	16.6 346 ± 23 95.9
0.0295 ± 0.0006				₹ 66 100.9	93.0 1865 ± 99 100.9
0.3447 ± 0.0049 5.457 ± 0.188 1909.4 ± 26.9 0.0480 ± 0.0021 0.387 ± 0.076 30.24 ± 18.5 0.0398 ± 0.00029 0.310 ± 0.027 251.8 ± 5.7 0.0426 ± 0.0015 0.287 ± 0.032 268.9 ± 9.3 0.0426 ± 0.0016 0.300 ± 0.036 268.9 ± 9.3 0.0426 ± 0.0016 0.300 ± 0.036 268.9 ± 8.3 0.0426 ± 0.0016 0.300 ± 0.037 268.5 ± 8.3 0.0424 ± 0.0012 0.320 ± 0.037 267.5 ± 7.5 0.3949 ± 0.0106 6.666 ± 0.29 2145.5 ± 57.5 0.0477 ± 0.0019 0.575 ± 0.029 2145.5 ± 57.5 0.0699 ± 0.0019 0.575 ± 0.029 2145.5 ± 57.5 0.0477 ± 0.0019 0.575 ± 0.029 2145.5 ± 57.5 0.0477 ± 0.0019 0.575 ± 0.029 2145.2 ± 12.1 0.0477 ± 0.0019 0.575 ± 0.029 2145.2 ± 12.1 0.0499 ± 0.0010 0.311 ± 0.031 255.0 ± 6.2 0.3196 ± 0.0010 0.311 ± 0.031 255.0 ± 6.2 0.0418 ± 0.0010 0.264 ± 0.029 264.3 ± 6.7 0.0418 ± 0.0041 0.266 ± 0.029 264.3 ± 6.7 0.3288 ± 0.0086 0.241 ± 0.135 1822.4 ± 8.6 0.0419 ± 0.0013 0.342 ± 0.030 1980.7 ± 48.6 0.0419 ± 0.0014 0.337 ± 0.033 254.5 ± 8.8 0.0431 ± 0.0014 0.337 ± 0.033 27.2.2 ± 8.8 0.0431 ± 0.0014 0.337 ± 0.035	0.71 F		238.7	367 ± 51 238.7	367 ± 51
0.0480 ± 0.0021 0.387 ± 0.076 312.4 ± 13.5 0.0398 ± 0.0009 0.310 ± 0.027 251.8 ± 5.7 0.0426 ± 0.0012 0.287 ± 0.035 268.9 ± 9.3 0.0426 ± 0.0015 0.289 ± 0.032 268.9 ± 9.3 0.0426 ± 0.0013 0.329 ± 0.023 268.9 ± 9.3 0.0424 ± 0.0013 0.329 ± 0.020 289.3 ± 8.3 0.0424 ± 0.0012 0.320 ± 0.017 267.5 ± 7.5 0.3999 ± 0.0106 6.666 ± 0.039 20.655 ± 7.5 0.0499 ± 0.0109 0.375 ± 0.029 245.5 ± 7.5 0.0499 ± 0.0019 0.375 ± 0.029 45.5 ± 12.1 0.0497 ± 0.0019 0.375 ± 0.029 45.4 ± 12.1 0.0497 ± 0.0019 0.375 ± 0.029 27.0 ± 8.9 0.0403 ± 0.0019 0.375 ± 0.029 264.3 ± 6.7 0.0346 ± 0.0049 5.067 ± 0.251 1788.0 ± 27.6 0.0348 ± 0.0041 0.266 ± 0.029 264.3 ± 6.7 0.0288 ± 0.0086 0.241 ± 0.016 219.1 ± 3.7 0.0418 ± 0.0011 0.266 ± 0.029 264.3 ± 6.7 0.3288 ± 0.0080 5.309 ± 0.193 189.90 ± 46.4 0.3597 ± 0.0088 5.860 ± 0.030 1980.7 ± 48.6 0.0419 ± 0.0011 0.335 ± 0.035 264.5 ± 8.8 0.0431 ± 0.0014 0.337 ± 0.035 27.2. ± 8.8 0.0431 ± 0.0014 0.337 ± 0.035 27.2. ± 8.8			89.0	± 31	14.3 303 ± 31
0.0338 ± 0.0009			626	+ 34	14.5 276 ± 34
0.04373 ± 0.00112			93.7	₹ 28	20.8 380 ± 58
0.0426 ± 0.0015  0.287 ± 0.032  268.9 ± 9.3  0.0426 ± 0.0016  0.300 ± 0.036  268.6 ± 9.8  0.0459 ± 0.0016  0.320 ± 0.036  289.3 ± 8.3  0.0459 ± 0.0013  0.329 ± 0.037  267.5 ± 7.5  0.3949 ± 0.0106  6.666 ± 0.239  2145.5 ± 57.5  0.0477 ± 0.0016  6.666 ± 0.239  2145.5 ± 57.5  0.0477 ± 0.0019  0.3575 ± 0.029  435.4 ± 12.1  0.0569 ± 0.0019  0.3575 ± 0.029  435.4 ± 12.1  0.0569 ± 0.0019  0.3375 ± 0.029  435.4 ± 12.1  0.0477 ± 0.0019  0.3435 ± 0.031  255.0 ± 6.2  0.0419 ± 0.0010  0.311 ± 0.031  255.0 ± 6.2  0.0418 ± 0.0010  0.311 ± 0.031  1788 0 ± 27.6  0.0418 ± 0.0010  0.241 ± 0.016  291.1 ± 3.7  0.0418 ± 0.0011  0.296 ± 0.029  264.3 ± 6.7  0.3288 ± 0.0050  5.373 ± 0.135  182.2 ± 28.1  0.349 ± 0.0039  5.860 ± 0.020  1980.7 ± 48.6  0.0419 ± 0.0013  0.342 ± 0.029  283.1 ± 8.4  0.0419 ± 0.0014  0.335 ± 0.035  272.2 ± 8.8  0.0431 ± 0.0014  0.337 ± 0.035			102.9	± 25	14.8 278 ± 25
0.0426 ± 0.0016 0.300 ± 0.036 288.6 ± 9.8 0.0459 ± 0.0013 0.329 ± 0.020 289.3 ± 8.3 0.0452 ± 0.0010 0.329 ± 0.020 289.3 ± 8.3 0.0477 ± 0.0016 0.566 ± 0.239 2145.5 ± 57.5 0.0699 ± 0.0019 0.575 ± 0.029 45.5 ± 12.1 0.0477 ± 0.0019 0.575 ± 0.029 45.5 ± 12.1 0.0477 ± 0.0019 0.575 ± 0.029 45.5 ± 12.1 0.0497 ± 0.0019 0.5475 ± 0.029 45.5 ± 12.1 0.0497 ± 0.0019 0.5475 ± 0.029 27.0 ± 8.9 0.0498 ± 0.0010 0.311 ± 0.031 255.0 ± 6.2 0.316 ± 0.0006 0.241 ± 0.016 219.1 ± 3.7 0.0418 ± 0.0010 0.266 ± 0.029 264.3 ± 6.7 0.3288 ± 0.0080 0.241 ± 0.135 182.2 ± 28.1 0.3597 ± 0.0088 5.860 ± 0.193 189.0 ± 46.4 0.0591 ± 0.0013 0.354 ± 0.036 37.5 ± 0.035 0.0419 ± 0.0011 0.335 ± 0.038 254.6 ± 8.8 0.0431 ± 0.0014 0.337 ± 0.033 27.2 ± 8.8			1.66	± 20	9.5 179 ± 20
0.0459 ± 0.0013			95.1	± 12	5.2 225 ± 12
0.0424 ± 0.0012			114.6	£ 29	9.3 264 ± 29
0.3949 ± 0.0106 6.666 ± 0.239 2145.5 ± 57.5 0.0477 ± 0.0015 0.398 ± 0.034 300.4 ± 9.7 0.0699 ± 0.0019 0.575 ± 0.029 435.4 ± 12.1 0.0693 ± 0.0010 0.311 ± 0.031 297.0 ± 8.9 0.0403 ± 0.0010 0.311 ± 0.031 297.0 ± 8.9 0.0346 ± 0.0006 0.241 ± 0.016 2191.1 ± 3.7 0.0418 ± 0.0011 0.296 ± 0.029 264.3 ± 6.7 0.338 ± 0.0050 5.373 ± 0.193 187.9 ± 46.4 0.3597 ± 0.0084 5.529 ± 0.193 187.9 ± 46.4 0.3597 ± 0.0088 5.860 ± 0.200 1980.7 ± 48.6 0.0419 ± 0.0013 0.342 ± 0.039 283.1 ± 8.4 0.0419 ± 0.0014 0.337 ± 0.035 224.3 ± 8.8 0.0431 ± 0.0014 0.335 ± 0.038 224.6 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 27.2. ± 8.8			6.98	± 28	7.8 298 ± 28
0.06477 ± 0.0015 0.598 ± 0.034 300.4 ± 9.7 0.06699 ± 0.0019 0.575 ± 0.029 435.4 ± 12.1 0.0477 ± 0.0019 0.575 ± 0.029 435.4 ± 12.1 0.0477 ± 0.0014 0.435 ± 0.031 297.0 ± 8.9 0.0408 ± 0.0010 0.341 ± 0.031 255.0 ± 6.2 0.0346 ± 0.0006 0.241 ± 0.016 219.1 ± 3.7 0.0418 ± 0.0011 0.296 ± 0.029 264.3 ± 6.7 0.3288 ± 0.0050 5.373 ± 0.135 1832.4 ± 28.1 0.3597 ± 0.0084 5.529 ± 0.193 1879.0 ± 46.4 0.3597 ± 0.0088 5.860 ± 0.200 1980.7 ± 48.6 0.0494 ± 0.0013 0.342 ± 0.029 283.1 ± 8.4 0.0419 ± 0.0011 0.335 ± 0.035 27.2.2 ± 8.8			91.5	4 €7	$36.6   1715 \pm 67$
0.0699 ± 0.0019 0.555 ± 0.029 455.4 ± 12.1 0.0477 ± 0.0014 0.455 ± 0.029 455.4 ± 12.1 0.0403 ± 0.0010 0.311 ± 0.031 255.0 ± 6.2 0.0346 ± 0.0006 0.341 ± 0.031 255.0 ± 6.2 0.0348 ± 0.0006 0.241 ± 0.036 219.1 ± 3.7 0.0418 ± 0.0010 0.296 ± 0.029 264.3 ± 6.7 0.3288 ± 0.0050 5.373 ± 0.135 182.2 ± 28.1 0.3384 ± 0.0084 5.529 ± 0.193 182.0 ± 46.4 0.3597 ± 0.0088 5.860 ± 0.020 1980.7 ± 48.6 0.0494 ± 0.0013 0.342 ± 0.029 283.1 ± 8.4 0.0419 ± 0.0014 0.335 ± 0.035 25.4 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 27.2 ± 8.8			92.9		8.1 316 ± 25
0.0471 ± 0.0014  0.435 ± 0.051 297.0 ± 8.9 0.0403 ± 0.0010  0.311 ± 0.031 255.0 ± 6.2 0.3196 ± 0.0049 5.007 ± 0.231 1788.0 ± 27.6 0.0346 ± 0.0006 0.241 ± 0.016 219.1 ± 3.7 0.0418 ± 0.0011 0.266 ± 0.029 264.3 ± 6.7 0.3288 ± 0.0050 5.373 ± 0.135 182.2 ± 28.1 0.3384 ± 0.0084 5.229 ± 0.193 189.0 ± 46.4 0.3597 ± 0.0088 5.806 ± 0.093 189.0 ± 46.4 0.0494 ± 0.0013 0.345 ± 0.035 27.2 ± 8.8 0.0431 ± 0.0014 0.337 ± 0.035 20.46 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035			103.0	± 45	11.5 283 ± 45
0.0403 ± 0.0010 0.311 ± 0.031 255.0 ± 6.2 0.3196 ± 0.0049 5.067 ± 0.251 1788.0 ± 27.6 0.0346 ± 0.0006 0.241 ± 0.016 219.1 ± 3.7 0.0418 ± 0.0001 0.206 ± 0.029 264.3 ± 6.7 0.3288 ± 0.0050 5.373 ± 0.135 182.4 ± 28.1 0.3597 ± 0.0088 5.800 ± 0.093 1879.0 ± 46.4 0.3597 ± 0.0088 5.800 ± 0.200 19807 ± 48.6 0.0494 ± 0.0013 0.342 ± 0.029 233.1 ± 8.4 0.0491 ± 0.0014 0.337 ± 0.038 224.6 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 27.2.2 ± 8.8			95.3	# 70 +	42.2 1941 ± 70
0.3196 ± 0.0049 5.067 ± 0.251 1788.0 ± 27.6 0.0346 ± 0.0066 0.241 ± 0.016 219.1 ± 3.7 0.0418 ± 0.0011 0.296 ± 0.029 264.3 ± 6.7 0.3288 ± 0.0080 5.373 ± 0.135 182.4 ± 28.1 0.3384 ± 0.0084 5.529 ± 0.193 1879.0 ± 46.4 0.3597 ± 0.0088 5.860 ± 0.200 1980.7 ± 48.6 0.0601 ± 0.0020 0.546 ± 0.056 376.3 ± 12.7 0.0449 ± 0.0013 0.342 ± 0.029 283.1 ± 8.4 0.0419 ± 0.0011 0.337 ± 0.035 27.2.2 ± 8.8			86.8	± 42	10.7 360 ± 42
0.0346 ± 0.0006	0.57 F		92.0	平 45	13.1 458 ± 45
0.0418 ± 0.0011 0.206 ± 0.029 2.64.3 ± 6.7 0.2288 ± 0.0050 5.373 ± 0.135 1822.4 ± 28.1 0.338 ± 0.0080 5.373 ± 0.135 1822.4 ± 28.1 0.338 ± 0.0088 5.229 ± 0.193 1879.0 ± 46.4 0.2597 ± 0.0088 5.806 ± 0.200 1980.7 ± 48.6 0.0061 ± 0.0020 0.546 ± 0.055 3.76.3 ± 12.7 0.0499 ± 0.0013 0.342 ± 0.029 2.83.1 ± 8.4 0.0419 ± 0.0014 0.337 ± 0.038 2.64.6 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035			2.96	+ 40	11,2 326 ± 40
0.3288 ± 0.0050 5.373 ± 0.135 1832.4 ± 28.1 0.3384 ± 0.0084 5.529 ± 0.193 1879.0 ± 46.4 0.2597 ± 0.0088 5.800 ± 0.200 1980.7 ± 48.6 0.0601 ± 0.0020 0.546 ± 0.056 376.3 ± 12.7 0.0449 ± 0.0013 0.342 ± 0.029 283.1 ± 8.4 0.0431 ± 0.0014 0.337 ± 0.035 272.2 ± 8.8		-	78.7	29 =	$526 \pm 67$
0.3584 ± 0.0084 5.529 ± 0.193 1879.0 ± 46.4 0.3597 ± 0.0088 5.860 ± 0.200 1980.7 ± 48.6 0.0601 ± 0.0020 0.546 ± 0.056 376.3 ± 12.7 0.0449 ± 0.0013 0.342 ± 0.029 233.1 ± 8.4 0.0419 ± 0.0011 0.335 ± 0.038 24.6 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 272.2 ± 8.8		-	0.05	¥9 =	386 ± 64
0.3597 ± 0.0088 5.860 ± 0.200 1980.7 ± 48.6 0.0601 ± 0.0020 0.546 ± 0.056 376.3 ± 12.7 0.0449 ± 0.0013 0.342 ± 0.029 283.1 ± 8.4 0.0419 ± 0.0011 0.335 ± 0.038 224.6 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 272.2 ± 8.8			102.5		143 ± 13
0.0601 ± 0.0020 0.546 ± 0.056 376.3 ± 12.7 0.0449 ± 0.0013 0.342 ± 0.029 283.1 ± 8.4 0.0419 ± 0.0011 0.353 ± 0.018 264.6 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 272.2 ± 8.8			103.7	± 45	278 ± 45
0.0449 ± 0.0013 0.342 ± 0.029 283.1 ± 8.4 0.0419 ± 0.0011 0.335 ± 0.018 264.6 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 272.2 ± 8.8			100.0	± 78	1903 ± 78
0.0419 ± 0.0011 0.335 ± 0.018 264.6 ± 6.8 0.0431 ± 0.0014 0.337 ± 0.035 272.2 ± 8.8			90.1	± 32	8.9 289 ± 32
$0.0431 \pm 0.0014$ $0.337 \pm 0.035$ $272.2 \pm 8.8$			986	+ 26	236 ± 26
			101.1	± 23	248 ± 23
$0.0277 \pm 0.0008$ $0.200 \pm 0.015$ $176.1 \pm 4.9$			105.4	254 ± 25 105.4	12.0 254 ± 25

Grain	Ω <sub>852</sub> /9d <sub>902</sub>	Ossz/9d_cor	200Pb/238U age (Ma)	<sup>207</sup> Pb/ <sup>235</sup> U age (Ma)	%conc	Th/U	Grain	$\Omega_{8EE}/9d_{90E}$	$^{207}{\rm Pb/^{235}U}$	206 Pb/23fU age (Ma)	<sup>207</sup> Pb/ <sup>225</sup> U age (Ma)	%conc	Th/U
Fu-1-96	0.0466 ± 0.0014	$0.402 \pm 0.032$	293,8 ± 8,7	343 ± 38	85.7	0.63	Ha-1-22	$0.2663 \pm 0.0041$	$4.165 \pm 0.147$	1521,9 ± 23.6	1667 ± 59	613	0.54
Fu-1-97	$0.0324 \pm 0.0010$	0.216 ± 0.016	$205.7 \pm 6.2$	198 ± 15	103.8	0.51	Ha-1-23	0.0339 ± 0.0006	#	215.1 ± 3.6	$350 \pm 16$	61.5	0,41
Fu-1-98	0.0486 ± 0.0018	$0.309 \pm 0.042$	306.0 ± 11.6	$273 \pm 38$	112.0	0.55	Ha-1-24	$0.2998 \pm 0.0062$	$4.656 \pm 0.142$	$1690.2 \pm 35.2$	1759 ± 54	1.96	0.31
Fu-1-99	$0.0347 \pm 0.0012$	$0.240 \pm 0.023$	220.1 ± 7.3	218 ± 21	1003	0.40	Ha-1-25	41	$0.232 \pm 0.012$	177.5 ± 4.0	212 ± 11	83.7	0.41
Fu-1-100	$0.3289 \pm 0.0088$	$5.078 \pm 0.150$	$1833.0 \pm 49.2$	1832 ± 54	0.001	0.10	Ha-1-26		$0.287 \pm 0.012$	$253.1 \pm 5.5$	256 ± 11	8.86	0.49
Fu-1-101		$0.302 \pm 0.024$	$270.5 \pm 8.4$	$268 \pm 21$	101.0	0.71	Ha-1-27	+1.	+	152,5 ± 3.9		99.4	0.68
Fu-1-102	$0.0497 \pm 0.0021$	$0.425 \pm 0.063$	308.9 ± 13.2	360 ± 53	85.9	0.33	Ha-1-28	#	-11	188.3 ± 5.4	+	5.19	0.76
Fu-1-103	$0.4067 \pm 0.0110$	$7.797 \pm 0.233$	2199.9 ± 59.3	$2208 \pm 66$	9.66	0.70	Ha-1-29	++	#	226.5 ± 5.0	$229 \pm 11$	8.86	0.42
Fu-1-104	$0.0477 \pm 0.0020$	$0.384 \pm 0.055$	$300.1 \pm 12.3$	330 ± 48	0.16	0.59	Ha-1-30	-14	#	$161.3 \pm 3.8$	4	88.0	0.97
Fu-1-105	$0.3555 \pm 0.0097$	5.468 ± 0.188	$1960.9 \pm 53.8$	1896 ± 65	103.4	0.21	Ha-1-31	$0.3359 \pm 0.0071$	$5.420 \pm 0.179$	1866,8 ± 39,6	1888 ± 62	686	0.34
Fu-1-106	$0.0462 \pm 0.0016$	0,329 ± 0.052	291,3 ± 10,2	289 ± 45	100.8	99.0	Ha-1-32	-11	0,286 ± 0.017	192.2 ± 4.7	255 ± 15	75.4	0,51
Fu-1-107	$0.0429 \pm 0.0011$	0,317 ± 0,035	270.8 ± 7.0	279 ± 31	6.96	0.87	Ha-1-33	$0.0397 \pm 0.0009$	$0.296 \pm 0.018$	250,9 ± 5.9	+	95.4	0.81
Fu-1-108	$0.0307 \pm 0.0005$	$0.221 \pm 0.013$	195.1 ± 3.1	203 ± 12	6.96	0.26	Ha-1-34	0.0396 ± 0.0009	$0.293 \pm 0.012$	250,2 ± 5,4	261 ± 11	0.96	0.38
Fu-1-109	0.3308 ± 0.0044	5.324 ± 0.176	$1842.0 \pm 24.8$	1873 ± 62	98.4	0.37	Ha-1-35	$0.0298 \pm 0.0007$	$0.226 \pm 0.016$	189.0 ± 4.7	207 ± 15	61.4	0.5
Fu-1-110	0.0458 ± 0.0010	$0.389 \pm 0.034$	288.5 ± 6.6	334 ± 29	86.5	0.66	Ha-1-36	0.0208 ± 0.0005	0.198 ± 0.014	132.6 ± 3.5	183 ± 13	72.4	0.58
Fu-1-111	0.0549 ± 0.0019	$0.476 \pm 0.068$	344.3 ± 12.0	396 ± 57	87.0	0.64	Ha-1-37	41.	#	$170.0 \pm 4.0$	+	92.3	0.67
Fu-1-112	$0.4100 \pm 0.0052$	6.503 ± 0.196	2215.0 ± 28.2	2046 ± 62	108.2	0.44	Ha-1-38	+	-8	214.7 ± 4.7	365 ± 14	58.9	0.36
Fu-1-113	$0.0332 \pm 0.0006$	$0.249 \pm 0.016$	$210.4 \pm 3.6$	226 ± 14	633	0.48	Ha-1-39	$0.0471 \pm 0.0011$	$0.361 \pm 0.019$	296.6 ± 6.8	313 ± 17	94.7	0.5
Fu-1-114	$0.0470 \pm 0.0007$	$0.324 \pm 0.015$	$296.0 \pm 4.1$	285 ± 13	104.0	0.25	Ha-1-40	$0.0280 \pm 0.0007$	$0.201 \pm 0.014$	178.3 ± 4.4	186 ± 13	95.7	0.4
Fu-1-115	$0.0396 \pm 0.0010$	$0.281 \pm 0.024$	$250.3 \pm 6.3$	252 ± 22	5.66	1.09	Ha-1-41	+1		$189.0 \pm 4.0$	189 ± 8	6.66	0.5
Fu-1-116	$0.0405 \pm 0.0011$	$0.305 \pm 0.031$	255.6 ± 7.1	270 ± 27	94.6	0.88	Ha-1-42	$0.0285 \pm 0.0006$	0.365 ± 0.019	181,4 ± 3.9	$316 \pm 16$	57.4	0.7
Fu-1-117	$0.0422 \pm 0.0009$	$0.511 \pm 0.029$	266.4 ± 5.9	419 ± 24	63.6	0.62	Ha-1-43	+	9,458 ± 0,206	2226,9 ± 37,7	2383 ± 52	93.4	0,36
Fu-1-118	$0.0439 \pm 0.0017$	$0.296 \pm 0.050$	$276.8 \pm 10.7$	264 ± 44	105.0	0.48	Ha-1-44	41.	$0.260 \pm 0.010$	$178.1 \pm 3.3$	235 ± 9	75.9	0.45
Fu-1-119	$0.0377 \pm 0.0010$	$0.268 \pm 0.024$	238.7 ± 6.1	$241 \pm 22$	99.2	0.28	Ha-1-45	-46	$0.843 \pm 0.043$	182.5 ± 4.5	$621 \pm 32$	29.4	1.28
Fu-1-120	$0.0338 \pm 0.0010$	$0.257 \pm 0.027$	$214.3 \pm 6.2$	232 ± 25	92.2	0.55	Ha-1-46	$0.3243 \pm 0.0055$	$5.166 \pm 0.119$	$1810.5 \pm 30.8$	1847 ± 43	0.86	0.14
Fu-1-121	$0.0438 \pm 0.0014$	$0.280 \pm 0.036$	276.1 ± 8.5	250 ± 32	110.3	6,64	Ha-1-47	#1	$0.241 \pm 0.011$	$201.8 \pm 3.8$	$219 \pm 10$	92.1	0.38
Fu-1-122	$0.0774 \pm 0.0019$	0,592 ± 0.049	480.5 ± 11.9		101.7	0.54	Ha-1-48	44	$0.492 \pm 0.037$	$277.7 \pm 7.0$	40€ ₹ 30	68.4	0.83
Fu-1-123	$0.0422 \pm 0.0015$	$0.307 \pm 0.045$	266.5 ± 9.6	272 ± 40	0.86	0.52	Ha-1-49	41	$0.197 \pm 0.010$	175.5 ± 3.9	183 ± 9	0.96	0.42
							Ha-1-50	#		$1823.2 \pm 37.0$	1836 ± 52	99.3	0.5
	Sandstone of the Hagino Formation from Sano (Ha-1; 33-37' 16.89"	ormation from Sano (	Ha-1; 33 37 16.89	N, 133	7" E)	100	Ha-1-51	#	$0.610 \pm 0.044$	$383.5 \pm 10.0$	484 ± 35	79.3	0.4
Ha-1-1	0.0232 ± 0.0005	0.154 ± 0.009	148.1 ± 3.5	4	101.7	0.56	Ha-1-52	H -		$213.1 \pm 5.3$	258 ± 17	82.6	0.6
Ha-1-2	0.2518 ± 0.0054	# -	1447.7 ± 31.1	# -	88.8	0.17	Ha-1-53	+1 -	# 1	261.8 ± 6.1	290 ± 17	90.1	8,0
110-1-3	0,020 ± 0,000/	0.213 ± 0.021	130.0 = 4.2	H F	7.00	17.1	Ha-1-54	# -	H1 -	0,44 ± 8,2412	233/ ± 04	93.8	6.0
H-1-DH	0.0333 ± 0.0010	H =	710 ± 0.77	H 8	13.6	0.40	119-1-55	0.0300 = 0.0009		4.0 ± 2.822	70 = 7/2	0.78	0.0
110-1-2	0.0344 ± 0.0009	0.282 ± 0.019	2010 + 2010	252 ± 17	20.0	0.70	Ha-1-50	11 -	0.307 ± 0.033	23/.3 ± /.2	3/3 ± 30	0.60	0.04
Ho. L.7	0.000 + 0.0006	4 4	1316 + 30	+ +	65.3	130	Ho. 1. 58	1 +	4	1660 + 30	201 + 100	82.6	0.0
Ho-1-8		0.282 + 0.015	103.1 + 4.4	+	5 92	0.47	Ha-1-50	1 +	+	14757 + 27 A	1607 + 50	X8.7	0.5
Ho-1-9		1	1353 + 36		65.5	0.87	Ha-1-60	+	+	1449 ± 3.3	200 ± 15	72.3	0.50
Ha-1-10	0.0292 ± 0.0007	+	185.8 ± 4.4	+	76.1	0.66	Ha-1-61	-#	+	-11	155 ± 10	29.0	0.7
Ha-1-11		#	335.3 ± 10.1	#	67.9	0.51	Ha-1-62	-11	+	+		81.9	0.32
Ha-1-12	$0.2897 \pm 0.0059$	$4.587 \pm 0.154$	1640.1 ± 33.5	-14	93.9	0.38	Ha-1-63	+	4	+	198 ± 12	7.06	0.5
Ha-1-13	0,0247 ± 0.0005	0.201 ± 0.010	157,2 ± 3,4	#	84.4	0,28	Ha-1-64	0.0430 ± 0,0008	$0.355 \pm 0.020$	271.7 ± 5.1	308 ± 17	88.1	0.2
Ha-1-14	0.0391 ± 0.0009	$0.332 \pm 0.022$	247.1 ± 5.9.	291 ± 19.	84.8	0.53	Ha-1-65	$0.0235 \pm 0.0008$	+1	149.9 ± 5.2	15 = 29	22.9	1.00
Ha-1-15	$0.0292 \pm 0.0007$	$0.228 \pm 0.015$	185.7 ± 4.4	+	89.0	0.79	Ha-1-66	$0.0332 \pm 0.0007$	+	210.3 ± 4.7		9006	0.53
Ha-1-16	0.0462 ± 0.0012	$0.445 \pm 0.040$	297.2 ± 7.3	374 ± 33	78.0	0.36	Ha-1-67	41	$0.295 \pm 0.014$	245.7 ± 5.5	#(	93.5	0.5
Ha-1-17	$0.3097 \pm 0.0053$	5,454 ± 0,221	$1739.4 \pm 29.7$	1893 ± 77	616	0.40	Ha-1-68	$0.0331 \pm 0.0007$	+1	$209.8 \pm 4.5$	+	91.2	0.47
Ha-1-18	$0.0393 \pm 0.0010$	$0.454 \pm 0.037$	248,4 ± 6,1	$380 \pm 31$	65.4	0.77	Ha-1-69	+1	#	+	1761 ± 55	94.4	0.9
Ha-1-19	$0.0250 \pm 0.0004$	$0.181 \pm 0.009$	159.2 ± 2.5	169 ± 8	94.3	0.52	Ha-1-70	0.0446 ± 0.0010	0.439 ± 0.022	$281.2 \pm 6.5$	369 ± 19	76.1	0.44
Ha-1-20	$0.0306 \pm 0.0006$	$0.221 \pm 0.015$	194.1 ± 3.7	$203 \pm 14$	95.8	95.0	Ha-1-71	46	$0.327 \pm 0.022$	$219.2 \pm 5.6$	#	16.4	0.65
10 1 01	20000 0 10000	2000			100			The second second second		The second second	The state of the state of		,

TABLE 1. (Continued)

Û852/9d, 100	D <sub>552</sub> /9d <sub>202</sub>	(Ma)	(Ma)	%conc	Th/U	Grain	Dec./9d.	Occa/9d	(Ma)	(Ma)	%conc	TUVE
0.0209 ± 0.0006	0.158 ± 0.016	4	149 ± 15	2.68	1.33	Ha-2-9	$0.0298 \pm 0.0010$	$0.204 \pm 0.020$	189.2 ± 6.1	61 = 681	100.2	0.45
$0.2843 \pm 0.0060$	4,462 ± 0,149	1612.9 ± 34.2	1724 ± 58	93.6	0.31	Ha-2-10	$0.0239 \pm 0.0009$	#	152.1 ± 5.4	177 ± 15	85.9	0.56
0.0400 ± 0.0013	$0.386 \pm 0.039$		332 ± 34	76.3	0.64	Ha-2-11	$0.0282 \pm 0.0011$	0.515 ± 0.045	179.6 ± 7.2	422 ± 37	42.6	0.53
0.0465 ± 0.0014	0.555 ± 0.047		449 ± 38	65.3	0.56	Ha-2-12	$0.0222 \pm 0.0009$	$\overline{H}$	141.3 ± 5.9	$137 \pm 19$	103.3	69.0
$0.0253 \pm 0.0006$	$0.217 \pm 0.013$	161.1 ± 3.8	199 ± 12	80.9	0.83	Ha-2-13	$0.0256 \pm 0.0009$	$0.179 \pm 0.012$	$163.2 \pm 5.5$	167 ± 12	7.76	0.41
$0.3033 \pm 0.0065$	$4.780 \pm 0.165$	$1707.7 \pm 36.5$	1781 ± 62	626	0.32	Ha-2-14	$0.0284 \pm 0.0010$	41	$180.4 \pm 6.5$	$91 \pm 081$	100.0	0,36
0.0404 ± 0.0011	0.376 ± 0.027		324 ± 24	78.7	0.59	Ha-2-15	0,4139 ± 0.0136	$8.029 \pm 0.391$	2232,9 ± 73,2	$2234 \pm 109$	6.66	0.11
± 0.0009	$0.288 \pm 0.030$	184.6 ± 6.0	257 ± 27	21.8	0.72	Ha-2-16	$0.0187 \pm 0.0007$	+	119.5 ± 4.4	$125 \pm 12$	95.6	0.66
$0.0359 \pm 0.0009$	$0.343 \pm 0.024$		$300 \pm 21$	75.8	0.84	Ha-2-17	$0.0280 \pm 0.0011$	#	$178.1 \pm 6.9$	154 ± 19	115.8	0.57
± 0.0011	$0.312 \pm 0.030$		276 ± 27	85.2	060	Ha-2-18	$0.0265 \pm 0.0010$	#	$168.9 \pm 6.1$	161 ± 15	104.8	0.53
$0.0273 \pm 0.0007$	$0.213 \pm 0.018$		$196 \pm 17$	88.5	0.42	Ha-2-19	$0.0320 \pm 0.0011$	-#	$203.3 \pm 6.9$	$202 \pm 19$	100.5	0.58
$0.3165 \pm 0.0063$	5.069 ± 0.171	40	1831 ± 62	8.96	0.47	Ha-2-20		$0.142 \pm 0.013$	133,6 ± 4.4	135 ± 12	99.1	0.85
0.0408 ± 0.0010	$0.443 \pm 0.031$		$372 \pm 26$	69.3	0.73	Ha-2-21	$0.0279 \pm 0.0008$	#	$177.5 \pm 5.4$	$181 \pm 12$	98.1	0.45
$0.0277 \pm 0.0006$	$0.204 \pm 0.010$	100	$189 \pm 10$	93.4	0.42	Ha-2-22	44	91	$117.1 \pm 4.2$	117 ± 14	100.2	0.86
0.0320 ± 0.0007	0.289 ± 0.013	203.1 ± 4.2	257 ± 12	6.82	0.80	Ha-2-23	0.0268 ± 0.0009	31	$170.7 \pm 6.0$	181 ± 19	94.1	0.52
$0.0267 \pm 0.0006$	0.190 ± 0.009	170.0 ± 3.6	177 ± 8	6.3	0.37	Ha-2-24	0.0421 ± 0.0014	33	265.7 ± 8.6	$351 \pm 26$	75.8	0.52
0.0211 ± 0.0007	$0.182 \pm 0.019$		170 ± 18	5.64	190	Ha-2-25	0,0292 ± 0,0010	++	185.8 ± 6.1	91 = 681	0.86	0,44
± 0.0005	$0.195 \pm 0.013$	157.5 ± 3.3	$181 \pm 12$	87.3	0.34	Ha-2-26	$0.0300 \pm 0.0012$	11	190.6 ± 7.4	$206 \pm 26$	92.7	99.0
$0.0277 \pm 0.0006$	0.225 ± 0.016	176.2 ± 3.9	206 ± 14	85.5	0.51	Ha-2-27	$0.0350 \pm 0.0012$	-11	221.5 ± 7.4	222 ± 21	7.66	0.52
$0.3149 \pm 0.0051$	$4.904 \pm 0.123$	1764.7 ± 28.8	1803 ± 45	67.6	0.32	Ha-2-28	$0.0287 \pm 0.0012$	- 11	182.3 ± 7.5	184 ± 18	1.66	0.41
0.0323 ± 0.0007	$0.273 \pm 0.017$		245 ± 15	83.6	0.52	Ha-2-29		+	1826,3 ± 70,0	1841 ± 117	99.2	0.18
$0.3078 \pm 0.0052$	4.805 ± 0,133	1729.8 ± 29.1	1786 ± 50	6.96	0.37	Ha-2-30	$0.0418 \pm 0.0019$	+	$264.1 \pm 12.0$	278 ± 36	6.46	0,25
$0.0267 \pm 0.0005$	$0.194 \pm 0.012$		180 ± 12	94.4	09.0	Ha-2-31	#	$0.194 \pm 0.018$	173.7 ± 7.1	180 ± 17	9.96	09'0
0.0295 ± 0.0007	$0.223 \pm 0.018$		204 ± 16	91.6	0.37	Ha-2-32	+1.	111	$127.1 \pm 5.5$	128 ± 15	0.66	09.0
$0.0385 \pm 0.0007$	0.305 ± 0.013		$270 \pm 12$	90,1	0.51	Ha-2-33	+1	+1	135.3 ± 7.3	152 ± 29	1.68	0.59
$0.0301 \pm 0.0005$	$0.223 \pm 0.011$		$204 \pm 10$	93.5	0.55	Ha-2-34	#	$0.138 \pm 0.017$	122,2 ± 5.4	$131 \pm 16$	93.1	1.72
$0.0662 \pm 0.0010$	0.538 ± 0.025	$413.0 \pm 6.2$	$437 \pm 21$	94.5	0.75	Ha-2-35	+9.	-44.	$218.3 \pm 8.8$	$216 \pm 19$	101.0	0.68
$0.0303 \pm 0.0006$	$0.233 \pm 0.017$		212 ± 16	9006	09'0	Ha-2-36	$0.1579 \pm 0.0060$	44	945.3 ± 36.2	1234 ± 78	9.97	0.20
$0.0202 \pm 0.0004$	$0.360 \pm 0.020$		$312 \pm 17$	41.3	0.73	Ha-2-37	+1	-44	$1817.2 \pm 29.9$	$1834 \pm 65$	99.1	0.45
$0.2997 \pm 0.0036$	$4.804 \pm 0.116$	1689.8 ± 20.2	1786 ± 43	94.6	0.44	Ha-2-38	$0.0315 \pm 0.0008$	44	$200.1 \pm 5.3$	217 ± 22	92.2	0.47
$0.0340 \pm 0.0007$	0.416 ± 0.029		$353 \pm 25$	61.0	1.29	Ha-2-39	4	$0.256 \pm 0.017$	242.8 ± 4.9	$231 \pm 16$	104.9	0.63
0.0367 ± 0.0006	$0.307 \pm 0.019$		$272 \pm 17$	85.4	0.28	Ha-2-40	+	-#	$248.1 \pm 7.4$	247 ± 30	100.3	0.71
$0.0348 \pm 0.0005$	0.268 ± 0.012	220.6 ± 3.1	241 ± 11	91.4	0.83	Ha-2-41	#	44	1729,3 ± 28,2	$1770 \pm 62$	7.76	0.39
$0.0280 \pm 0.0006$	$0.208 \pm 0.013$	178,3 ± 3,8	191 ± 12	93.1	650	Ha-2-42	$0.0426 \pm 0.0013$	141	268.9 ± 8.4	$278 \pm 35$	6.96	0.61
$0.0377 \pm 0.0007$	$0.281 \pm 0.0[1]$	238:5 ± 4.5	$252 \pm 10$	94.7	0.87	Ha-2-43	+1	+1	$121.3 \pm 2.9$	$122 \pm 11$	9.66	1.54
$0.0339 \pm 0.0006$	$0.246 \pm 0.011$	214.9 ± 4.1	224 ± 10	1.96	0.95	Ha-2-44	$0.0270 \pm 0.0010$	#	$172.0 \pm 6.1$	81 ± 061	903	0.58
$0.0272 \pm 0.0005$	$0.222 \pm 0.010$	$173.1 \pm 3.4$	$204 \pm 9$	85.0	0.58	Ha-2-45	+1.	+1	202,8 ± 7.1	$224 \pm 20$	506	0.62
± 0.0008	$0.344 \pm 0.021$	235.6 ± 5.2	$300 \pm 19$	78.4	0.86	Ha-2-46	#	-0	129.2 ± 4.9	149 ± 17	86.6	0.73
$0.0319 \pm 0.0006$	$0.246 \pm 0.009$	202.6 ± 3.8	223 ± 8	8.06	0.47	Ha-2-47	#	-11	156.6 ± 8.5	457 ± 62	34.3	1.32
$0.0270 \pm 0.0006$	0.301 ± 0.019	171.7 ± 4.0	267 ± 17	64.3	1.14	Ha-2-48	$0.0265 \pm 0.0009$	$0.175 \pm 0.017$	168.7 ± 5.9	164 ± 16	103.0	0.54
≠ 0.0009	$0.378 \pm 0.021$	265.6 ± 5.6	326 ± 18	81.5	0.70	Ha-2-49	#	#	$168.6 \pm 5.6$	$170 \pm 14$	6.86	0.45
						Ha-2-50	+)	$0.194 \pm 0.013$	$165.2 \pm 5.3$	$180 \pm 12$	91.6	0.25
e Hagino Fo	Sandstone of the Hagino Formation from Hagino (Ha-2; 33		" N, 133 45' 25.7.	4" E)		Ha-2-51	#	+	$182.9 \pm 6.2$	$199 \pm 16$	6.16	0.46
$0.0385 \pm 0.0015$	0.305 ± 0.041		270 ± 36	90.2	0.63	Ha-2-52	$0.3075 \pm 0.0098$	#1.	$1728.2 \pm 54.9$	1776 ± 98	97.3	0.43
0.0253 ± 0.0009	$0.217 \pm 0.026$		199 ± 24	80.8	0.58	Ha-2-53	#	#	253.7 ± 12.3	271 ± 25	93.7	0.52
$0.0214 \pm 0.0006$	$0.140 \pm 0.011$		133 ± 10	102.3	0.72	Ha-2-54	$0.0212 \pm 0.0010$	$0.138 \pm 0.014$	135,1 ± 6.6	$131 \pm 13$	103.2	0.58
$0.0403 \pm 0.0011$	$0.273 \pm 0.017$	254.6 ± 6.9	245 ± 15	103.9	0.22	Ha-2-55	$0.0302 \pm 0.0015$	$0.208 \pm 0.024$	191.8 ± 9.7	192 ± 22	100.0	0,39
$0.0293 \pm 0.0011$	0.202 ± 0.028	186.1 ± 7.0	186 ± 26	8.66	9.58	Ha-2-56	0.0341 ± 0.0017	+	216.3 ± 10.7	237 ± 23	91.4	0.53
$0.0309 \pm 0.0009$	0.229 ± 0.018		$209 \pm 16$	63.6	0.32	Ha-2-57	0.0355 ± 0.0017	$0.247 \pm 0.022$	$224.8 \pm 10.8$	$224 \pm 20$	100.3	0.79
$0.0294 \pm 0.0008$	0.197 ± 0.012	187.0 ± 5.0	183 ± 11	102.4	0.41	Ha.9.58	0.0260 ± 0.0012	0.178 + 0.015	0 4 4 4 591	166 + 14	200	N. C.
					MATERIA	200	The second secon	V.1./0 + 0.01.2	100°/ ± 1.3	+T + 001	93.0	0.34

TABLE 1. (Continued)

	U255/234	200Pb/235U age	207Pb/235U age	%conc	Th/U	Grain	U852/94/00	$\Omega^{552}/4q^{702}$	206 Pb/238U age	207 Pb/225 U age	%conc	Th/U
ш	2100 ± 5310	(Ma)	(Ma)	1040	423	THE C 411	00000 + 00000	A100 ± 9010	(Ma)	(Ma)	2 201	0.30
	0.206 + 0.013	1849 + 92	190 + 20	07.7	0.32	Ho-2-113	0.0265 ± 0.0009	0.168 ± 0.010	1373 + 611	153 + 75	2007	0.38
	0.134 ± 0.015	128.3 ± 4.3		100.8	0.84	Ha-2-113	1	( #)	176.6 ± 8.4	193 ± 16	91.4	0.65
	$0.124 \pm 0.019$	118.9 ± 4.7	81 ± 611	100.1	89.0	Ha-2-114	$0.0179 \pm 0.0009$	$0.113 \pm 0.013$	114.4 ± 5.7	109 ± 13	105.3	1.06
	$0.206 \pm 0.018$	$182.7 \pm 5.5$	$190 \pm 17$	0.96	0.53	Ha-2-115	$0.0279 \pm 0.0014$	$0.203 \pm 0.023$	$177.6 \pm 8.9$	188 ± 21	94.7	0.39
	$0.959 \pm 0.064$	181.8 ± 6.0	683 ± 46	26.6	0.40	Ha-2-116	$0.0205 \pm 0.0011$	$0.150 \pm 0.023$	131.1 ± 7.3	$142 \pm 22$	92.3	1,25
	$0.115 \pm 0.017$	124.0 ± 4.6	111 + 16	111.8	290	Ha-2-117	$0.2970 \pm 0.0137$	$4.619 \pm 0.300$	1676,5 ± 77,4	$1753 \pm 1.14$	95.7	0.40
	$0.222 \pm 0.018$	$205.3 \pm 5.9$	$204 \pm 16$	100.7	0.55	Ha-2-118	$0.0230 \pm 0.0013$	$0.243 \pm 0.037$	146.8 ± 8.5	$221 \pm 33$	66.4	1.07
	$0.123 \pm 0.014$	118.4 ± 3.9	118 ± 13	100.6	68'0	Ha-2-119	$0.0248 \pm 0.0013$	$0.228 \pm 0.028$	157.8 ± 8.3	208 ± 26	75.8	0.65
	0.193 ± 0.014	177.7 ± 4.9	179 ± 13	0.66	0.33	Ha-2-120	$0.0270 \pm 0.0013$	$0.188 \pm 0.017$	171.9 ± 8.3	175 ± 16	98.2	0.45
	0.195 ± 0.020	178.5 ± 5.7	180 ± 18	6.86	0.48	Ha-2-121	0.0268 ± 0.0009	$0.182 \pm 0.013$	$170.2 \pm 5.5$	170 ± 12	100.1	0,52
	0.168 ± 0.012	163.8 ± 5.6	157 ± 12	104.0	0.43	Ha-2-122	0.0280 ± 0.0010	0.196 ± 0.018	177,9 = 6.1	182 ± 16	8.76	0,39
	0.176 ± 0.013	150.3 ± 5.1	165 ± 12	91.1	99.0	Ha-2-123	0.0209 ± 0.0007	# 1	133,5 ± 4.4	141 ± 11	95.0	0.50
	5.024 ± 0.235	1785.1 ± 58.2	1823 ± 85	67.6	2.34	Ha-2-124	0.0382 ± 0.0012	Η.	241.0 ± 7.0	220 ± 15	109.7	0.50
	0.207 ± 0.024	100.3 ± 6.6	191 ± 22	7.79	0.78	110-2-173	710000 = 76700	- H	183.8 ± 7.0	101 = 24	113.7	0.00
	$0.217 \pm 0.016$	$192.1 \pm 6.5$	199 ± 14	96.4	0.42	Ha-2-126	$0.0275 \pm 0.0009$	$0.208 \pm 0.017$	$175.0 \pm 5.9$	192 ± 16	91.3	0,53
	0,312 ± 0.046	$292.0 \pm 12.6$	$276 \pm 41$	105,9	0.45	Ha-2-127	0,0201 ± 0,0007	-53	128.4 ± 4.7	186 ± 17	50.5	0.89
	$0.259 \pm 0.020$	219.9 ± 7.7	$234 \pm 18$	94.2	0.74	Ha-2-128	$0.2986 \pm 0.0089$	$4.718 \pm 0.183$	$1684.1 \pm 50.3$	$1770 \pm 69$	95.1	0.76
	$11.153 \pm 0.398$	2524.7 ± 78.9	$2536 \pm 91$	9.66	0.48	Ha-2-129	$0.3688 \pm 0.0083$	-31	2023.8 ± 45.4	1946 ± 72	104.0	0.17
	$0.704 \pm 0.075$	389.9 ± 15.8	541 ± 58	72.0	0.43	Ha-2-130	$0.3388 \pm 0.0077$	#	$1880.9 \pm 42.6$	1876 ± 72	100.2	0.16
	$0.234 \pm 0.026$	200.3 ± 7.7	213 ± 24	93.9	0.50	Ha-2-131	$0.0345 \pm 0.0010$	+1	218.4 ± 6.3	$346 \pm 27$	63.1	0.45
	$0.216 \pm 0.017$	$205.1 \pm 7.0$	199 ± 15	103.2	89.0	Ha-2-132	$0.0493 \pm 0.0014$	+	310.0 ± 8.8	369 ± 31	84.0	0.57
$0.3494 \pm 0.0110$	5.470 ± 0.237	1931.8 ± 60.6	$1896 \pm 82$	101.9	0.32	Ha-2-133	$0.0275 \pm 0.0007$	#	$175.0 \pm 4.5$	$179 \pm 13$	6.7.6	0.37
	$0.298 \pm 0.028$	$223.3 \pm 8.2$	$265 \pm 25$	84.2	1.14	Ha-2-134	$0.1607 \pm 0.0037$	$2.507 \pm 0.101$	960.5 ± 22.0	$1274 \pm 51$	75.4	0.31
	$0.130 \pm 0.020$	122.5 ± 5.4	124 ± 19	98.5	68'0	Ha-2-135	41	#	$175.6 \pm 5.3$	192 ± 19	91.3	0.95
	$0.117 \pm 0.010$	$112.9 \pm 3.9$	112 ± 9	100.5	1.57	Ha-2-136	41	-93	$182.0 \pm 6.1$	159 ± 21	114.3	62.0
$0.0265 \pm 0.0010$	$0.194 \pm 0.022$	$168.7 \pm 6.6$	180 ± 21	93.8	0.45	Ha-2-137	$0.0284 \pm 0.0007$	$0.202 \pm 0.013$	$180.2 \pm 4.5$	$187 \pm 12$	96.4	0.38
$0.3380 \pm 0.0107$	5.339 ± 0.240	$1876.9 \pm 59.3$	1875 ± 84	1001	0.52							
$0.0344 \pm 0.0009$	$0.237 \pm 0.012$	$218.2 \pm 5.4$	$216 \pm 11$	101.0	0.58	A Sa	A sandstone cobble from the	Ryoseki	(RySs-1; 33 38° 17.	23" N, 133 45"	23.01" E)	
$0.0276 \pm 0.0008$	0.185 ± 0.018	175.6 ± 5.4	$172 \pm 17$	8.101	0.52	RySs-1-1	$0.0391 \pm 0.0008$	# .	$247.4 \pm 5.2$	91 <del>=</del>	92.6	0.48
$0.0422 \pm 0.0012$	0.289 ± 0.026	266.2 ± 7.9	258 ± 23	103.4	0.51	KySs-1-2	$0.0399 \pm 0.0008$	# .	252.4 ± 4.9	248 ± 15	6101	0.27
	0.201 ± 0.016	185.2 ± 5.2	186 ± 14	5.66	0,47	RySs-1-3	+1 -	+1	249,4 ± 4,9	242 ± 13	102,9	0.43
	0.173 ± 0.026	137.3 ± 5.7	162 ± 25	84.5	0.52	Ky35-1-4	0.0442 ± 0.0012	#	2/8.5 ± 7.8	386 ± 35	72.1	0.34
$0.0296 \pm 0.0008$	$0.194 \pm 0.016$	188.2 ± 5,3	180 ± 15	104.4	0.58	RySs-1-5	$0.0527 \pm 0.0012$	$0.424 \pm 0.029$	331.0 ± 7.5	359 ± 24	92.2	0.50
	$0.131 \pm 0.016$	125,2 ± 4,3	125 ± 15	100.0	0.73	RySs-1-6	$0.0679 \pm 0.0015$	+1	$423.3 \pm 9.1$	$419 \pm 26$	101.1	0.55
$0.0273 \pm 0.0008$	$0.185 \pm 0.015$	$173.6 \pm 5.0$	172 ± 14	100.7	0.73	RySs-1-7	$0.0474 \pm 0.0014$	#1	$298.4 \pm 8.6$	304 ± 33	98.3	0.44
$0.0252 \pm 0.0008$	$0.226 \pm 0.020$	$160.7 \pm 5.0$	207 ± 18	77.8	0.92	RySs-1-8	$0.0417 \pm 0.0008$	$0.302 \pm 0.015$	263,6 ± 5.2	$268 \pm 13$	98.4	0.37
	$0.178 \pm 0.014$	$165.9 \pm 3.8$	166 ± 13	8.66	0.44	RySs-1-9	$0.0395 \pm 0.0009$	+1	249,8 ± 5.7	$257 \pm 19$	67.3	0.95
$0.0367 \pm 0.0010$	$0.265 \pm 0.027$	$232.1 \pm 6.3$	239 ± 24	97.3	0.74	RySs-1-10	$0.0495 \pm 0.0011$	$0.375 \pm 0.022$	$311.2 \pm 6.8$	323 ± 19	96.4	0.38
	$0.296 \pm 0.020$	$256.2 \pm 5.5$	$263 \pm 18$	97.3	0.50	RySs-1-11	$0.0414 \pm 0.0009$	$0.284 \pm 0.018$	$261.3 \pm 5.8$	$253 \pm 16$	103.1	0.20
	5.210 ± 0.202	1825.3 ± 34.8	1854 ± 72	98.4	1.13	RySs-1-12	$0.0435 \pm 0.0012$	$0.324 \pm 0.033$	$274.6 \pm 7.8$	$285 \pm 29$	96.4	0.24
	$0.218 \pm 0.023$	191.4 ± 5.4	$200 \pm 22$	95.5	0.53	RySs-1-13	$0.0416 \pm 0.0010$	$0.301 \pm 0.021$	$262.8 \pm 6.0$	$267 \pm 18$	98.5	95.0
	$0.200 \pm 0.014$	$180.1 \pm 3.9$	$185 \pm 13$	97.4	0.62	RySs-1-14	0.0395 ± 0.0009	0,411 ± 0.026	249.6 ± 5.9	349 ± 22	71.4	0.71
	$0.192 \pm 0.016$	$172.1 \pm 4.2$		96.4	0.42	RySs-1-15	$0.0403 \pm 0.0008$	$0.292 \pm 0.010$	254.5 ± 4.8	$500 \pm 9$	8.76	0.40
	$0.247 \pm 0.025$	131.5 ± 4.8	$224 \pm 23$	58.8	0.51	RySs-1-16	$0.0440 \pm 0.0010$	$0.312 \pm 0.021$	$277.3 \pm 6.3$	$276 \pm 19$	9.001	0,32
	$0.171 \pm 0.016$	154.9 ± 4.9	161 ± 15	8.96	0.38	RySs-1-17	$0.0407 \pm 0.0008$	+1	$256.9 \pm 5.1$	$269 \pm 11$	95.5	0.74
	$0.156 \pm 0.017$	137.7 ± 4.7	$147 \pm 16$	93.8	0.59	RySs-1-18	$0.0429 \pm 0.0010$	31.	$270.5 \pm 6.3$	$273 \pm 19$	99.2	0.57
	$0.149 \pm 0.010$	147.9 ± 4.2	141 ± 10	104.6	0.36	RySs-1-19	$0.0409 \pm 0.0012$	+1	258.2 ± 7.7	251 ± 15	102,9	19.0
	$0.175 \pm 0.011$	165.1 ± 4.7	164 ± 11	100.7	0.42	RySs-1-20	$0.0397 \pm 0.0012$	41	251.0 ± 7.3	296 ± 14	84.8	0.51
	$0.152 \pm 0.017$	119.8 ± 4.2	144 ± 16	83.2	0.83	RySs-1-21	~~	#	240.2 ± 7.7	$232 \pm 19$	103.4	0.71
	$7.705 \pm 0.314$	2221.9 ± 58.8	$2197 \pm 90$	101.1	0.54	RySs-1-22	$0.0451 \pm 0.0016$	$0.349 \pm 0.034$	$284.5 \pm 9.8$	$304 \pm 30$	93.5	0.76

TABLE 1. (Continued)

99.6 0.29 RySs-1-74 0.0419 ± 0.0014 104.5 0.72 RySs-1-75 0.0425 ± 0.0014 102.0 0.66 RySs-1-76 0.0535 ± 0.0018 106.4 0.39 RySs-1-77 0.0428 ± 0.0018 99.2 0.40 RySs-1-77 0.0428 ± 0.0011 33.4 0.82 RySs-1-79 0.0454 ± 0.0011 101.6 0.38 RySs-1-80 0.04114 ± 0.0010 112.3 0.63 RySs-1-81 0.0407 ± 0.0010	303 ± 22 9 257 ± 22 10	301.8 ± 9.5 268.2 ± 8.7 289.2 ± 9.6	0,348 ± 0,026
0.72 RySs-1-75 0.0425 0.66 RySs-1-76 0.0535 0.39 RySs-1-77 0.0428 0.40 RySs-1-77 0.0428 0.82 RySs-1-79 0.0454 0.83 RySs-1-81 0.0407			
0.66 RySs-1-76 0.0535 0.39 RySs-1-77 0.0428 0.40 RySs-1-78 0.0419 0.82 RySs-1-79 0.0414 0.38 RySs-1-81 0.0414		28	
0.39 RySs-1-77 0.0428 0.40 RySs-1-78 0.0419 0.82 RySs-1-79 0.0454 0.38 RySs-1-81 0.0414 0.63 RySs-1-81 0.0414		220	
0.40 RySs-1-78 0.0419 0.82 RySs-1-79 0.0454 0.38 RySs-1-80 0.0414 0.63 RySs-1-81 0.0407		200	
0.82 Kyss-1-79 0.0454 0.38 RySs-1-80 0.0414 0.63 RvSs-1-81 0.0407		258	
0.63 RvSs-1-81 0.0407		250	
		240	
0.36		1833	
0.37 RySs-I-83 0.0418		305	
0.63 RySs-1-84 0.0400		267	267.6 ± 6.5 267
RySs-1-85 0.0461		262	8,8
0.58 RySs-1-86		284	7.1
0.67 RySs-1-87 0.0816		239	0.0
0.65 RySs-I-88 0.0411		320	6.2
0.45 RySs-1-89 0.0564 ±		464	7.3
0.44 RySs-1-90		277	
RySs-1-91 0.0414		274 +	
0.68 RySs-1-92		309 ∓	
0,25 RySs-1-93		292	
0.41 KySs-1-94		358	
KySs-1-95		787	
1.14 KySs-1-96		675	
0.59 RySs-1-9/		326 ±	
707 1187 B.S. 100 0.0431 ± 0.0010		237 ± 5/	
0.51 RySe-1-100		258 ±	
RvSr-1-101		273 ±	
0,57 RySs-1-102 0,0399		$283 \pm 20$	
0.47 RySs-1-103 0.0410 ±		344	
0.40 RySs-1-104 0.0753 ±		318	
0.58 RySs-1-105 0.0510 ±		312	
0.35 RVSs-1-106		275	
0.32 RySs-1-107 0.0414 ±		260	
9/.6 0.58 KySs-1-108 0.0522 ± 0.0013	77 1	100	107
0.04 RVSS-1-110 0.0394 ±		303	284.6 = 8.6 303
0.49		261	261
		272 4	272
0.60 YuSsI-1 0.3330 ±		337 ±	337
0.65 YuSs1-2 0.0410 ±		406 ±	406
41		272 ±	272
0.51 YuSsI-4 0.0571 ±		317 ±	317
0.33 YuSs1-5		473 ±	473
0.19 YuSsl-6 0.0388 ±	14	279	279
0.67 YuSs1-7 0.0464 ±		288	288
0.54 YuSs1-8 0.0476 ±	€1 ∓	293	
0.0465 ±	± 24	285	
0.44 YuSs1-10	± 13	271	
0.58 YuSs1-11 0.0447 ±	± 23	33	
0.68 YuSsI-12 0.3297 ±	± 20	272	278.0 ± 9.6 272

2.8         2.8         2.8         4.0         8.9         4.9         5.9         4.9         5.9 <th>Grain</th> <th><math>\Omega_{8e2}/9d_{WHZ}</math></th> <th>O 552/9d Lint</th> <th><sup>206</sup>Pb/<sup>238</sup>U age (Ma)</th> <th>207Pb/235U age (Ma)</th> <th>%conc</th> <th>Th/U</th> <th>Grain</th> <th>D<sub>SEZ</sub>/Qd<sub>SOZ</sub></th> <th>707Pb/235U</th> <th>Pb/2"U age (Ma)</th> <th>(Ma)</th> <th>%conc</th> <th>TPP/IT</th>	Grain	$\Omega_{8e2}/9d_{WHZ}$	O 552/9d Lint	<sup>206</sup> Pb/ <sup>238</sup> U age (Ma)	207Pb/235U age (Ma)	%conc	Th/U	Grain	D <sub>SEZ</sub> /Qd <sub>SOZ</sub>	707Pb/235U	Pb/2"U age (Ma)	(Ma)	%conc	TPP/IT
0.00091 0.0015 0.015 0.000 2.75 0.000 0.00091	YuSs1-13	$0.0452 \pm 0.0020$	$0.391 \pm 0.071$	284.7 ± 12.8	#	85.0	0.56	YuSs1-64	0,3375 ± 0,0046	$5.352 \pm 0.168$	1874.8 ± 25.4	#	6'66	0,20
0.0444 ± 0.0000	YuSs1-14	$0.0407 \pm 0.0011$	0.315 ± 0.030	$257.3 \pm 6.8$	-81	92.5	0.53	YuSs1-65	+1	#	269.8 ± 5.9	#	9.62	0,49
0.0041 ± 0.0009 0 0.279 ± 0.0019 0 X6.2.5.8.9 ± 10 0 10.5 T. Vickle 6 0.0059 ± 0.0055 ± 0.0058 ± 0.0059 ± 0.005	YuSs1-15	$0.0445 \pm 0.0010$	$0.313 \pm 0.025$	$280.6 \pm 6.6$	277 ± 22	101.5	0.29	YuSs1-66	-11	$0.306 \pm 0.024$	$237.3 \pm 5.0$	271 ± 21	87.5	0.64
0.0039 ± 0.0007   0.353 ± 0.001   3.054 ± 0.001   3.054 ± 0.001   3.054 ± 0.001   3.059 ± 0.001   3.059 ± 0.001   3.050 ± 0.00	YuSs1-16	$0.0417 \pm 0.0009$	$0.279 \pm 0.019$	$263.2 \pm 5.6$	31	105.2	0.35	YuSs1-67	$0.0473 \pm 0.0012$	$0.358 \pm 0.038$	298.1 ± 7.8	$310 \pm 33$	0.96	0.44
0.023 ± 0.007	YuSs1-17	$0.0418 \pm 0.0016$	$0.351 \pm 0.052$	263.8 ± 10.0	#	86.5	0.75	YuSs1-68	41	$0.398 \pm 0.091$	$314.3 \pm 15.7$	340 ± 78	92.5	0.37
0.0052 ± 0.0071	YuSs1-18	$0.0339 \pm 0.0007$	$0,233 \pm 0.013$	214.9 ± 4.3	+1	100.9	0.56	VuSs1-69	+1.	4	$269.7 \pm 4.1$	$269 \pm 12$	100.2	0.37
0.0054 ± 0.0077 5.372 ± 0.018 5.302 ± 0.0 10.1 0.04	VuSs1-19	0.0442 ± 0.0014	$0.525 \pm 0.048$	279.1 ± 8.9	428 ± 39	65.2	0.62	YuSs1-70	*	+1	264.2 ± 7.8	302 ± 47	52.6	64.0
0.3395 ± 0.0077 5.527 ± 0.108 188.0 ± 0.100 0 0 44 748.1-7 0.032 ± 0.000 0 77.7 ± 0.000 0 77.5 ±	YuSs1-20	$0.0461 \pm 0.0012$	$0.334 \pm 0.023$	290.3 ± 7.5	$292 \pm 20$	66.3	0.63	YuSs1-71	+	+1	$2070.3 \pm 47.6$	$1920 \pm 69$	107.9	0.57
0.8359 ± 0.007	YuSs1-21	$0.3392 \pm 0.0077$	$5.372 \pm 0.189$	1882.7 ± 42.8	1880 ± 66	1001	0.46	YuSsI-72	+#	+1	$210.8 \pm 6.0$	233 ± 20	90.3	0.38
0.0057 ± 0.0072 0.755 ± 0.0002 0.0052 0.755 ± 0.0002 0.0052 0.0002 0.0052 0.0002 0.0052 0.0002 0.0052 0.0002 0.0052 0.000	YuSs1-22	$0.3395 \pm 0.0077$	5.282 ± 0.186	$1884.1 \pm 42.8$	99 ∓ 9981	0.101	0.44	FuSs1-73	-94	0.771 ± 0.086	450.4 ± 15.9	581 ± 65	27.6	0.48
0.0345 ± 0.0002	YuSs1-23	0.0678 ± 0.0025	$0.784 \pm 0.092$	422.8 ± 15.8	$588 \pm 69$	71.9	0.59	YuSs1-74	+	$0.337 \pm 0.030$	272,5 ± 7.8	295 ± 26	92.4	080
0.0432 a 0.0003 0.233 a 0.003 2.25 2.14 a 1 931 0.033 4 VKSs-7-6 0.0333 a 0.0033 0.003 0.034 a 0.009 0.034 a 0.009 0.034 a 0.003 0.034 a 0.009 0.034 a 0.003 0.034 a 0.009 0.034 a 0.003 0.034 a 0.000 0.034 a 0.003 0.003 0.0034 a 0.0	YuSs1-24	$0.0467 \pm 0.0012$	0,346 ± 0.023	294.2 ± 7.5	-8	5.76	96'0	YuSs1-75	+11	$0.288 \pm 0.022$	$251.1 \pm 6.7$	$257 \pm 20$	8.76	0.89
0.0444 ± 0.000 0.33 ± 0.028 ± 0.004 0.37 = 2.68 ± 15.2 = 2.68 ± 15.2 = 2.68 ± 15.2 = 0.044 0.007	YuSs1-25	$0.0315 \pm 0.0008$	0.235 ± 0.016	199.6 ± 5.2	+0	93.1	0.48	YuSs1-76	-41	+	$211.2 \pm 5.1$	+	0.66	0.56
0.0444 # 0.0000 0.335 # 0.002	YuSs1-26	0.0432 ± 0.0024	0.298 ± 0.073	272.6 ± 15.2	265 ± 65	103.0	0.35	YuSs1-77	$0.3483 \pm 0.0078$	Ħ	1926.5 ± 43.0	1910 ± 59	100.9	0.36
0.0444 ± 0.0017	YuSs1-27	0.0448 ± 0.0020	$0.353 \pm 0.056$	282.6 ± 12.8	307 ± 48	92.2	0.41	YuSs1-78		31	296.9 ± 8.1	314 ± 25	94.6	0.57
0.0492 ± 0.0021 0.453 ± 0.002 2 17.10 ± 15.00 0.459 ± 5.7 0.45 0.459 0.4	YuSs1-28	$0.0441 \pm 0.0016$	0.333 ± 0.032	$277.9 \pm 9.9$	292 ± 28	95.1	0.63	YuSs1-79	$0.0366 \pm 0.0011$	#	$232.0 \pm 6.9$	+1	92.6	0,33
0.04974 ± 0.0011 0.335 ± 0.0022 2 (9.04 ± 7.3 2 9.4 ± 38 6.7 0.07 A sandstone cobible from the Fundani Formation (Formation (Formati	YuSs1-29	$0.0592 \pm 0.0021$	0,453 ± 0.042		379 ± 35	8.76	0.58							
0.0447 ± 0.0010	Yu.Ss1-30	0.0304 ± 0.0011	$0.335 \pm 0.032$		294 ± 28	65.7	0.79	A San	idstone cobble from the	e Funadani Formation		11.28" N, 133" 42"	02.22" E)	
0.588 ± 0.0011         6.163 ± 0.0224         2023.4 ± 0.021         2025.8 ± 0.0011         6.165 ± 0.0218         3.06 ± 0.0218         3.	YuSs1-31	$0.0447 \pm 0.0017$	$0.336 \pm 0.038$		294 ± 33	95.7	0.48	FuSs-1-1	$0.0432 \pm 0.0017$	$0.335 \pm 0.046$	272.9	293 ± 40	93.0	0.65
0.0325 ± 0.0001	YuSs1-32	$0.3698 \pm 0.0110$	$6.163 \pm 0.224$	2028.3 ± 60.4	1999 ± 73	101.5	0.26	FuSs-1-2	4	4	316.6 ± 12.9	#	116.7	0,45
0.0468 ± 0.0016 0.339 ± 0.023 ± 0.023 ± 0.024 ± 1.01 0.345 ± 0.0044 ± 0.0014 0.0447 ± 0.0014 0.0458 ± 0.0015 0.4048 ± 0.0016 0.449 ± 0.0015 0.4049 ± 0.0015 0.4049 ± 0.0015 0.4049 ± 0.0015 0.4049 ± 0.0016 0.215 ± 0.002 0.215 ± 0.002 0.215 ± 0.002 0.215 ± 0.002 0.215 ± 0.002 0.215 ± 0.002 0.215 ± 0.002 0.215 ± 0.003 0.215 ± 0.002 0.215 ± 0.003 0.215 ± 0.002 0.215 ± 0.003 0.215 ± 0.002 0.215 ± 0.004 0.215 ±	YuSs1-33	$0.0322 \pm 0.0011$	$0.253 \pm 0.020$	204.6 ± 6.9	229 ± 18	89.2	0.75	FuSs-1-3	-#	+1	1940.0 ± 55.2	+	102.1	0.26
0.0405	YuSs1-34	$0.0468 \pm 0.0016$	0.329 ± 0.028	$294.7 \pm 10.0$	289 ± 24	102,1	0.48	FuSs-1-4	+	#	+	293 ± 25	0.96	0.94
0.04413 ± 0.0029 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.002 0.515 ± 6.003 0.515 ± 6.002 0.515 ± 6.003 0.515 ± 6.003 0.515 ± 6.003 0.515 ± 6.003 0.515 ± 6.003 0.515 ± 6.003 0.515 ± 6.004 0.515 ± 6.003 0.515 ± 6.004 0.515 ± 6.003 0.515 ± 6.004 0.515 ± 6.003 0.515 ± 6.004 0.515 ± 6.004 0.515 ± 6.003 0.515 ± 6.004 0.515 ± 6.003 0.515 ± 6.004 0.515 ± 6.003 0.515 ± 6.003 0.515 ± 6.004 0.515 ± 6.003 0.515 ± 6.003 0.515 ± 6.004 0.515 ± 6.003	YuSs1-35	0.0465 ± 0.0019	0.419 ± 0.051	293.1 ± 11.9	356 ± 43	82.4	0.75	FuSs-1-5	+1	#	#	334 ± 44	88.8	0.56
0.030 ± 0.0006 0.229 ± 0.044 1912 ± 3.8 ± 0.04 1945 0.49 FaSk-1-7 0.0423 ± 0.0021 0.353 ± 0.0029 5.66.9 ± 17.3 ± 0.249 ± 50, 19.9 ±	YuSs1-36	$0.0413 \pm 0.0009$	$0.315 \pm 0.025$	$261.2 \pm 5.9$	$278 \pm 22$	93.9	65'0	FuSs-1-6	+1.	11	$319.1 \pm 13.1$	325 ± 48	98.1	0.69
0.0365 ± 0.0007 0.222 ± 0.018 230.2 ± 4.7 24 ± 16 94.6 0.49 6 Pask-1-9 0.0465 ± 0.0005 0.307 ± 0.0056 291.7 ± 10.2 299 ± 51 14.29 0.0465 ± 0.0007 0.307 ± 0.005 0.314 ± 0.045 0.307 ± 0.0005 0.357 ± 0.001 0.307 ± 0.0005 0.307 ± 0.0005 0.357 ± 0.001 0.307 ± 0.0005 0.357 ± 0.001 0.307 ± 0.0005 0.358 ± 0.0005 0.358 ± 0.0005 0.358 ± 0.0005 0.358 ± 0.0005 0.358 ± 0.0007 0.307 ± 0.0005 0.358 ± 0.0007 0.307 ± 0.0007 0.307 ± 0.0007 0.307 ± 0.0007 0.307 ± 0.0007 0.307 ± 0.0007 0.308 ± 0.0007 0.309 ± 0.0007 0.309 ± 0.0007 0.309 ± 0.0007 0.308 ± 0.0007 0.309 ± 0.0007	YuSs1-37	$0.0301 \pm 0.0006$	$0.219 \pm 0.014$	191,2 ± 3.8	201 ± 13	676	62.0	FuSs-1-7	41.	₹	$266.9 \pm 13.4$	294 ± 60	6.06	0.67
0.3554 ± 0.0074	YuSs1-38	$0.0365 \pm 0.0007$	$0.272 \pm 0.018$	230.9 ± 4.7	244 ± 16	94.6	0.49	FuSs-1-8	++	#	427.2 ± 17.2		142.9	0.55
0.3545 ± 0.00557 5.7/10 ± 0.135 \$ 200/11 ± 31.2 \$ 103.4 \$ 0.24 \$ 10.858-1.10 \$ 0.0439 ± 0.00757 \$ 0.0490 ± 0.04505 \$ 0.05057 \$ 0.0450 ± 0.00757 \$ 0.0450 ± 0.00757 \$ 0.0450 ± 0.00757 \$ 0.00752 ± 0.017 \$ 0.0455 ± 0.0075 \$ 0.3545 ± 0.0075 \$ 0.3075 ± 0.0075 \$ 0.0049 ± 0.0007 \$ 0.0049 ± 0.0075 \$ 0.0049 ± 0.0007 \$ 0.0049 ± 0.0007 \$ 0.0049 ± 0.0007 \$ 0.0049 ±	YuSs1-39	0.0468 ± 0.0014	0,354 ± 0.042	294.6 ± 8.8	307 ± 37	626	0.46	FuSs-1-9	4 -	# 1	291,7 ± 10,5	272 ± 31	107.3	0.35
0.354 ± 0.0037 0.354 ± 0.0131 0.3554 ± 0.0131 0.3554 ± 0.0131 0.3554 ± 0.0037 0.3554 ± 0.0131 0.3554 ± 0.0037 0.3554 ± 0.0131 0.3554 ± 0.0037 0.3554 ± 0.0131 0.3554 ± 0.0037 0.3555 ± 0.0037	Yussi-40	0.3653 # 0.0057	5.770 ± 0.158	2007.1 ± 51.2	1942 ± 53	103.4	67.0	Fuss-1-10	6	H -	362.0 ± 10.1	303 ± 42	8.66	0.47
0.6356 ± 0.0007	Yussi-41	0.3545 ± 0.0055	5.548 ± 0.151	1955.9 ± 50.3	1908 ± 52	102.5	0.44	Fuss-I-11	46	# :	288.4 ± 9.7	# :	80.0	0.68
$0.0375 \pm 0.0003 \qquad 0.437 \pm 0.014 = 20,10 \qquad 0.231 + 139 \qquad 0.431 \pm 0.0013 \qquad 0.4325 \pm 0.039 \qquad 0.4325 \pm 0.03 \qquad 0.4313 \pm 49 \qquad 9.431 \\ 0.0375 \pm 0.0003 \qquad 0.437 \pm 0.0143 \qquad 0.033 \pm 0.003 \qquad 0.234 \pm 40.03 \qquad 0.234 \pm 4$	Yussi-42	0.0356 ± 0.0007	0.252 ± 0.017	225.2 ± 4.0	CI # 627	5.86	0.39	FuSs-1-12	H. ~	Ħ -	30/3 = 13.0	# 4	5.76	0,62
$0.0375 \pm 0.0001$ $0.0396 \pm 0.003$ $0.0396 \pm $	V. Co. 1 44	0.3070 ± 0.0037	0.190 ± 0.170	2010.2 ± 31.3	26 ± 1981	101.1	0.51	FUSS-1-13	4	4	6'1 ± CC/7	# 4	112.4	0.98
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10001	0.0479 = 0.0009	4 -	301.0 = 2.0	300 ± 500	0.20	477	F. 16.55-1-14	H =	9 9	204.1 ± 04.	H :-	1,77	0.04
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	V.C. 145	0,0327 ± 0,0011	#1 4	240.1 ± 7.0	300 ± 46	0.40	0.30	El-1-Sch 7	H -	H 4	311,1 ± 9,0	H +	74.0	0.32
$0.0477 \pm 0.0014$ $0.0477 \pm 0.0014$ $0.0478 \pm 0.0024$ $0.0471 \pm 0.0014$ $0.0478 \pm 0.0014$ $0.0260 \pm 0.0014$ $0.0260 \pm 0.0014$ $0.0278 \pm 0.0014$ $0.0288 \pm 0.0024$ $0.0011 \pm 0.0014$ $0.0289 \pm 0.0004$ $0.0318 \pm 0.003$ $0.0319 \pm 0.003$ $0.0419 \pm 0.0017$ $0.0418 \pm 0.003$ $0.0419 \pm 0.0017$ $0.0418 \pm 0.003$ $0.0419 \pm 0.0017$ $0.0418 \pm 0.003$ $0.0419 \pm 0.0017$ $0.0419 \pm 0.00$	VarSet 47	0.0920 ± 0.0019	0.330 ± 0.032	264 8 + 8 4	04 ± 806	0.70	0.00	First-1-17	4 4	H H	313.0 + 7.6	366 + 37	013	1.30
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSvI-48	0.0417 ± 0.0014	0.408 ± 0.032	263.5 ± 9.1	348 ± 27	75.8	0.30	FuSs-1-18	1 34	0.318 ± 0.038	272.3 ± 7.7	280 ± 33	97.1	0.33
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	VuSe1-49	0.0457 ± 0.0021	0.387 ± 0.059	288.3 ± 13.3	328 ± 51	88.0	0.34	FuSs-1-19	- 41	0.355 ± 0.028	309.4 ± 8.1	309 ± 25	1003	0.45
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSs1-50	$0.0345 \pm 0.0011$	0.260 ± 0.017	218.9 ± 7.1	235 ± 15	93.2	1.00	FuSs-1-20	#	0.380 ± 0.052	311.0 ± 11.2	327 ± 44	95.0	0.69
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSs1-51	$0.0311 \pm 0.0010$	$0.222 \pm 0.013$	197.1 ± 6.3	204 ± 12	7.96.	0.53	FuSs-1-21	-++	$0.362 \pm 0.062$	295.8 ± 12.5	314 ± 53	94.3	0.58
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Yu8s1-52	$0.0344 \pm 0.0012$	$0.258 \pm 0.022$	218.1 ± 7.5	$233 \pm 20$	93.6	0.43	FuSs-1-22	*	-86	305.9 ± 13.7	334 ± 60	7.16	0.72
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSs1-53	$0.0420 \pm 0.0013$	$0.300 \pm 0.019$	265.1 ± 8.5	267 ± 17	99.4	0.43	FuSs-1-23	+	#	$287.4 \pm 10.9$	+	93.1	0.68
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSs1-54	$0.3229 \pm 0.0037$	5.070 ± 0.175	$1803.8 \pm 20.8$	1831 ± 63	98.5	0.39	FuSs-1-24	+	+	259.7 ± 7.2	+	93.2	0.63
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSs1-55	$0.0375 \pm 0.0005$	$0.270 \pm 0.014$	237.4 = 3.2	243 ± 12	7.76	0.94	FuSs-1-25	#	+	$326.8 \pm 10.9$	#	6.96	0.55
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSs1-56	0.0369 ± 0.0009	$0.304 \pm 0.029$	233.9 ± 5.4	$569 \pm 56$	86.8	0.57	FuSs-1-26	#	#	44.	4	101.3	69.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSs1-57	$0.0473 \pm 0.0011$	$0.384 \pm 0.036$	297.9 ± 6.7	330 ± 31	90.3	0.61	FuSs-1-27	#	#	280.7 ± 11.8	#	87.7	0.67
0.0418 ± 0.0018 0.303 ± 0.061 264.0 ± 11.3 269 ± 54 98.2 0.54 FbSs-1-29 0.0445 ± 0.0015 0.331 ± 0.036 280.4 ± 9.2 290 ± 32 96.6 0.0420 ± 0.0006 0.300 ± 0.015 265.2 ± 3.5 266 ± 13 99.6 0.59 FbSs-1-30 0.0477 ± 0.0017 0.338 ± 0.050 265.2 ± 10.8 295 ± 44 89.9 0.0460 ± 0.0008 0.451 ± 0.024 379.5 ± 5.3 378 ± 20 100.3 0.64 FbSs-1-31 0.0447 ± 0.0018 0.350 ± 0.050 281.8 ± 11.1 305 ± 44 92.5 0.0466 ± 0.0007 0.333 ± 0.022 262.5 ± 4.6 269 ± 19 97.8 0.59 FbSs-1-32 0.0475 ± 0.0016 0.358 ± 0.039 299.0 ± 9.8 310 ± 34 96.3 0.0476 ± 0.0007 0.305 ± 0.027 17.2 5.9 ± 4.6 0.0476 ± 0.0007 0.305 ± 0.027 17.2 5.9 ± 4.6 0.0476 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0276 ± 0.0007 0.305 ± 0.0007	YuSs1-58	$0.0289 \pm 0.0004$	$0.200 \pm 0.011$	$183.6 \pm 2.6$		0.66	69.0	FuSs-1-28	4	升	$279.1 \pm 11.8$	-11	82.4	09'0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSs1-59	$0.0418 \pm 0.0018$	$0.303 \pm 0.061$	264.0 ± 11.3		98.2	0.54	FuSs-1-29	+1_	+1.	280,4 ± 9.2	#	9.96	0.49
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Yussi-60	0.0420 ± 0.0006	0,300 ± 0.015	265.2 ± 5.5		966	0.59	FuSs-1-30	++ -	0	203.0 ± 10.8	## -	89.9	0.53
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YuSsi-61	0.0606 ± 0.0008	0.451 ± 0.024	5/9.5 ± 5.5	4 -	100.3	0.04	FuSs-1-31	0.044/ ± 0.0018	0.550 ± 0.050	1.11 ± 8,182	# -	6.76	0.72
	YuSS1-02	0.0416 ± 0.0007	0.303 ± 0.022		н -	0.70	60.0	Fubs-1-52	H -		299.0 ± 9.8	H -	50.0	0.49

TABLE 1. (Continued)

0 /01	0	rov O ago	%conc	Th/U	Grain	D <sub>862</sub> /9d <sub>902</sub>	Joy Pb/235U	Pb/ Uage	Pb/~ Uage	%conc	Th/U
0310 + 0.035	780 0 ± 0 3	(Ma)	1053	09.0	FuSe-1-85	0.0474 + 0.0017	0.325 ± 0.046	208 6 ± 10.6	(Ma)	105.5	0.69
0.519 ± 0.080	271.7 ± 12.9	425 ± 65	64.0	0.48	FuSs-1-86	+	+	265.4 ± 8.6	343 ± 38	77.4	0.84
$0.441 \pm 0.073$	302.6 ± 12.9	$371 \pm 62$	81.6	0.45	FuSs-1-87	- 4		292.1 ± 11.9	330 ± 52	88.6	0.43
$0.424 \pm 0.061$	287.0 ± 10.9	359 ± 52	80.0	090							
$0.321 \pm 0.030$	$273.2 \pm 6.9$	+1	9.96	86.0	4	rhyolite cobble from the	Vunoki Formation (	Yulg-1; 33, 42, 43.2	20" N, 133" 50' 06	.09" E)	
$0.308 \pm 0.054$	310.0 ± 11.9	272 ± 48	113.8	0.37	Yulg-1-1	#	$0.293 \pm 0.047$	268,7 ± 11,4	261 ± 42	103.0	0.70
0.390 ± 0.030	333.3 ± 7.5	334 ± 26	1.00	0.76	Yulg-1-2	0.0199 ± 0.0008	0.143 ± 0.022	127.0 ± 5.2	136 ± 20	93.5	0.51
0.297 ± 0.024	272.5 ± 6.1	+	103.1	0.70	Yulo-1-4	1 +1	( +	1 4	154 ± 17	80.5	000
0.360 ± 0.055	- 44	+1	88.6	0.81	Yulg-1-5	0.0213 ± 0.0009	-34	135.7 ± 5.6	4	82.2	040
0.400 ± 0.065	312.4 ± 12.5	341 ± 56	91.5	0.51	Vulg-1-6	+	+	$173.8 \pm 6.1$	+	103.7	0.41
0,391 ± 0,059	-11	335 ± 51	686	98'0	Yulg-1-7	+1	0.142 ± 0.018	117.3 ± 4.4	+1	86.8	0.57
$0.396 \pm 0.064$	#	339 ± 55	94.4	0.52	Yalg-1-8	+10	40	124.6 ± 4.8	#	87.5	0.50
$0.290 \pm 0.043$	-14	258 ± 38	106.7	09.0	Yulg-1-9	H	+	127.6 ± 4.2	#	88.7	0.55
0.356 ± 0.044	-84	309 ± 38	0.76	0.49	Yulg-1-10	41	0.148 ± 0.011	122.1 ± 2.8	140 # 11	87.2	0.77
$0.377 \pm 0.040$	295.8 ± 8.8	325 ± 35	91.0	1.03	Yulg-1-11	$0.0197 \pm 0.0005$	#	$125.8 \pm 3.1$	$123 \pm 11$	102.1	1.02
$0.422 \pm 0.098$	144	$358 \pm 83$	77.4	19.0	Yulg-1-12	41	#	$122.0 \pm 3.1$	133 ± 12	8.16	0.79
$0.412 \pm 0.057$	*	350 ± 48	92.2	0.47	Yulg-1-13	+1	0.163 ± 0.019	123.2 ± 3.9	153 ± 18	80.5	0.61
$0.422 \pm 0.086$	-41	358 ± 73	93.0	0.59	Yulg-1-14	+	#	134.7 ± 4.5	127 ± 18	106.5	0.53
$0.380 \pm 0.043$	330.6 ± 9.9	327 ± 37	101.0	0.46	Yulg-1-15	$0.0202 \pm 0.0008$	0.164 ± 0.025	128.9 ± 4.9	154 ± 24	83.5	0.56
$0.386 \pm 0.045$	+1	$331 \pm 38$	9.06	0.52	Yalg-1-16	+1	#	125.7 ± 3.9	141 ± 17	88.9	0.62
0,329 ± 0,050	-11	288 ± 44	666	0.43	Yulg-1-17	+	#	$128.9 \pm 4.1$	142 ± 18	8.06	0.65
$0.311 \pm 0.034$	#	$275 \pm 30$	108.7	09'0	Yulg-1-18	0.0191 ± 0.0007	$0.149 \pm 0.022$	122.2 ± 4.5	141 ± 21	86.5	0.50
$0.358 \pm 0.054$	297.5 ± 10.7	311 ± 47	95.7	0.32	Yulg-1-19	+0	#	122.9 ± 4.3	179 ± 22	88.89	0.48
$0.391 \pm 0.024$	330,3 ± 6,3	335 ± 21	98.5	0.88	Yulg-1-20	0,4363 ± 0,0082	8,424 ± 0.247	2334.2 ± 43.9	2278 ± 67	102.5	0.59
$0.399 \pm 0.054$	$321.1 \pm 10.7$	341 ± 46	94.3	0.46	Yudg-1-21	44	+)	133.6 ± 4.6		82.9	09'0
0.374 ± 0.059	+4.	323 ± 51	92.4	0.72	Yulg-1-22	+4	$0.143 \pm 0.015$	(14.0 ± 3.3		84.0	0.76
0.359 ± 0.032	294.5 ± 7.1	312 ± 28	94.5	0.77	Yulg-1-23	#	+1	126.8 ± 3.9		0.06	0.71
0.368 ± 0.032	291.3 ± 6.9	318 ± 28	91.5	0,46	Yulg-1-24	$0.0201 \pm 0.0007$	$1.037 \pm 0.072$	128.4 ± 4.5	$722 \pm 51$	17.8	09.0
0.591 ± 0.074	291.8 ± 12.7	333 ± 03	27.78	670	7ulg-1-23	#	#	129.9 ± 5.3		40.4	600
$0.392 \pm 0.054$	290.7 ± 10.3	336 ± 47	9.00	0.45	Yulg-1-26	+	#1	133.9 ± 4.5		5.69	0.53
0.463 ± 0.040	283.0 ± 7.8	$386 \pm 33$	73.3	0.65	Yulg-1-27	+)	+	181.4 ± 5.4	$183 \pm 21$	99.1	0.56
0.323 ± 0.046	# 1	284 ± 41	107.0	0.40	Yulg-1-28	0.0217 ± 0.0006	#	138.3 ± 3.5		88.7	1.00
0.390 ± 0.041	#	334 ± 35	6.96	0.43	Yulg-1-29	#	# :	125.2 ± 3.7		94.7	89.0
0.392 ± 0.060	н	330 ± 52	2.10	0.00	74/g-1-30	H. B	0.074 ± 0.048	400.1 = 9.8		0.70	0.58
0.339 ± 0.028	200.3 ± 7.1	67 ± /67	0.46	0.51	11dg-1-31	B >	0.170 ± 0.028	141.2 ± 3.3		00.0	0.44
0.377 + 0.049	360 F + 10.2	227 ± 43	7'001	0.39	Valle 1 23	0.0193 = 0.0000	0.000 # 0.000	1750 ± 3.6		95.6	1.13
0.3/1 ± 0,000	307 0 ± 10.2	200 ± 46	-06.4	0.40	Vale 134	00015 + 0,0007	0.130 + 0.000	137.0 + 4.7	125 + 10	102.0	1.14
0.341 ± 0.033	2810 + 0.707	200 ± 300	900	00.00	1 mg-1-24	H	0.139 ± 0.020	13/12 = 4.7	132 ± 13	105.0	0.03
0.348 + 0.041	36 7 4 7 6	218 + 36	83.7	0.00	A contract	andianita ashbla fram th	o Hibiham Commit	on /Hills. 1. 22" 20:	34 60" N 132" AG	M 624 EV	
7670 + 0169	2143.0 + 27.5	2187 ± 48	0.80	0.46	Hilos 1-1	0.0193 + 0.0005			133 + 12	02.7	1.10
670 m 7730	373 4 4 11 6	525 ± 57	111	0.41	Gilla.1.2	+	d	1204 + 34	1	01.7	0.56
0.873 + 0.067	301 + 5 707	07 + 009	209	0.51	Hilo-1-3	1.4	1 +	1291+34	1 4	0.40	0.61
	14	303 + 43	70 5	0.45	Hilo.1-4	+	4100 + 0510	75 + 3 8 1	0.4	102 6	0.57
0.453 ± 0.046	317.5 ± 9.6	379 ± 39	83.8	0.65	Hile-1-5	11.39		125.9 ± 3.8	98	61.7	0.45
0.333 ± 0.028	284.3 ± 7.3	#	97.5	0.79	Hile-1-6	0.0201 ± 0.0005	+	128.2 ± 3.3	-44	83.5	0.48
0.341 ± 0.031	293.0 ± 7.8	298 ± 27	5.86	0.44	Hilo-1-7	- 48	+9	119.6 ± 3.9	143	83.3	0.51
0.330 ± 0.049	- 44	290 ± 43	93.2	0.51	Hilg-1-8			132.4 ± 3.2	161 ± 15	82.4	090
0.368 ± 0.037	-#	318 ± 32	1001	0.35	Hile-1-9	+	+		-11	6'06	0.59
0.374 ± 0.074	- 4	332 ± 64	9 2 6	0.43	Hilo-1-10	+	+	1342 ± 36	185 + 19	725	0.47

TABLE 1. (Continued)

| (Ma) %conc Th/U<br>(Ma) 96.9 0.59     |               | 55              |                   | 82.4            | 82.4            | 82.4<br>85.6<br>102.3<br>86.2                                | 82.4<br>85.6<br>102.3<br>86.2<br>94.4                    | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1                        | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1   | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1<br>91.2  | 82.4<br>85.6<br>102.3<br>86.2<br>86.2<br>93.1<br>93.1<br>93.5  | 82.4<br>85.6<br>102.3<br>86.2<br>86.2<br>99.1<br>99.1<br>76.2<br>76.2   | 82.4<br>85.6<br>102.3<br>86.2<br>86.2<br>93.1<br>91.2<br>76.2<br>95.5<br>95.8  | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1<br>93.5<br>76.2<br>95.8<br>95.8   | 82.4<br>85.6<br>102.3<br>86.2<br>86.2<br>93.1<br>91.2<br>93.5<br>95.8<br>96.3<br>88.0  | 82.4<br>85.6<br>102.3<br>86.2<br>84.4<br>94.4<br>91.2<br>93.5<br>76.2<br>95.8<br>96.3<br>86.8  | 82.4<br>85.6<br>102.3<br>102.3<br>86.2<br>93.1<br>93.5<br>76.2<br>93.5<br>96.3<br>86.8<br>86.8   | 82.4<br>85.6<br>102.3<br>102.3<br>86.2<br>93.1<br>93.5<br>93.5<br>96.3<br>86.8<br>86.8   | 82.4<br>85.6<br>102.3<br>86.2<br>93.1<br>93.1<br>93.5<br>96.3<br>96.3<br>98.3<br>98.3  
   | 82.4<br>85.6<br>102.3<br>102.3<br>86.2<br>93.1<br>93.1<br>93.5<br>96.3<br>96.3<br>98.3<br>98.3<br>98.3   | 82.4<br>85.6<br>102.3<br>86.2<br>93.1<br>93.1<br>93.5<br>93.5<br>96.2<br>96.2<br>96.3<br>96.3<br>96.8<br>96.8<br>96.8<br>96.8<br>96.8<br>96.8<br>96.8<br>96.8   | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1<br>91.2<br>91.7<br>91.6<br>98.8<br>98.8<br>98.3<br>91.6<br>91.6<br>92.0  | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1<br>93.5<br>91.7<br>96.8<br>88.0<br>98.3<br>98.3<br>98.3<br>98.2<br>97.9<br>97.9<br>97.9   
  | 82.4<br>85.6<br>102.3<br>102.3<br>86.2<br>93.1<br>93.1<br>94.0<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3   | 82.4<br>85.6<br>102.3<br>102.3<br>86.2<br>93.1<br>93.1<br>93.2<br>93.2<br>93.4<br>93.4<br>93.4<br>93.4<br>93.5<br>93.5<br>93.5<br>93.5<br>93.5<br>93.5<br>93.5<br>93.5   | 82.4<br>85.6<br>102.3<br>102.3<br>86.2<br>93.1<br>93.1<br>93.2<br>93.2<br>93.2<br>85.2<br>93.2<br>85.2<br>85.2<br>85.2<br>85.3<br>85.3<br>85.3<br>85.3<br>85.3<br>85.3<br>85.3<br>85.3   | 82.4<br>85.6<br>102.3<br>86.2<br>93.1<br>93.1<br>93.2<br>93.2<br>93.2<br>93.4<br>93.2<br>86.8<br>93.2<br>93.2<br>93.2<br>86.3<br>86.3<br>86.3<br>86.3<br>86.3<br>86.3<br>86.3<br>86.3   
  | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1<br>99.1<br>91.6<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3  | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>99.1<br>99.1<br>99.7<br>98.8<br>98.8<br>98.8<br>98.8<br>98.8<br>98.8<br>98.8  | 82.4<br>85.6<br>102.3<br>85.6<br>94.4<br>99.1<br>99.1<br>96.2<br>98.8<br>98.8<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3  | 82.4<br>85.6<br>102.3<br>86.2<br>93.1<br>93.1<br>93.1<br>96.8<br>88.0<br>98.2<br>91.7<br>92.0<br>93.4<br>90.5<br>88.8<br>88.8<br>93.4<br>90.5<br>90.5   
   | 82.4<br>85.6<br>102.3<br>86.2<br>93.1<br>93.1<br>93.1<br>96.8<br>88.0<br>98.0<br>98.2<br>98.2<br>98.2<br>98.3<br>98.3<br>98.3<br>98.3<br>98.4<br>99.5<br>90.5<br>90.5<br>90.5  | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1<br>93.1<br>96.2<br>96.8<br>98.8<br>98.8<br>98.2<br>98.2<br>98.2<br>98.3<br>98.3<br>98.3<br>98.4<br>98.2<br>98.6<br>88.8<br>98.6<br>99.5<br>97.7<br>97.7<br>97.7<br>97.7<br>97.7<br>97.7<br>97.7   | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>93.1<br>96.3<br>88.0<br>98.3<br>98.2<br>98.2<br>98.3<br>98.2<br>98.3<br>98.2<br>98.3<br>98.2<br>98.3<br>98.2<br>98.3<br>99.5<br>77.7<br>100.7   | 82.4<br>82.4<br>85.6<br>102.3<br>86.2<br>99.1<br>99.1<br>99.2<br>98.8<br>98.8<br>98.8<br>98.8<br>98.8<br>98.8<br>98.8   
   | 82.4<br>85.6<br>102.3<br>85.6<br>94.4<br>99.1<br>99.1<br>99.2<br>98.8<br>98.8<br>98.8<br>98.8<br>98.8<br>98.8<br>99.6<br>99.6   | 82.4<br>85.6<br>102.3<br>85.6<br>94.4<br>93.1<br>91.2<br>93.5<br>96.8<br>98.8<br>98.3<br>98.2<br>98.2<br>98.2<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>99.5<br>90.5<br>90.5<br>90.5<br>90.5<br>90.5<br>90.5<br>90.5   | 82.4<br>85.6<br>102.3<br>86.2<br>94.4<br>91.2<br>93.1<br>91.7<br>96.8<br>88.8<br>98.2<br>99.5<br>88.8<br>88.8<br>88.8<br>88.8<br>88.8<br>88.8<br>88.8   | 82.4<br>82.4<br>85.6<br>102.3<br>86.2<br>99.1<br>99.1<br>99.2<br>98.8<br>88.8<br>88.8<br>88.8<br>99.5<br>90.5<br>90.5<br>90.5<br>90.5<br>90.5<br>90.5<br>90.5   
   | 82.4<br>85.6<br>102.3<br>85.6<br>94.2<br>99.1<br>99.1<br>99.2<br>98.8<br>88.8<br>99.8<br>99.8<br>99.8<br>99.8<br>99.8  | 82.4<br>85.6<br>102.3<br>85.6<br>94.4<br>93.1<br>91.2<br>93.1<br>96.2<br>96.8<br>98.8<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98.3<br>98  | 82.4<br>85.6<br>102.3<br>86.2<br>93.1<br>93.1<br>93.1<br>93.2<br>93.2<br>93.2<br>93.4<br>93.4<br>90.5<br>88.8<br>88.8<br>88.8<br>88.8<br>88.8<br>93.4<br>90.7<br>101.1<br>99.7<br>99.7<br>99.7<br>99.7<br>99.7<br>99.7<br>99.7<br>9   | 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| ± 0.052                               | 0000          | ± 0.092         |                   | ₩ 0.039         |                 | ± 0.030  | ± 0.030<br>± 0.030<br>± 0.048                            | ± 0.030<br>± 0.048<br>± 0.028  | ± 0.030<br>± 0.030<br>± 0.048<br>± 0.028<br>± 0.025                                   | ± 0.030<br>± 0.030<br>± 0.048<br>± 0.028<br>± 0.025<br>± 0.025                                 | # 0.030<br># 0.030<br># 0.028<br># 0.025<br># 0.025<br># 0.024   | ± 0.030<br>± 0.048<br>± 0.048<br>± 0.028<br>± 0.025<br>± 0.024<br>± 0.044   | ± 0.030<br>± 0.030<br>± 0.048<br>± 0.048<br>± 0.025<br>± 0.023<br>± 0.024<br>± 0.034<br>± 0.043                                  | ± 0.030<br>± 0.030<br>± 0.030<br>± 0.028<br>± 0.025<br>± 0.024<br>± 0.044<br>± 0.044<br>± 0.044<br>± 0.044<br>± 0.044<br>± 0.044<br>± 0.044               | ± 0.030<br>± 0.030<br>± 0.030<br>± 0.028<br>± 0.025<br>± 0.024<br>± 0.037<br>± 0.037<br>± 0.037<br>± 0.037<br>± 0.037                            | ± 0.030<br>± 0.038<br>± 0.028<br>± 0.023<br>± 0.024<br>± 0.024<br>± 0.037<br>± 0.043<br>± 0.044<br>± 0.043<br>± 0.044<br>± 0.045<br>± 0.044<br>± 0.045<br>± 0.044<br>± 0.045<br>± 0 | ## 0.030<br>## 0.028<br>## 0.028<br>## 0.023<br>## 0.024<br>## 0.024<br>## 0.034<br>## 0.037<br>## 0.043<br>## 0.046<br>## 0.076<br>## 0.076   | ± 0.030<br>± 0.030<br>± 0.033<br>± 0.023<br>± 0.024<br>± 0.024<br>± 0.034<br>± 0.037<br>± 0.076<br>± 0 | ± 0.030<br>± 0.030<br>± 0.038<br>± 0.028<br>± 0.024<br>± 0.034<br>± 0.044<br>± 0.044<br>± 0.045<br>± 0.037<br>± 0.037<br>± 0.037<br>± 0.037<br>± 0.037<br>± 0.036<br>± 0.037<br>± 0.036<br>± 0.037<br>± 0.036<br>± 0.037<br>± 0 | ± 0.030<br>± 0.030<br>± 0.028<br>± 0.023<br>± 0.024<br>± 0.024<br>± 0.034<br>± 0.043<br>± 0.043<br>± 0.031<br>± 0.031<br>± 0.031<br>± 0.034<br>± 0 | ## 0.030<br>## 0.048<br>## 0.028<br>## 0.023<br>## 0.024<br>## 0.024<br>## 0.037<br>## 0.048<br>## 0.048<br>## 0.048<br>## 0.048<br>## 0.034<br>## 0.024<br>## 0.024  | ## 0.030<br>## 0.030<br>## 0.028<br>## 0.023<br>## 0.024<br>## 0.024<br>## 0.037<br>## 0.037<br>## 0.037<br>## 0.034<br>## 0.034<br>## 0.034<br>## 0.034<br>## 0.034<br>## 0.034   | ## 0.036<br>## 0.028<br>## 0.028<br>## 0.023<br>## 0.024<br>## 0.024<br>## 0.034<br>## 0.037<br>## 0.034<br>## 0.024<br>## 0.024<br>## 0.024<br>## 0.024<br>## 0.024<br>## 0.024<br>## 0.024<br>## 0.024  
  | # 0.030<br># 0.030<br># 0.028<br># 0.028<br># 0.024<br># 0.033<br># 0.043<br># 0.043<br># 0.032<br># 0.033<br># 0.033<br># 0.033<br># 0.033<br># 0.033   | # 0.030<br># 0.030<br># 0.028<br># 0.028<br># 0.023<br># 0.033<br># 0.043<br># 0.043<br># 0.032<br># 0.033<br># 0.033<br># 0.033<br># 0.033<br># 0.033<br># 0.033  | # 0.030<br># 0.030<br># 0.028<br># 0.028<br># 0.023<br># 0.033<br># 0.043<br># 0.043<br># 0.031<br># 0.034<br># 0.034<br># 0.034<br># 0.034<br># 0.034<br># 0.033<br># 0.034<br># 0.033  | # 0.030<br># 0.030<br># 0.028<br># 0.028<br># 0.024<br># 0.024<br># 0.037<br># 0.037<br># 0.034<br># 0.034  
  | # 0.030<br># 0.030<br># 0.028<br># 0.028<br># 0.024<br># 0.024<br># 0.034<br># 0.035  | ### 0.030 #### 0.030 ##################################  | ## 0.033<br>## 0.033<br>## 0.023<br>## 0.023<br>## 0.023<br>## 0.023<br>## 0.023<br>## 0.033<br>## 0.033<br>## 0.033<br>## 0.033<br>## 0.033<br>## 0.033<br>## 0.033<br>## 0.033<br>## 0.033   | ## 0.033 ## 0.033 ## 0.033 ## 0.033 ## 0.033 ## 0.033 ## 0.033 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.034 ## 0.035 ## 0.035   | ## 0.030 ## 0.033 ## 0.023 ## 0.023 ## 0.023 ## 0.024 ## 0.024 ## 0.037 ## 0.037 ## 0.037 ## 0.034 ## 0.034 ## 0.034 ## 0.034
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| ± 0.0029<br>± 0.0059                  | + 0.0059      | 0.0000          |                   | = 0.0018        | ± 0.0014        | ± 0.0013   | ± 0.0021   | ± 0.0013<br>± 0.0021<br>± 0.0012                                     | # 0.0013<br># 0.0021<br># 0.0012<br># 0.0011  | # 0.00033<br># 0.0021<br># 0.0012<br># 0.0011<br># 0.0011                                      | # 0.0003<br># # 0.0021<br># # 0.0011<br># 0.0011<br># 0.0011   | # 0.0013<br># 0.0021<br># 0.0011<br># 0.0011<br># 0.0011<br># 0.0014  | # 0.0013<br># 0.0012<br># 0.0011<br># 0.0011<br># 0.0011<br># 0.0014<br># 0.0014   | = 0.0013<br>+ 0.0021<br>+ 0.0012<br>+ 0.0011<br>+ 0.0011<br>+ 0.0014<br>+ 0.0014<br>+ 0.0018<br>+ 0.0018  | = 0.0013<br>+ 0.0021<br>+ 0.0021<br>+ 0.0012<br>+ 0.0011<br>+ 0.0014<br>+ 0.0014<br>+ 0.0018<br>+ 0.0043<br>+ 0.0043                             | 2 0.0013<br>2 0.0012<br>2 0.0012<br>2 0.0011<br>2 0.0014<br>3 0.0014<br>5 0.0014<br>5 0.0018<br>6 0.0013<br>7 0.0040<br>6 0.0013<br>7 0.0040<br>8 0.0040   | 20003<br>20003<br>20003<br>20003<br>20003<br>20003<br>20003<br>20003<br>20003<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20004<br>20 | = 0.0013<br>= 0.0013<br>= 0.0021<br>= 0.0011<br>= 0.0011<br>= 0.0011<br>= 0.0014<br>= 0.0014<br>= 0.0018<br>= 0.0040<br>= 0.0013<br>= 0.0040<br>= 0.0013   | = 0.0013<br>+ 0.0021<br>+ 0.0021<br>+ 0.0011<br>+ 0.0011<br>+ 0.0011<br>+ 0.0014<br>+ 0.0014<br>+ 0.0013<br>+ 0.0013<br>+ 0.0013<br>+ 0.0012<br>+ 0.0012<br>+ 0.0020   
   | = 0.0013<br>= 0.0021<br>= 0.0021<br>= 0.0021<br>= 0.0011<br>= 0.0011<br>= 0.0014<br>= 0.0014<br>= 0.0014<br>= 0.0013<br>= 0.0014<br>= 0.0013<br>= 0.0012<br>= 0.0012<br>= 0.0012<br>= 0.0012<br>= 0.0012   | = 0.0013<br>+ 0.0021<br>+ 0.0021<br>+ 0.0011<br>+ 0.0011<br>+ 0.0014<br>+ 0.0014<br>+ 0.0014<br>+ 0.0013<br>+ 0.0013<br>+ 0.0012<br>+ 0.0012<br>+ 0.0012<br>+ 0.0012<br>+ 0.0012<br>+ 0.0014  | 2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.000.3<br>2.0 | 2.000.3<br>± 0.00021<br>± 0.00021<br>± 0.00011<br>± 0.00011<br>± 0.00014<br>± 0.00014<br>± 0.00014<br>± 0.00013<br>± 0.00012<br>± 0.00012   
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  | = 0.0013<br>= 0.0021<br>= 0.0021<br>= 0.0011<br>= 0.0011<br>= 0.0014<br>= 0.0014<br>= 0.0014<br>= 0.0013<br>= 0.0020<br>= 0.0012<br>= 0.0015<br>= 0.0015<br>= 0.0018<br>= 0.0018   | = 0.0013<br>= 0.0021<br>= 0.0021<br>= 0.0011<br>= 0.0011<br>= 0.0014<br>= 0.0014<br>= 0.0014<br>= 0.0014<br>= 0.0013<br>= 0.0015<br>= 0.0015   | ## 0.00011<br>## 0.00011<br>## 0.00011<br>## 0.00011<br>## 0.00011<br>## 0.00014<br>## 0.00014<br>## 0.00014<br>## 0.00012<br>## 0.00012<br>## 0.00012<br>## 0.00012<br>## 0.00012<br>## 0.00012<br>## 0.00012<br>## 0.00012<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013   | ## 0.00013<br>## 0.00011<br>## 0.00011<br>## 0.00011<br>## 0.00014<br>## 0.00014<br>## 0.00014<br>## 0.00014<br>## 0.00013<br>## 0.00012<br>## 0.00012<br>## 0.00012<br>## 0.00012<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013<br>## 0.00013  
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| 129 ± 22 9:<br>329 ± 29 4(138 ± 14 9: |               |                 |                   |                 |                 |  |  |  |   |  |  |   | # # # # 12 12 12 12 12 12 12 12 12 12 12 12 12   | 126 ± 12<br>108 ± 12<br>137 ± 17<br>28' 22.83" E)   | (47 ± 10<br>126 ± 12<br>108 ± 12<br>137 ± 17<br>28* 22.83* E)<br>294 ± 17  | 147 ± 10<br>126 ± 12<br>108 ± 12<br>137 ± 17<br>28' 22.83" E)<br>294 ± 17<br>286 ± 28  | (47 ± 10<br>126 ± 12<br>108 ± 12<br>108 ± 17<br>28 * 22.83° E)<br>29 ± 17<br>286 ± 28<br>343 ± 28  | 126 ± 12<br>126 ± 12<br>108 ± 17<br>137 ± 17<br>294 ± 17<br>28 5 ± 28<br>343 ± 28  | 126 ± 12<br>126 ± 12<br>108 ± 17<br>137 ± 17<br>294 ± 17<br>284 ± 28<br>343 ± 28<br>362 ± 25<br>1163 ± 56  | 126 ± 12<br>126 ± 12<br>108 ± 17<br>137 ± 17<br>294 ± 28<br>294 ± 28<br>343 ± 28<br>362 ± 28<br>362 ± 25<br>423 ± 44<br>433 ± 18   | 126 ± 12<br>126 ± 12<br>108 ± 17<br>137 ± 17<br>294 ± 17<br>284 ± 17<br>286 ± 28<br>343 ± 28<br>302 ± 25<br>31163 ± 56<br>423 ± 44<br>423 ± 44<br>318 ± 24  | 126 ± 12<br>126 ± 12<br>108 ± 17<br>137 ± 17<br>294 ± 17<br>284 ± 17<br>286 ± 28<br>302 ± 28<br>302 ± 25<br>1163 ± 56<br>423 ± 44<br>423 ± 44<br>780 ± 35  | 126 ± 10<br>126 ± 12<br>108 ± 12<br>137 ± 17<br>28 ± 22.83" E)<br>29 ± 17<br>28 ± 28<br>302 ± 28<br>303 ± 28<br>303 ± 18<br>423 ± 18<br>423 ± 18<br>423 ± 18<br>284 ± 23<br>284 ± 23   | 147 ± 10<br>126 ± 12<br>108 ± 17<br>197 ± 17<br>28' 22.83" E)<br>28' 22.83" E)<br>28' 22.83 ± 28<br>302 ± 28<br>302 ± 28<br>303 ± 28<br>318 ± 24<br>780 ± 28<br>780 ± 28<br>163 ± 66<br>423 ± 18<br>533 ± 18<br>533 ± 18<br>534 ± 24<br>780 ± 24   | 147 ± 10<br>126 ± 12<br>108 ± 17<br>108 ± 17<br>137 ± 17<br>286 ± 28<br>302 ± 25<br>302 ± 25<br>303 ± 28<br>304 ± 24<br>423 ± 44<br>423 ± 44<br>553 ± 18<br>553 ± 18<br>564 ± 24<br>780 ± 35<br>780 ± 24<br>780 ±  | 147 ± 10<br>126 ± 12<br>108 ± 17<br>197 ± 17<br>137 ± 17<br>28 ± 28<br>302 ± 28<br>302 ± 28<br>302 ± 28<br>302 ± 28<br>423 ± 44<br>533 ± 18<br>533 ± 18<br>533 ± 18<br>533 ± 24<br>780 ± 2   | 147 ± 10<br>126 ± 12<br>108 ± 17<br>137 ± 17<br>28, 22,83° E)<br>294 ± 17<br>286 ± 28<br>343 ± 28<br>392 ± 25<br>1163 ± 44<br>533 ± 18<br>533 ± 18<br>533 ± 18<br>540 ± 35<br>560 ± 35<br>665 ± 60<br>473 ± 44<br>533 ± 34<br>572 ± 39<br>516 ± 39<br>516 ± 39<br>516 ± 39<br>516 ± 39<br>517 ± 39<br>518 ± 34<br>518 ± 34<br>518 ± 34<br>518 ± 34<br>518 ± 34<br>518 ± 34<br>518 ± 34   | 147 ± 10<br>126 ± 12<br>108 ± 17<br>137 ± 17<br>28, 22,83° E)<br>294 ± 17<br>286 ± 28<br>343 ± 28<br>392 ± 25<br>1163 ± 44<br>533 ± 18<br>533 ± 18<br>533 ± 18<br>533 ± 34<br>543 ± 34<br>533 ± 34<br>533 ± 34<br>534 ± 24<br>535 ± 39<br>537 ± 40<br>537 ± 40<br>538 ± 34<br>538 ± 36<br>538 ± 36 | 147 ± 10<br>126 ± 12<br>108 ± 17<br>137 ± 17<br>287 22.83" E)<br>294 ± 17<br>286 ± 28<br>343 ± 28<br>343 ± 28<br>310 ± 25<br>1163 ± 56<br>423 ± 14<br>533 ± 18<br>533 ± 18<br>534 ± 24<br>535 ± 34<br>545 ± 39<br>546 ± 20<br>576 ± 20<br>577 ± 47<br>576 ± 20<br>577 ± 47<br>576 ± 20<br>577 ± 47<br>577 ± 47 | 126 ± 10<br>126 ± 12<br>108 ± 12<br>108 ± 17<br>28 * 22.83 * E)<br>29 ± 17<br>28 * 22.83 * E)<br>29 ± 17<br>20 ± 26<br>423 ± 18<br>302 ± 26<br>423 ± 18<br>318 ± 24<br>780 ± 35<br>284 ± 23<br>516 ± 20<br>318 ± 24<br>780 ± 33<br>516 ± 20<br>318 ± 43<br>516 ± 20<br>318 ± 33<br>516 ± 20<br>318 ± 31<br>516 ± 31<br>517 ± 31<br>518 ± | 126 ± 10<br>126 ± 12<br>108 ± 12<br>108 ± 17<br>137 ± 17<br>286 ± 28<br>304 ± 27<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>423 ± 18<br>423 ± 18<br>423 ± 18<br>423 ± 18<br>423 ± 18<br>423 ± 18<br>423 ± 18<br>533 ± 18<br>533 ± 18<br>533 ± 18<br>533 ± 18<br>533 ± 18<br>533 ± 18<br>534 ± 24<br>780 ± 35<br>284 ± 23<br>516 ± 20<br>365 ± 40<br>526 ± 30<br>526 ± 30<br>527 ± 18<br>527 ± 18  | 126 ± 10<br>126 ± 12<br>108 ± 12<br>108 ± 17<br>137 ± 17<br>286 ± 28<br>304 ± 27<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>423 ± 18<br>423 ± 18<br>553 ± 18<br>780 ± 3<br>516 ± 20<br>645 ± 60<br>645 ± 60<br>645 ± 60<br>647 ± 20<br>648 ± 30<br>648 ± 30<br>648 ± 30<br>649 ± 30<br>640 ± 3 | 126 ± 10<br>126 ± 12<br>108 ± 17<br>108 ± 17<br>137 ± 17<br>286 ± 28<br>304 ± 27<br>286 ± 28<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>423 ± 18<br>318 ± 24<br>423 ± 18<br>318 ± 24<br>423 ± 18<br>318 ± 24<br>423 ± 30<br>524 ± 23<br>364 ± 23<br>372 ± 42<br>284 ± 23<br>385 ± 39<br>366 ± 33<br>367 ± 47<br>258 ± 30<br>369 ± 30<br>360 ± 31<br>451 ± 42<br>452 ± 42<br>453 ± 42<br>453 ± 42<br>453 ± 42<br>453 ± 42<br>454 ± 30<br>454 ± 30<br>454 ± 30<br>457 ± 42<br>458 ± 30<br>457 ± 42<br>458 ± 30<br>458 ± | 126 ± 12<br>108 ± 12<br>108 ± 17<br>108 ± 17<br>137 ± 17<br>286 ± 28<br>304 ± 27<br>286 ± 28<br>305 ± 28<br>423 ± 44<br>423 ± 44<br>423 ± 44<br>423 ± 39<br>435 ± 30<br>1645 ± 60<br>1645 ± 60<br>1645 ± 60<br>1645 ± 33<br>336 ± 34<br>372 ± 42<br>228 ± 30<br>330 ± 34<br>457 ± 30<br>330 ± 24<br>457 ± 30<br>457 ± 30<br>330 ± 30<br>457 ± 30<br>45 | 126 ± 12<br>108 ± 12<br>108 ± 17<br>137 ± 17<br>28, 22,83° E)<br>294 ± 17<br>286 ± 28<br>343 ± 28<br>390 ± 25<br>11645 ± 60<br>433 ± 18<br>533 ± 18<br>533 ± 18<br>535 ± 39<br>366 ± 20<br>372 ± 42<br>298 ± 39<br>372 ± 42<br>298 ± 30<br>372 ± 42<br>298 ± 30<br>373 ± 18<br>374 ± 28<br>375 ± 42<br>274 ± 38<br>377 ± 38<br>377 ± 38<br>377 ± 38<br>377 ± 38<br>377 ± 38<br>377 ± 38   | 126 ± 10<br>176 ± 10<br>178 ± 12<br>178 ± 17<br>188 ± 12<br>288 ± 22,83° E)<br>294 ± 17<br>286 ± 28<br>392 ± 28<br>393 ± 18<br>393 ± 18<br>393 ± 18<br>393 ± 18<br>394 ± 23<br>318 ± 34<br>780 ± 35<br>516 ± 20<br>318 ± 39<br>318 ± 39<br>318 ± 31<br>318 ± 31 | 126 ± 10<br>127 ± 10<br>108 ± 12<br>108 ± 17<br>137 ± 17<br>286 ± 28<br>302 ± 25<br>303 ± 28<br>303 ± 28<br>304 ± 25<br>304 ± 25<br>304 ± 25<br>308 ± 24<br>423 ± 18<br>318 ± 24<br>423 ± 18<br>318 ± 24<br>423 ± 18<br>318 ± 24<br>423 ± 18<br>318 ± 24<br>423 ± 30<br>319 ± 31<br>310 ± 20<br>310 ± 31<br>310 ± 31<br>310 ± 20<br>310 ± 31<br>310 ± 20<br>310 ± | 126 ± 10<br>126 ± 12<br>108 ± 12<br>108 ± 17<br>137 ± 17<br>286 ± 28<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>423 ± 18<br>308 ± 24<br>423 ± 18<br>318 ± 24<br>423 ± 42<br>423 ± 43<br>364 ± 23<br>364 ± 23<br>364 ± 24<br>370 ± 20<br>370 ± 31<br>370 ± 31<br>370 ± 31<br>370 ± 31<br>370 ± 31<br>370 ± 32<br>370 ± 31<br>370 ± 25<br>370 ± 37<br>370 ± 27<br>444 ± 56<br>370 ± 25<br>370 ± | 126 ± 12<br>127 ± 10<br>108 ± 12<br>108 ± 17<br>108 ± 17<br>294 ± 17<br>286 ± 28<br>304 ± 28<br>304 ± 28<br>305 ± 28<br>423 ± 44<br>423 ± 44<br>423 ± 44<br>423 ± 30<br>435 ± 30<br>435 ± 30<br>435 ± 30<br>442 ± 30<br>309 ± 24<br>457 ± 42<br>309 ± 34<br>457 ± 45<br>309 ± 24<br>457 ± 45<br>309 ± 34<br>309 ± 35<br>309 ± 34<br>309 ± 35<br>309 ± 34<br>309 ± 36<br>309 ± 36<br>300 ± 36<br>300 ± 36<br>300 ± 36<br>300 ± 36<br>300 ± 36<br>300 ± | 28' 22,83" E) 126' + 10 126' + 17 137 + 17 137 + 17 286 + 28 343 + 28 393 + 28 393 + 28 393 + 28 393 + 28 393 + 28 533 + 18 533 + 18 533 + 18 533 + 18 533 + 18 533 + 18 534 + 29 536 + 23 536 + 23 537 + 42 538 + 34 536 + 33 537 + 42 538 + 34 537 + 58 538 + 34 537 + 58 538 + 34 539 + 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24<br>303 ± 24<br>303 ± 33<br>303 ± 34<br>303 ±  | 197 + 10<br>197 + 10<br>198 + 12<br>198 + 12<br>288 22,83° E)<br>294 + 17<br>296 + 28<br>392 + 28<br>393 + 28<br>393 + 28<br>393 + 28<br>393 + 28<br>394 + 28<br>473 + 44<br>780 ± 35<br>516 + 20<br>198 + 23<br>318 + 43<br>318 + 44<br>423 + 44<br>318 + 23<br>319 + 24<br>444 + 58<br>444 + 58<br>467 + 44<br>464 + 58<br>310 + 24<br>464 + 58<br>311 + 32<br>467 + 44<br>464 + 58<br>311 + 32<br>467 + 44<br>464 + 58<br>311 + 32<br>467 + 44<br>464 + 58<br>311 + 32<br>311 + 32<br>311 + 32<br>311 + 32<br>312 + 23<br>313 + 23<br>313 + 23<br>314 + 23<br>317 + 23<br>318 + 23<br>3  | 126 ± 10<br>127 ± 10<br>108 ± 12<br>108 ± 12<br>294 ± 17<br>286 ± 28<br>302 ± 28<br>303 ± 28<br>303 ± 28<br>304 ± 28<br>304 ± 28<br>304 ± 28<br>308 ± 28<br>318 ± 29<br>318 ± 29<br>319 ± 20<br>310 ± 20<br>407 ± 18<br>310 ± 22<br>407 ± 18<br>310 ± 22<br>310 ± 23<br>310 ±  |
| 123.7 ± 4.7                           | 132.7 ± 4.0   | 144 1 144       | 133.3 ± 3.1       | 125.2 ± 5.3     | 130.5 ± 3.3     | 126.9 ± 3.3  | 121.1 ± 3.0  | 132.4 ± 5.1  | 123,5 ± 3,2   |  |  |   |  | 1 88 ×  | 124.1 ± 2.7<br>119.7 ± 2.8<br>133.0 ± 3.6<br>36 16.44" N, 133°   | 100 X 411  | LOO ZANO   | LOO ZANON!   | L 20 X + 10 8 12 -   
   | 2-37854× 684   | 237 378 S 4 X 687   | 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5  | 5.60 3 - 3.08 S + Z 5.08 5  
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   |
| 0.000                                 | 0.136 ± 0.023 |                 |                   | 0.145 ± 0.016   | 0.144 ± 0.016   | 0.164 ± 0.017  |  | ± 0.024  |   | $0.133 \pm 0.013$  |  |   |  | 0.112 ± 0.012<br>0.144 ± 0.018<br>gai Unit (13072103; 33°   | 60   | 0.112 ± 0.012<br>0.144 ± 0.018<br>gai Unit (13072103; 33°<br>0.336 ± 0.020<br>0.325 ± 0.032  | 0.112 ± 0.012<br>0.144 ± 0.018<br>gai Unit (13072103; 33°<br>0.356 ± 0.020<br>0.325 ± 0.032<br>0.402 ± 0.033   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.136 ± 0.020<br>0.356 ± 0.020<br>0.365 ± 0.032<br>0.402 ± 0.033   | a,112 ± a,012<br>0,144 ± 0.018<br>gai Unit (13072103; 33°<br>0,336 ± 0,020<br>0,346 ± 0,033<br>0,402 ± 0,033<br>0,346 ± 0,029<br>0,346 ± 0,029   
   | 0.112 ± 0.012<br>0.144 ± 0.018<br>gai Unit (13072103; 33°<br>0.336 ± 0.032<br>0.402 ± 0.033<br>0.346 ± 0.029<br>2.143 ± 0.103 11<br>0.517 ± 0.054<br>0.660 ± 0.023   | a,112 ± a,012<br>0,144 ± 0.018<br>gai Unit (13072103; 33°<br>0,336 ± a,020<br>0,345 ± 0.033<br>0,462 ± 0.039<br>0,346 ± 0.029<br>1,143 ± 0,103<br>0,567 ± 0,054<br>0,569 ± 0,023  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.144 ± 0.018<br>0.336 ± 0.020<br>0.335 ± 0.032<br>0.436 ± 0.033<br>0.346 ± 0.039<br>2.143 ± 0.103<br>0.557 ± 0.054<br>0.690 ± 0.023<br>0.568 ± 0.023<br>0.155 ± 0.052   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.144 ± 0.018<br>0.336 ± 0.020<br>0.325 ± 0.032<br>0.402 ± 0.033<br>0.405 ± 0.039<br>2.143 ± 0.103<br>0.517 ± 0.054<br>0.609 ± 0.023<br>0.608 ± 0.023<br>0.508 ± 0.023<br>0.508 ± 0.023<br>0.508 ± 0.023<br>0.508 ± 0.023<br>0.508 ± 0.023  
  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.144 ± 0.018<br>0.356 ± 0.020<br>0.325 ± 0.032<br>0.402 ± 0.033<br>0.346 ± 0.029<br>2.134 ± 0.103<br>0.517 ± 0.054<br>0.690 ± 0.023<br>0.560 ± 0.023<br>0.560 ± 0.023<br>0.560 ± 0.023<br>0.560 ± 0.023<br>0.560 ± 0.023<br>0.560 ± 0.054   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.144 ± 0.018<br>0.356 ± 0.020<br>0.325 ± 0.032<br>0.402 ± 0.033<br>0.346 ± 0.029<br>2.134 ± 0.103<br>0.517 ± 0.054<br>0.690 ± 0.023<br>0.598 ± 0.023<br>1.152 ± 0.048<br>0.403 ± 0.047<br>0.403 ± 0.047   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.144 ± 0.018<br>0.356 ± 0.020<br>0.325 ± 0.032<br>0.405 ± 0.033<br>0.346 ± 0.029<br>2.143 ± 0.103<br>0.517 ± 0.054<br>0.690 ± 0.023<br>0.587 ± 0.054<br>0.690 ± 0.023<br>0.155 ± 0.052<br>0.333 ± 0.047<br>0.461 ± 0.041  | 0.112 ± 0.012<br>0.144 ± 0.018<br>gai Unit (13072103; 33°<br>0.336 ± 0.020<br>0.325 ± 0.032<br>0.406 ± 0.033<br>0.346 ± 0.039<br>2.143 ± 0.034<br>0.690 ± 0.033<br>0.517 ± 0.034<br>0.690 ± 0.023<br>1.155 ± 0.042<br>0.403 ± 0.147<br>0.403 ± 0.147<br>0.404 ± 0.041<br>0.667 ± 0.042<br>0.404 ± 0.044   
  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.144 ± 0.018<br>0.356 ± 0.020<br>0.325 ± 0.032<br>0.405 ± 0.033<br>0.346 ± 0.029<br>2.143 ± 0.034<br>0.690 ± 0.033<br>0.517 ± 0.034<br>0.690 ± 0.023<br>0.585 ± 0.026<br>0.593 ± 0.047<br>0.693 ± 0.147<br>0.653 ± 0.048<br>0.664 ± 0.048  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.136 ± 0.020<br>0.335 ± 0.032<br>0.435 ± 0.033<br>0.346 ± 0.033<br>0.346 ± 0.033<br>0.347 ± 0.034<br>0.690 ± 0.023<br>0.588 ± 0.028<br>1.155 ± 0.052<br>0.333 ± 0.047<br>0.461 ± 0.041<br>0.461 ± 0.041<br>0.462 ± 0.026<br>0.463 ± 0.048<br>0.461 ± 0.041<br>0.463 ± 0.048<br>0.461 ± 0.049<br>0.463 ± 0.036<br>0.463 ± 0.036  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.346 ± 0.020<br>0.325 ± 0.032<br>0.402 ± 0.033<br>0.346 ± 0.029<br>2.143 ± 0.103<br>0.557 ± 0.054<br>0.690 ± 0.023<br>0.568 ± 0.028<br>1.155 ± 0.026<br>4.033 ± 0.147<br>0.562 ± 0.048<br>0.461 ± 0.041<br>0.662 ± 0.048<br>0.461 ± 0.049<br>0.462 ± 0.049<br>0.463 ± 0.049<br>0.462 ± 0.049<br>0.463 ± 0.049<br>0.463 ± 0.049<br>0.463 ± 0.049<br>0.463 ± 0.049<br>0.463 ± 0.039<br>0.463 ± 0.039  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.346 ± 0.020<br>0.325 ± 0.020<br>0.402 ± 0.023<br>0.406 ± 0.029<br>2.143 ± 0.103<br>0.517 ± 0.054<br>0.690 ± 0.023<br>0.591 ± 0.026<br>0.401 ± 0.041<br>0.402 ± 0.034<br>0.401 ± 0.044<br>0.401 ± 0.044<br>0.401 ± 0.044<br>0.401 ± 0.034<br>0.401 ± 0.034  
   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.136 ± 0.020<br>0.235 ± 0.020<br>0.402 ± 0.023<br>0.402 ± 0.029<br>2.143 ± 0.103<br>0.517 ± 0.054<br>0.690 ± 0.023<br>0.591 ± 0.026<br>0.401 ± 0.041<br>0.401 ± 0.041<br>0.401 ± 0.044<br>0.401 ± 0.044  | 0.112 ± 0.072<br>0.144 ± 0.018<br>0.336 ± 0.020<br>0.335 ± 0.020<br>0.402 ± 0.033<br>0.402 ± 0.029<br>2.143 ± 0.103<br>0.517 ± 0.054<br>0.699 ± 0.025<br>0.598 ± 0.026<br>1.155 ± 0.025<br>0.335 ± 0.048<br>0.461 ± 0.041<br>0.662 ± 0.039<br>0.443 ± 0.039<br>0.443 ± 0.039<br>0.451 ± 0.039<br>0.451 ± 0.039<br>0.451 ± 0.039<br>0.452 ± 0.039<br>0.452 ± 0.039<br>0.453 ± 0.039<br>0.453 ± 0.039<br>0.453 ± 0.039<br>0.456 ± 0.039   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.346 ± 0.020<br>0.325 ± 0.032<br>0.402 ± 0.033<br>0.346 ± 0.029<br>2.134 ± 0.103<br>1.55 ± 0.025<br>0.509 ± 0.025<br>0.509 ± 0.047<br>0.401 ± 0.047<br>0.401 ± 0.047<br>0.402 ± 0.032<br>0.323 ± 0.048<br>0.403 ± 0.049<br>0.403 ± 0.034<br>0.403 ± 0.039<br>0.403 ± 0.039  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.144 ± 0.018<br>0.356 ± 0.020<br>0.325 ± 0.032<br>0.402 ± 0.033<br>0.346 ± 0.029<br>2.143 ± 0.103<br>0.517 ± 0.054<br>0.690 ± 0.023<br>1.155 ± 0.052<br>0.332 ± 0.062<br>0.433 ± 0.040<br>0.443 ± 0.040<br>0.443 ± 0.034<br>0.443 ± 0.036<br>0.443 ± 0.036   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.136 ± 0.020<br>0.325 ± 0.033<br>0.346 ± 0.023<br>0.346 ± 0.023<br>0.346 ± 0.023<br>0.467 ± 0.033<br>0.568 ± 0.023<br>0.568 ± 0.023<br>0.568 ± 0.023<br>0.568 ± 0.023<br>0.47 ± 0.048<br>0.401 ± 0.048<br>0.401 ± 0.049<br>0.402 ± 0.039<br>0.403 ± 0.039<br>0.404 ± 0.039<br>0.404 ± 0.039<br>0.404 ± 0.039<br>0.405 ± 0.039<br>0.407 ± 0.039<br>0.408 ± 0.048<br>0.408 ± 0.048  
   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.346 ± 0.020<br>0.325 ± 0.033<br>0.346 ± 0.029<br>2.143 ± 0.103<br>0.547 ± 0.028<br>1.155 ± 0.028<br>1.155 ± 0.026<br>4.033 ± 0.147<br>0.662 ± 0.026<br>4.033 ± 0.147<br>0.461 ± 0.041<br>0.462 ± 0.039<br>0.343 ± 0.039<br>0.344 ± 0.039<br>0.356 ± 0.033<br>0.356 ± 0.033<br>0.357 ± 0.033<br>0.358 ± 0.033  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.346 ± 0.020<br>0.325 ± 0.020<br>0.402 ± 0.023<br>0.402 ± 0.029<br>2.143 ± 0.103<br>0.517 ± 0.054<br>0.699 ± 0.025<br>0.598 ± 0.026<br>1.155 ± 0.025<br>0.323 ± 0.026<br>0.323 ± 0.048<br>0.461 ± 0.041<br>0.662 ± 0.029<br>0.461 ± 0.041<br>0.662 ± 0.039<br>0.461 ± 0.041<br>0.662 ± 0.039<br>0.461 ± 0.041<br>0.662 ± 0.039<br>0.473 ± 0.039<br>0.474 ± 0.039<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.577 ± 0.045<br>0.430 ± 0.045<br>0.340 ± 0.045<br>0.340 ± 0.045<br>0.349 ± 0.072   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.346 ± 0.020<br>0.325 ± 0.032<br>0.402 ± 0.033<br>0.346 ± 0.029<br>2.134 ± 0.103<br>0.547 ± 0.054<br>0.569 ± 0.025<br>0.569 ± 0.025<br>0.572 ± 0.054<br>0.561 ± 0.040<br>0.573 ± 0.040<br>0.573 ± 0.040<br>0.574 ± 0.034<br>0.575 ± 0.039<br>0.575 ± 0.039<br>0.576 ± 0.039<br>0.577 ± 0.039<br>0.576 ± 0.039<br>0.577 ± 0.039<br>0.578 ± 0.035<br>0.579 ± 0.072<br>0.599 ± 0.072<br>0.599 ± 0.072   | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.346 ± 0.020<br>0.355 ± 0.033<br>0.346 ± 0.033<br>0.346 ± 0.033<br>0.346 ± 0.033<br>0.347 ± 0.034<br>0.659 ± 0.023<br>0.568 ± 0.028<br>1.155 ± 0.052<br>0.368 ± 0.028<br>1.155 ± 0.026<br>0.343 ± 0.048<br>0.461 ± 0.041<br>0.462 ± 0.039<br>0.463 ± 0.039<br>0.463 ± 0.039<br>0.463 ± 0.039<br>0.463 ± 0.039<br>0.473 ± 0.039<br>0.473 ± 0.039<br>0.473 ± 0.039<br>0.473 ± 0.039<br>0.474 ± 0.039<br>0.310 ± 0.048<br>0.310 ± 0.048<br>0.310 ± 0.048<br>0.310 ± 0.048<br>0.310 ± 0.049<br>0.310 ± 0.039<br>0.359 ± 0.072<br>0.499 ± 0.072<br>0.499 ± 0.073<br>0.399 ± 0.072  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.346 ± 0.020<br>0.325 ± 0.033<br>0.346 ± 0.029<br>0.402 ± 0.033<br>0.402 ± 0.033<br>0.407 ± 0.029<br>1.158 ± 0.026<br>0.509 ± 0.026<br>0.509 ±
0.026<br>0.509 ± 0.026<br>0.401 ± 0.041<br>0.402 ± 0.026<br>0.403 ± 0.044<br>0.403 ± 0.039<br>0.403 ± 0.039<br>0.404 ± 0.039<br>0.403 ± 0.039<br>0.403 ± 0.039<br>0.403 ± 0.039<br>0.404 ± 0.039<br>0.403 ± 0.039<br>0.404 ± 0.033<br>0.549 ± 0.033<br>0.549 ± 0.033<br>0.544 ± 0.033<br>0.544 ± 0.033<br>0.544 ± 0.033<br>0.544 ± 0.033<br>0.544 ± 0.033 | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.136 ± 0.020<br>0.235 ± 0.020<br>0.402 ± 0.023<br>0.402 ± 0.023<br>0.402 ± 0.023<br>0.402 ± 0.023<br>0.403 ± 0.024<br>0.401 ± 0.041<br>0.401 ± 0.041<br>0.401 ± 0.041<br>0.401 ± 0.041<br>0.402 ± 0.034<br>0.403 ± 0.036<br>0.403 ± 0.036<br>0.403 ± 0.036<br>0.404 ± 0.039<br>0.404 ± 0.025<br>0.355 ± 0.039<br>0.404 ± 0.026<br>0.402 ± 0.039<br>0.403 ± 0.039<br>0.404 ± 0.026<br>0.404 ± 0.028<br>0.344 ± 0.028<br>0.344 ± 0.035<br>0.344 ± 0.035  | 0.112 ± 0.072<br>0.144 ± 0.018<br>0.136 ± 0.020<br>0.325 ± 0.020<br>0.325 ± 0.023<br>0.402 ± 0.029<br>2.134 ± 0.103<br>0.517 ± 0.054<br>0.609 ± 0.025<br>0.509 ± 0.025<br>0.517 ± 0.048<br>0.617 ± 0.048<br>0.617 ± 0.048<br>0.617 ± 0.048<br>0.617 ± 0.048<br>0.618 ± 0.020<br>0.619 ± 0.020<br>0.619 ± 0.020<br>0.619 ± 0.020<br>0.610  | 0.112 ± 0.012<br>0.144 ± 0.018<br>0.145 ± 0.018<br>0.355 ± 0.032<br>0.366 ± 0.023<br>0.367 ± 0.033<br>0.368 ± 0.023<br>0.568 ± 0.023<br>0.568 ± 0.023<br>0.568 ± 0.023<br>0.568 ± 0.023<br>0.568 ± 0.026<br>0.517 ± 0.048<br>0.461 ± 0.047<br>0.461 ± 0.047<br>0.462 ± 0.039<br>0.463 ± 0.039<br>0.463 ± 0.039<br>0.463 ± 0.039<br>0.464 ± 0.020<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.576 ± 0.039<br>0.577 ± 0.045<br>0.399 ± 0.020<br>0.599 ± 0.020<br>0.599 ± 0.039<br>0.599 ± 0.039  | 0.112 ± 0.072<br>0.144 ± 0.018<br>0.136 ± 0.020<br>0.402 ± 0.023<br>0.402 ± 0.023<br>0.402 ± 0.023<br>0.402 ± 0.023<br>0.402 ± 0.023<br>0.403 ± 0.103<br>0.407 ± 0.024<br>0.408 ± 0.026<br>4.033 ± 0.026<br>4.033 ± 0.026<br>4.033 ± 0.026<br>0.401 ± 0.041<br>0.402 ± 0.039<br>0.403 ± 0.039<br>0.403 ± 0.039<br>0.403 ± 0.039<br>0.403 ± 0.020<br>0.403 ± 0.020<br>0.404 ± 0.023<br>0.403 ± 0.020<br>0.403 ± 0.020<br>0.403 ± 0.020<br>0.403 ± 0.020<br>0.404 ± 0.023<br>0.404 ± 0.023<br>0.404 ± 0.023<br>0.404 ± 0.023<br>0.504 ± 0.003<br>0.504 ± 0.003<br>0.506 ± 0.003  |
| $0.0194 \pm 0.0007$                   |               | 0.0208 ± 0.0006 | 0.0209 ± 0.0005   | 0.0193 ± 0.0006 | 0.0205 ± 0.0005 | 0.0199 ± 0.0005  | 0.0190 ± 0.0005  | $0.0207 \pm 0.0008$  | 0.0193 ± 0.0005   | $0.0194 \pm 0.0004$  | F0000 + 2870 0   | 0.0000 + 0.0000   | 0.0208 ± 0.0006  | 0.0208 ± 0.0006   | 0.0208 ± 0.0006<br>Sandstone of the Shing  | Sandstone of the Shing<br>0.0377 ± 0.0009<br>0.0377 ± 0.0009   | 0.0208 ± 0.0006 Sandstone of the Shing 0.0377 ± 0.0009 0.0411 ± 0.0012 0.0543 ± 0.0014   | Sandstone of the Shing<br>0.0208 ± 0.0006<br>Sandstone of the Shing<br>0.0377 ± 0.0000<br>0.0543 ± 0.0014<br>0.0433 ± 0.0011   | 0.0208 ± 0.0006<br>0.0208 ± 0.0006<br>0.0377 ± 0.0009<br>0.0411 ± 0.0012<br>0.0433 ± 0.0011<br>0.0433 ± 0.0011   
   | Sandstone of the Shing<br>0.0208 ± 0.0006<br>0.0377 ± 0.0009<br>0.0411 ± 0.0012<br>0.0433 ± 0.0014<br>0.0435 ± 0.0041<br>0.0426 ± 0.0043<br>0.0926 ± 0.0017  | \$\text{Sandstone of the Shing}\$  \$\text{Sandstone of the Shing}\$  \$0.0208 \pi 0.0006  \$0.0377 \pi 0.0007  \$0.0433 \pi 0.0011  \$0.0433 \pi 0.0011  \$0.0455 \pi 0.0014  \$0.0426 \pi 0.0017  \$0.0440 \pi 0.0011   | Sandstone of the Shing<br>0.0208 ± 0.0006<br>0.0208 ± 0.0009<br>0.0431 ± 0.0012<br>0.0543 ± 0.0014<br>0.0435 ± 0.0014<br>0.0426 ± 0.0017<br>0.0820 ± 0.0017<br>0.0420 ± 0.0017<br>0.0420 ± 0.0017  | Sandstone of the Shing<br>0.0208 ± 0.0006<br>0.0208 ± 0.0006<br>0.0441 ± 0.0012<br>0.0543 ± 0.0014<br>0.0543 ± 0.0011<br>0.1965 ± 0.0017<br>0.0820 ± 0.0017<br>0.0820 ± 0.0017<br>0.0420 ± 0.0017<br>0.0440 ± 0.0017<br>0.0440 ± 0.0011   
  | Sandstone of the Shing<br>0.0208 ± 0.0006<br>0.0377 ± 0.0009<br>0.0431 ± 0.0014<br>0.0433 ± 0.0011<br>0.1965 ± 0.0043<br>0.0426 ± 0.0017<br>0.0420 ± 0.0017<br>0.0440 ± 0.0017<br>0.1256 ± 0.0012<br>0.0409 ± 0.0012   | Sandstone of the Shing 0.0208 ± 0.0006 Sandstone of the Shing 0.0377 ± 0.0006 0.0411 ± 0.0012 0.0543 ± 0.0014 0.0455 ± 0.0014 0.0426 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017 0.0420 ± 0.0017  | Sandstone of the Shing 0.0208 ± 0.0006 Sandstone of the Shing 0.0377 ± 0.0009 0.0411 ± 0.0012 0.0543 ± 0.0014 0.1965 ± 0.0014 0.0820 ± 0.0017 0.0440 ± 0.0017 0.0420 ± 0.0012 0.1256 ± 0.0063 0.0125 ± 0.0069 0.0125 ± 0.0069 0.0125 ± 0.0069 0.0128 ± 0.0012 0.02836 ± 0.0015 0.0468 ± 0.0017   | Sandstone of the Shing 0.0208 ± 0.0006 Sandstone of the Shing 0.0377 ± 0.0009 0.0411 ± 0.0012 0.0543 ± 0.0014 0.0452 ± 0.0043 0.0426 ± 0.0017 0.0440 ± 0.0017 0.0440 ± 0.0017 0.0440 ± 0.0016 0.0400 ± 0.0016 0.0400 ± 0.0016 0.0400 ± 0.0016 0.0400 ± 0.0016 0.0400 ± 0.0016 0.0400 ± 0.0016 0.0400 ± 0.0016 0.0400 ± 0.0016 0.0400 ± 0.0016   
  | Sandstone of the Shing 0.0208 ± 0.0006 Sandstone of the Shing 0.0377 ± 0.0009 0.0411 ± 0.0012 0.0543 ± 0.0014 0.0435 ± 0.0014 0.0820 ± 0.0017 0.0440 ± 0.0017 0.0440 ± 0.0017 0.0440 ± 0.0016 0.0455 ± 0.0016 0.0512 ± 0.0016 0.0512 ± 0.0016 0.0545 ± 0.0015 0.0658 ± 0.0015 0.0658 ± 0.0015 0.0658 ± 0.0015 0.0658 ± 0.0015 0.0658 ± 0.0015 0.0658 ± 0.0015  | Sandstone of the Shing<br>0.0208 ± 0.0006<br>0.0373 ± 0.0007<br>0.0411 ± 0.0009<br>0.0411 ± 0.0014<br>0.0433 ± 0.0014<br>0.0435 ± 0.0014<br>0.0426 ± 0.0017<br>0.0440 ± 0.0017<br>0.0440 ± 0.0012<br>0.0409 ± 0.0012<br>0.0409 ± 0.0012<br>0.0409 ± 0.0015<br>0.0432 ± 0.0015<br>0.0432 ± 0.0015<br>0.0432 ± 0.0015<br>0.0432 ± 0.0017<br>0.04410 ± 0.0013   | Sandstone of the Shing<br>0.0208 ± 0.0006<br>0.0208 ± 0.0006<br>0.0341 ± 0.0012<br>0.0543 ± 0.0014<br>0.0435 ± 0.0014<br>0.0435 ± 0.0017<br>0.0440 ± 0.0017<br>0.0440 ± 0.0017<br>0.0400 ± 0.0017<br>0.0400 ± 0.0017<br>0.0400 ± 0.0016<br>0.0400 ± 0.0016<br>0.0400 ± 0.0016<br>0.0432 ± 0.0015<br>0.0432 ± 0.0015<br>0.0432 ± 0.0015<br>0.0432 ± 0.0015<br>0.0432 ± 0.0015<br>0.0410 ± 0.0013<br>0.0410 ± 0.0013   | Sandstone of the Shing<br>0.0208 ± 0.0006<br>0.0208 ± 0.0006<br>0.0411 ± 0.0012<br>0.0543 ± 0.0014<br>0.0435 ± 0.0014<br>0.0435 ± 0.0017<br>0.0440 ± 0.0017<br>0.0400 ± 0.0011<br>0.0526 ± 0.0016<br>0.0512 ± 0.0016<br>0.0512 ± 0.0016<br>0.0400 ± 0.0017<br>0.0400 ± 0.0017<br>0.0400 ± 0.0017<br>0.0400 ± 0.0017<br>0.0400 ± 0.0013<br>0.0410 ± 0.0013<br>0.0410 ± 0.0013<br>0.0410 ± 0.0013<br>0.0410 ± 0.0013  
   | Sandstone of the Shing<br>0.0208 ± 0.0006<br>0.0208 ± 0.0006<br>0.0431 ± 0.0012<br>0.0543 ± 0.0014<br>0.0435 ± 0.0014<br>0.0435 ± 0.0017<br>0.040 ± 0.0016<br>0.0408 ± 0.0016<br>0.0432 ± 0.0016<br>0.0432 ± 0.0016<br>0.0432 ± 0.0016<br>0.0432 ± 0.0016<br>0.0432 ± 0.0017<br>0.0438 ± 0.0017<br>0.0410 ± 0.0013<br>0.0438 ± 0.0017  | Sandstone of the Shing 0.0208 ± 0.0006 Sandstone of the Shing 0.037 ± 0.0006 0.0411 ± 0.0012 0.0543 ± 0.0014 0.0455 ± 0.0014 0.0426 ± 0.0017 0.0426 ± 0.0017 0.0426 ± 0.0017 0.0430 ± 0.0017 0.0432 ± 0.0015 0.0438 ± 0.0017 0.0432 ± 0.0017 0.0432 ± 0.0013 0.0438 ± 0.0010 0.0806 ± 0.0010 0.0806 ± 0.0010 0.0806 ± 0.0017 0.0437 ± 0.0017 0.0437 ± 0.0017  | Sandstone of the Shing 0.0208 ± 0.0006 Sandstone of the Shing 0.037 ± 0.0006 0.0411 ± 0.0012 0.0543 ± 0.0014 0.0455 ± 0.0014 0.0426 ± 0.0017 0.0426 ± 0.0017 0.0426 ± 0.0017 0.0426 ± 0.0017 0.0426 ± 0.0017 0.0426 ± 0.0017 0.0426 ± 0.0017 0.0426 ± 0.0015 0.0428 ± 0.0015 0.0438 ± 0.0015 0.0438 ± 0.0010 0.0438 ± 0.0010 0.0438 ± 0.0010 0.0438 ± 0.0011 0.0438 ± 0.0011 0.0446 ± 0.0013 0.0441 ± 0.0011   | Sandstone of the Shing 0.0228 ± 0.0006 0.0371 ± 0.0009 0.0411 ± 0.0009 0.0411 ± 0.0012 0.0543 ± 0.0014 0.0552 ± 0.0014 0.0450 ± 0.0017 0.0440 ± 0.0017 0.0440 ± 0.0017 0.0450 ± 0.0015 0.0450 ± 0.0015 0.0450 ± 0.0015 0.052 ± 0.0015 0.052 ± 0.0015 0.053 ± 0.0015 0.053 ± 0.0015 0.054 ± 0.0017 0.043 ± 0.0017 0.043 ± 0.0017 0.043 ± 0.0017 0.043 ± 0.0017 0.043 ± 0.0017 0.043 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017 0.056 ± 0.0017  
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Hilo-1-D					Hilg-I-17	Hilg-1-18		Hilg-1-20	Hilg-1-21					5				
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13072103-1<br>13072103-2<br>13072103-3<br>13072103-3<br>13072103-4<br>13072103-7<br>13072103-1<br>13072103-1<br>13072103-1<br>13072103-1<br>13072103-1<br>13072103-1<br>13072103-1<br>13072103-1<br>13072103-1<br>13072103-2<br>13072103-2<br>13072103-2<br>13072103-2<br>13072103-2<br>13072103-2<br>13072103-2<br>13072103-2<br>13072103-2<br>13072103-2<br>13072103-3<br>13072103-3<br>13072103-3<br>13072103-3<br>13072103-3<br>13072103-3<br>13072103-3<br>13072103-3   |

TABLE 1. (Continued)

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| (Ma)                          | 202 ± 04        | 273 ± 40        | 285 ± 64            | 280 ± 95            | MONTH AND AND       | 372 ± 64            | 372 ± 64<br>336 ± 54         | 372 ± 64<br>336 ± 54<br>271 ± 41                         | 372 ± 64<br>336 ± 54<br>271 ± 41<br>293 ± 46                                 |  |   |   |  |  |  |  |   |  |   |   |  |   | 2017<br>2017<br>2017<br>2017<br>2017<br>2017<br>2017<br>2017   |   | 37.25<br>3.36<br>3.36<br>3.36<br>3.36<br>3.36<br>3.37<br>3.31<br>3.31<br>3.31<br>3.31<br>3.31<br>3.31<br>3.31  | 3.20<br>3.30<br>3.30<br>3.30<br>2.70<br>2.70<br>2.70<br>2.70<br>2.70<br>2.70<br>2.70<br>2.7  | 37.26<br>3.36<br>3.36<br>3.36<br>3.36<br>3.36<br>3.36<br>3.36<br>3  
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   |
131 - 1012	2078 ± 03.4	257.7 ± 9.6	273.7 ± 14.6	264.7 ± 21.1		284.7 ± 13.5	284.7 ± 13.5 285.7 ± 12.2	$284.7 \pm 13.5$ $285.7 \pm 12.2$ $271.9 \pm 10.2$	$284.7 \pm 13.5$ $285.7 \pm 12.2$ $271.9 \pm 10.2$ $259.4 \pm 10.5$	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 38.9	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 38.9 248.7 ± 12.9	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 58.9 248.7 ± 12.9 289.9 ± 9.2	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 28.9 248.7 ± 12.9 289.9 ± 9.2 255.9 ± 8.4	2847 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 38.9 248.7 ± 12.9 259.9 ± 8.4 255.9 ± 8.4	2847 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 38.9 248.7 ± 12.9 249.9 ± 9.2 255.9 ± 8.4 257.0 ± 12.0 252.3 ± 11.4	2847 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 38.9 248.7 ± 12.9 255.9 ± 9.2 255.9 ± 8.4 257.0 ± 12.0 252.3 ± 11.4 305.6 ± 17.8	284.7 ± 13.5 283.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 38.9 248.7 ± 12.9 285.9 ± 9.2 255.9 ± 8.4 257.0 ± 11.4 305.6 ± 11.8 264.5 ± 16.1	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.2 1814.7 ± 38.9 248.7 ± 12.9 259.9 ± 8.4 255.9 ± 8.4 255.0 ± 12.0 255.5 ± 11.4 205.6 ± 11.8 205.6 ± 16.1	2847 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.2 259.4 ± 10.2 248.7 ± 12.9 248.7 ± 12.9 255.9 ± 8.4 257.0 ± 12.0 255.3 ± 11.4 254.5 ± 16.1 274.5 ± 16.1 274.5 ± 16.1	2847 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 248.7 ± 12.9 248.7 ± 12.9 248.9 ± 9.2 255.9 ± 8.4 257.0 ± 12.0 252.3 ± 11.4 265.5 ± 11.8 205.5 ± 11.8 205.5 ± 11.8 205.5 ± 11.7 205.5 ± 11.7 205.5 ± 11.7 205.5 ± 11.7 205.5 ± 11.7 205.5 ± 11.7	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.5 1814.7 ± 38.9 248.7 ± 12.9 255.9 ± 9.2 255.9 ± 8.4 257.9 ± 2.0 255.9 ± 8.4 257.6 ± 11.4 305.6 ± 11.8 305.6 ± 11.7 204.5 ± 16.1 274.5 ± 8.0 257.6 ± 11.7 261.0 ± 7.5 261.0 ± 7.5	2847 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.2 1814.7 ± 38.9 289.9 ± 2.2 255.9 ± 8.4 257.0 ± 12.0 257.0 ± 11.4 205.5 ± 16.1 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11.7 261.0 ± 11.7 261.0 ± 11.7 261.0 ± 11.7 289.1 ± 14.3 257.6 ± 11.7 289.1 ± 14.3 257.6 ± 11.7 289.1 ± 14.3 257.6 ± 11.7 289.1 ± 11.7 289.0 ± 9.8 277.2 ± 14.4 264.8 ± 11.2 286.8 ± 11.2 286.8 ± 11.5 286.8 ± 11.5 286.8 ± 11.5 286.8 ± 11.5 287.8 ± 11.2 287.8 ± 11.3 287.8	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.2 259.4 ± 10.2 259.9 ± 8.4 255.9 ± 8.4 255.9 ± 8.4 255.9 ± 8.4 255.5 ± 11.4 205.6 ± 11.7 251.0 ± 11.7 251.0 ± 11.7 251.0 ± 11.7 251.0 ± 11.7 251.0 ± 11.7 252.2 ± 11.7 253.2 ± 11.7 253.2 ± 11.7 253.2 ± 11.7 254.4 ± 11.5 256.0 ± 9.8 270.2 ± 14.4 264.8 ± 11.5 256.0 ± 9.8 270.3 ± 11.2 270.3 ± 11.2 271.3 ± 9.0 265.8 ± 11.5 275.8 ± 8.3 275.8 ± 8.3 275.8 ± 8.3 275.8 ± 8.3 275.8 ± 8.3 275.8 ± 8.3 277.8 ± 8.3	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.2 259.4 ± 10.2 269.9 ± 8.4 257.0 ± 12.0 257.0 ± 12.0 257.0 ± 11.4 205.6 ± 11.4 205.6 ± 11.7 201.6 ± 11.7 200.7 ± 4.6.6 200.7 ± 4.6.	284.7 ± 13.5 285.7 ± 17.2 271.9 ± 10.2 259.4 ± 10.2 259.4 ± 10.2 259.9 ± 8.4 255.9 ± 8.4 255.9 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287.0 ± 11.4 287.5 ± 8.4 287.5 ± 11.4 287.5 ± 11.4 287.5 ± 11.7 287.5 ± 11.7 287.6 ± 11.7 287.6 ± 11.7 287.6 ± 18.7 289.0 ± 13.7 286.0 ± 11.7 287.0 ± 11.5 286.0 ± 11.7 287.0 ± 11.5 286.4 ± 11.5 286.0 ± 11.7 286.0 ± 11.7 287.0 ± 11.5 286.4 ± 11.5 287.8 ± 10.9 287.8 ± 10.9 287.8 ± 10.9 287.8 ± 10.9 287.8 ± 10.9 287.2 ± 10.9 287.2 ± 10.9 287.2 ± 10.9 287.3 ± 10.9 287.	284.7 ± 13.5 285.7 ± 12.2 271.9 ± 10.2 259.4 ± 10.2 289.9 ± 8.4 287.0 ± 12.9 289.9 ± 8.4 257.0 ± 12.0 257.0 ± 11.4 265.5 ± 8.0 277.5 ± 8.0 277.5 ± 11.4 264.5 ± 11.7 277.5 ± 8.0 277.5 ± 18.7 261.6 ± 17.5 261.6 ± 17.5 261.6 ± 11.7 277.5 ± 18.7 289.1 ± 14.4 284.4 ± 11.5 259.0 ± 8.3 259.0 ± 8.3 259.0 ± 8.3 259.0 ± 8.3 250.7 ± 46.6 377.1 ± 9.0 264.8 ± 11.5 256.0 ± 9.8 270.2 ± 11.5 256.0 ± 9.8 270.2 ± 11.5 286.4 ± 11.5 281.0 ± 11.5 281.0 ± 11.5 281.0 ± 11.5 281.0 ± 11.5 281.4 ± 7.0 277.8 ± 10.9 277.8 ± 10.9 277.8 ± 12.5 270.8 ± 12.5	284.7 ± 13.5 285.7 ± 17.2 271.9 ± 10.2 259.4 ± 10.2 259.4 ± 10.2 259.9 ± 2.2 255.9 ± 8.4 255.0 ± 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0,574 ± 0.074	NEU 0 + CIE 0	0.308 ± 0.045	+	$0.317 \pm 0.107$	0.442 . 0.077	Ħ	16 46	# # #	# # # #	H H H H H	444444	* * * * * * * *	0.332 ± 0.064 0.305 ± 0.046 0.305 ± 0.046 4.983 ± 0.196 0.238 ± 0.060 0.238 ± 0.041 0.325 ± 0.043	0.392 ± 0.064 0.305 ± 0.046 0.305 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.238 ± 0.040 0.325 ± 0.041 0.305 ± 0.041	0.392 ± 0.064 0.306 ± 0.064 0.334 ± 0.052 4.983 ± 0.196 0.238 ± 0.060 0.286 ± 0.041 0.325 ± 0.063 0.304 ± 0.062 0.303 ± 0.062	0.392 ± 0.064 0.306 ± 0.064 0.308 ± 0.052 4.983 ± 0.196 0.238 ± 0.060 0.238 ± 0.060 0.304 ± 0.062 0.304 ± 0.062 0.304 ± 0.062 0.426 ± 0.065	0.392 ± 0.064 0.306 ± 0.046 0.306 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.286 ± 0.041 0.325 ± 0.043 0.304 ± 0.062 0.303 ± 0.063 0.426 ± 0.064 0.426 ± 0.064	0.392 ± 0.064 0.306 ± 0.046 0.306 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.238 ± 0.041 0.325 ± 0.041 0.304 ± 0.062 0.304 ± 0.062 0.304 ± 0.062 0.301 ± 0.063 0.301 ± 0.063	0.392 ± 0.064 0.305 ± 0.046 0.305 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.238 ± 0.041 0.325 ± 0.041 0.304 ± 0.062 0.303 ± 0.059 0.426 ± 0.066 0.301 ± 0.083 0.391 ± 0.083 0.391 ± 0.083	0.392 ± 0.064 0.305 ± 0.064 0.305 ± 0.046 0.238 ± 0.196 0.238 ± 0.041 0.328 ± 0.041 0.328 ± 0.041 0.328 ± 0.043 0.301 ± 0.065 0.301 ± 0.056 0.301 ± 0.058 0.301 ± 0.058 0.301 ± 0.058 0.301 ± 0.058 0.301 ± 0.058	0.392 ± 0.064 0.306 ± 0.046 0.306 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.285 ± 0.041 0.325 ± 0.043 0.304 ± 0.062 0.304 ± 0.062 0.405 ± 0.059 0.406 ± 0.053 0.309 ± 0.053 0.309 ± 0.053 0.300 ± 0.063 0.300 ± 0.063 0.300 ± 0.065	0.392 ± 0.064 0.306 ± 0.046 0.306 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.285 ± 0.041 0.304 ± 0.062 0.304 ± 0.062 0.301 ± 0.083 0.304 ± 0.068 0.301 ± 0.083 0.304 ± 0.066 0.301 ± 0.083 0.304 ± 0.066 0.309 ± 0.046 0.309 ± 0.046 0.309 ± 0.028	0.392 ± 0.064 0.306 ± 0.046 0.306 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.238 ± 0.041 0.325 ± 0.041 0.304 ± 0.062 0.304 ± 0.062 0.304 ± 0.063 0.304 ± 0.066 0.301 ± 0.083 0.309 ± 0.038 0.309 ± 0.046 0.300 ± 0.028	0.332 ± 0.064 0.305 ± 0.046 0.305 ± 0.045 4.983 ± 0.196 0.238 ± 0.196 0.238 ± 0.041 0.325 ± 0.043 0.304 ± 0.062 0.303 ± 0.063 0.426 ± 0.065 0.301 ± 0.083 0.309 ± 0.046 0.309 ± 0.046 0.300 ± 0.028 0.300 ± 0.028 0.300 ± 0.028 0.300 ± 0.046 0.300 ± 0.046 0.256 ± 0.046 0.256 ± 0.077 0.077 ± 0.055	0.392 ± 0.064 0.305 ± 0.064 0.305 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.288 ± 0.040 0.288 ± 0.060 0.304 ± 0.059 0.426 ± 0.059 0.426 ± 0.058 0.301 ± 0.038 0.309 ± 0.046 0.301 ± 0.046 0.301 ± 0.046 0.301 ± 0.046 0.256 ± 0.055 0.301 ± 0.055 0.301 ± 0.055 0.301 ± 0.055	0.392 ± 0.064 0.305 ± 0.046 0.305 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.238 ± 0.043 0.304 ± 0.059 0.426 ± 0.059 0.426 ± 0.059 0.436 ± 0.059 0.436 ± 0.059 0.436 ± 0.050 0.301 ± 0.083 0.309 ± 0.046 0.209 ± 0.046 0.209 ± 0.046 0.201 ± 0.071 0.311 ± 0.011 0.417 ± 0.120 0.267 ± 0.055 0.287 ± 0.055 0.287 ± 0.055	0.332 ± 0.064 0.305 ± 0.046 0.305 ± 0.046 0.238 ± 0.049 0.228 ± 0.041 0.238 ± 0.041 0.325 ± 0.043 0.304 ± 0.062 0.303 ± 0.059 0.415 ± 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0.283 ± 0.043 0.284 ± 0.055 0.285 ± 0.033 0.285 ± 0.033	$0.332 \pm 0.064$ $0.305 \pm 0.046$ $0.305 \pm 0.046$ $0.305 \pm 0.036$ $0.238 \pm 0.196$ $0.238 \pm 0.041$ $0.235 \pm 0.041$ $0.325 \pm 0.041$ $0.325 \pm 0.041$ $0.329 \pm 0.062$ $0.301 \pm 0.063$ $0.301 \pm 0.063$ $0.301 \pm 0.063$ $0.301 \pm 0.065$ $0.301 \pm 0.065$ $0.301 \pm 0.065$ $0.302 \pm 0.041$ $0.026 \pm 0.028$ $0.302 \pm 0.046$ $0.201 \pm 0.071$ $0.021 \pm 0.071$ $0.021 \pm 0.021$ $0.021 \pm 0.031$ $0.021 \pm 0.032$ $0.262 \pm 0.032$ $0.262 \pm 0.033$ $0.263 \pm 0.033$	0.392 ± 0.064 0.305 ± 0.046 0.305 ± 0.046 0.334 ± 0.052 4.983 ± 0.196 0.238 ± 0.043 0.304 ± 0.059 0.476 ± 0.062 0.301 ± 0.083 0.299 ± 0.038 0.309 ± 0.046 0.209 ± 0.046 0.209 ± 0.046 0.200 ± 0.052 0.200 ± 0.052 0.200 ± 0.053 0.200 ± 0.053 0.200 ± 0.054 0.200 ± 0.074 0.201 ± 0.071 0.201 ± 0.071 0.202 ± 0.034 0.202 ± 0.034 0.203 ± 0.034 0.203 ± 0.034 0.203 ± 0.034 0.204 ± 0.054 0.206 ± 0.034 0.206 ± 0.034 0.207 ± 0.034 0.308 ± 0.044 0.208 ± 0.044 0.208 ± 0.034 0.308 ± 0.044 0.208 ± 0.034 0.308 ± 0.034	0.392 ± 0.064 0.305 ± 0.046 0.305 ± 0.046 0.238 ± 0.040 0.238 ± 0.041 0.335 ± 0.043 0.304 ± 0.052 0.476 ± 0.053 0.476 ± 0.053 0.476 ± 0.053 0.476 ± 0.053 0.476 ± 0.054 0.301 ± 0.053 0.309 ± 0.046 0.256 ± 0.071 0.301 ± 0.071 0.301 ± 0.054 0.302 ± 0.046 0.256 ± 0.052 0.256 ± 0.053 0.256 ± 0.054 0.256 ± 0.054 0.256 ± 0.054 0.256 ± 0.054 0.258 ± 0.054 0.268 ± 0.054 0.268 ± 0.034 0.268 ± 0.054	0.392 ± 0.064 0.305 ± 0.046 0.305 ± 0.045 4.983 ± 0.196 0.285 ± 0.041 0.325 ± 0.043 0.304 ± 0.062 0.303 ± 0.063 0.304 ± 0.062 0.304 ± 0.063 0.304 ± 0.063 0.301 ± 0.013 0.299 ± 0.038 0.301 ± 0.071 0.201 ± 0.027 0.202 ± 0.025 0.203 ± 0.046 0.265 ± 0.027 0.204 ± 0.025 0.265 ± 0.034 0.267 ± 0.034 0.268 ± 0.034 0.268 ± 0.034 0.298 ± 0.034	0.392 ± 0.064 0.306 ± 0.046 0.306 ± 0.045 4.983 ± 0.196 0.238 ± 0.041 0.325 ± 0.043 0.304 ± 0.062 0.304 ± 0.065 0.301 ± 0.083 0.304 ± 0.065 0.301 ± 0.028 0.309 ± 0.038 0.309 ± 0.028 0.309 ± 0.028 0.309 ± 0.038 0.301 ± 0.071 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0.0473 ± 0.0015	0000 - 0000	0.0408 ± 0.0013	$0.0434 \pm 0.0023$	$0.0419 \pm 0.0033$	$0.0452 \pm 0.0021$	0.00452 + 0.0010	0.0423 = 0.0013	0.0431 ± 0.0016	0.0431 ± 0.0016 0.0411 ± 0.0017	$0.0431 \pm 0.0016$ $0.0431 \pm 0.0016$ $0.0411 \pm 0.0017$ $0.3251 \pm 0.0070$	$0.0431 \pm 0.0016$ $0.0431 \pm 0.0016$ $0.0411 \pm 0.0017$ $0.3251 \pm 0.0070$ $0.0393 \pm 0.0020$	$\begin{array}{c} 0.0453 \pm 0.0013 \\ 0.0431 \pm 0.0015 \\ 0.0411 \pm 0.0017 \\ 0.3251 \pm 0.0070 \\ 0.0393 \pm 0.0020 \\ 0.0460 \pm 0.0015 \end{array}$	$\begin{array}{c} 0.0431 \pm 0.0016 \\ 0.0431 \pm 0.0016 \\ 0.0411 \pm 0.00070 \\ 0.03251 \pm 0.0070 \\ 0.0393 \pm 0.0020 \\ 0.0460 \pm 0.0013 \\ 0.0405 \pm 0.0013 \end{array}$	$0.0431 \pm 0.0015$ $0.0411 \pm 0.0016$ $0.0411 \pm 0.0010$ $0.0351 \pm 0.0020$ $0.0460 \pm 0.0015$ $0.0405 \pm 0.0013$	H 44 44 45 46 46 46 46 46	$0.0431 \pm 0.0016$ $0.0411 \pm 0.0016$ $0.0411 \pm 0.0017$ $0.3251 \pm 0.0070$ $0.0492 \pm 0.0015$ $0.0407 \pm 0.0019$ $0.0497 \pm 0.0019$ $0.0486 \pm 0.0019$	14 4 4 4 4 4 4 4 4 4 4 4	1 4 4 4 4 4 4 4 4 4 4 4 4 4		1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4																											
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| in 100                        | h               | 264.1 ± 10.2    | . 99                | 802.1 ± 28.9        |                     | -11                 |                              | $408.3 \pm 19.5$   |  | 4  | # #   |   | 4 4 4 4  |  |  |  |   |  |   |   |  |   |  | 254.6 ± 9.8<br>263.4 ± 11.9<br>253.7 ± 11.0.7<br>277.0 ± 13.5<br>995.1 ± 38.2<br>537.8 ± 20.8<br>255.1 ± 10.1<br>255.1 ± 10.1<br>257.3 ± 7.6<br>925.1 ± 27.7<br>292.6 ± 13.2<br>291.2 ± 9.6<br>266.9 ± 8.5<br>269.9 ± 8.6   | **************************************   |  | * * * * * * * * * * * * * * * * * * *   
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AND ADDRESS OF TAXABLE PARTY.	1.653 ± 0.034	0.315 ± 0.029	0.322 ± 0.027	1,212 ± 0.075	$3.155 \pm 0.139$	0,330 ± 0.030	$0.472 \pm 0.068$	$0.465 \pm 0.070$	0.294 ± 0.021	Diezy - Diller	0.304 ± 0.039	$0.304 \pm 0.039$ $0.317 \pm 0.034$	$0.304 \pm 0.039$ $0.317 \pm 0.034$ $0.385 \pm 0.056$	0.304 ± 0.039 0.317 ± 0.034 0.385 ± 0.056 1.639 ± 0.112	0.304 ± 0.031 0.317 ± 0.034 0.317 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.052	0.334 ± 0.035 0.314 ± 0.034 0.317 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.052 0.302 ± 0.022	0.304 ± 0.039 0.317 ± 0.039 0.317 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.302 ± 0.022 0.408 ± 0.034	0.239 ± 0.039 0.317 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.052 0.302 ± 0.022 0.408 ± 0.034 0.298 ± 0.038	0.304 ± 0.039 0.317 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.022 0.302 ± 0.022 0.408 ± 0.018 1.601 ± 0.094	0.304 ± 0.039 0.317 ± 0.034 0.387 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.022 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060	0.304 ± 0.039 0.317 ± 0.039 0.317 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.302 ± 0.022 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.032	0.375 ± 0.039 0.317 ± 0.039 0.317 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.302 ± 0.022 0.408 ± 0.032 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.032	0.237 ± 0.039 0.317 ± 0.034 0.318 ± 0.036 1.639 ± 0.112 0.706 ± 0.022 0.302 ± 0.022 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.032 0.313 ± 0.022 0.313 ± 0.023	0.239 ± 0.039 0.317 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.022 0.302 ± 0.022 0.408 ± 0.034 0.408 ± 0.034 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.032 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.325 ± 0.033	0.304 ± 0.039 0.317 ± 0.034 0.387 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.032 0.313 ± 0.025 0.325 ± 0.033 0.299 ± 0.025	0.0407 ± 0.0019 0.304 ± 0.039 263.4 0.0401 ± 0.0017 0.304 ± 0.039 263.4 0.0401 ± 0.0017 0.304 ± 0.039 263.7 0.0439 ± 0.0021 0.304 ± 0.039 0.0402 0.0669 ± 0.0064 1.639 ± 0.1659 ± 0.1669 ± 0.0064 1.639 ± 0.162 263.1 0.0407 ± 0.0016 0.302 ± 0.032 ± 0.032 ± 0.032 ± 0.0407 ± 0.0014 0.308 ± 0.018 257.3 0.0464 ± 0.0012 0.388 ± 0.060 292.6 0.0462 ± 0.0015 0.368 ± 0.060 292.6 0.0462 ± 0.0015 0.313 ± 0.032 266.9 0.0453 ± 0.0015 0.313 ± 0.032 266.9 0.0427 ± 0.0014 0.323 ± 0.033 285.8 0.0427 ± 0.0014 0.325 ± 0.033 285.8 0.0427 ± 0.0014 0.369 ± 0.025 266.9 0.0427 ± 0.0014 0.369 ± 0.025 269.9 ± 0.0464 ± 0.0030 0.369 ± 0.055 269.9 ± 0.0464 ± 0.0030 0.369 ± 0.055 269.9 ± 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.33 37.8 0.0464 ± 0.0030 0.369 ± 0.055 20.34	0.304 ± 0.039 0.317 ± 0.034 0.385 ± 0.056 1.639 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0.025 0.315 ± 0.025 0.315 ± 0.025 0.316 ± 0.095 0.316 ± 0.095 0.316 ± 0.095 0.375 ± 0.033 0.375 ± 0.033 0.375 ± 0.033 0.378 ± 0.033 0.378 ± 0.033	0.375 ± 0.039 0.317 ± 0.034 0.387 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.032 0.313 ± 0.025 0.325 ± 0.033 0.325 ± 0.033 0.335 ± 0.095 0.316 ± 0.052 0.318 ± 0.095 0.318 ± 0.095	0.375 ± 0.039 0.317 ± 0.039 0.317 ± 0.034 0.388 ± 0.056 1.639 ± 0.112 0.706 ± 0.022 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.034 0.361 ± 0.032 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.314 ± 0.033 0.299 ± 0.095 0.315 ± 0.033 0.348 ± 0.095 0.316 ± 0.032 0.318 ± 0.025 0.318 ± 0.025 0.318 ± 0.025 0.318 ± 0.025 0.318 ± 0.032 0.348 ± 0.095 0.318 ± 0.032 0.348 ± 0.099 0.348 ± 0.099 0.348 ± 0.099 0.348 ± 0.099 0.348 ± 0.099 0.292 ± 0.039 0.292 ± 0.039 0.293 ± 0.039	0.375 ± 0.039 0.317 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.018 1.601 ± 0.094 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.052 0.313 ± 0.025 0.313 ± 0.025 0.315 ± 0.032 0.316 ± 0.032 0.317 ± 0.033 0.318 ± 0.032 0.318 ± 0.032 0.328 ± 0.032 0.328 ± 0.032 0.328 ± 0.032 0.328 ± 0.032 0.328 ± 0.033 0.328 ± 0.033 0.328 ± 0.033	0.375 ± 0.039 0.377 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.052 0.302 ± 0.032 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.052 0.313 ± 0.025 0.325 ± 0.033 0.299 ± 0.025 0.316 ± 0.095 0.329 ± 0.095 0.316 ± 0.095 0.318 ± 0.095 0.318 ± 0.093 0.318 ± 0.093 0.329 ± 0.030 0.329 ± 0.030	0.375 ± 0.039 0.377 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.052 0.302 ± 0.022 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.361 ± 0.094 0.361 ± 0.054 0.313 ± 0.025 0.313 ± 0.025 0.315 ± 0.033 0.299 ± 0.025 0.316 ± 0.095 0.318 ± 0.095 0.318 ± 0.095 0.318 ± 0.092 0.318 ± 0.092 0.318 ± 0.092 0.318 ± 0.092 0.328 ± 0.033 0.228 ± 0.039 0.228 ± 0.050 0.329 ± 0.039	0.375 ± 0.039 0.317 ± 0.034 0.387 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.032 0.313 ± 0.025 0.313 ± 0.025 0.325 ± 0.033 0.348 ± 0.095 0.315 ± 0.095 0.316 ± 0.095 0.316 ± 0.095 0.316 ± 0.095 0.318 ± 0.094 0.292 ± 0.093 0.348 ± 0.094 0.292 ± 0.039 0.283 ± 0.039 0.283 ± 0.041 0.283 ± 0.041 0.288 ± 0.041	0.375 ± 0.039 0.317 ± 0.034 0.388 ± 0.056 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.361 ± 0.032 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.315 ± 0.033 0.348 ± 0.049 0.348 ± 0.049 0.292 ± 0.039 0.275 ± 0.039 0.275 ± 0.039 0.275 ± 0.039 0.283 ± 0.041 0.283 ± 0.041 0.283 ± 0.041 0.283 ± 0.041 0.283 ± 0.041 0.288 ± 0.043 0.288 ± 0.041	0.375 ± 0.039 0.317 ± 0.034 0.388 ± 0.056 1.639 ± 0.112 0.706 ± 0.022 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.034 0.361 ± 0.032 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.314 ± 0.033 0.348 ± 0.094 0.348 ± 0.039 0.348 ± 0.039 0.348 ± 0.039 0.348 ± 0.039 0.325 ± 0.039 0.348 ± 0.041 0.288 ± 0.044 0.388 ± 0.044 0.288 ± 0.048 0.331 ± 0.049 0.331 ± 0.049	0.374 ± 0.039 0.377 ± 0.034 0.387 ± 0.036 1.639 ± 0.112 0.706 ± 0.022 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.094 0.368 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.314 ± 0.032 0.348 ± 0.082 0.348 ± 0.082 0.292 ± 0.039 0.292 ± 0.039 0.293 ± 0.039 0.293 ± 0.041 0.293 ± 0.048 0.314 ± 0.048 0.318 ± 0.041 0.298 ± 0.048 0.319 ± 0.048 0.319 ± 0.049 0.298 ± 0.048 0.319 ± 0.049 0.298 ± 0.048 0.319 ± 0.049 0.298 ± 0.048 0.319 ± 0.049 0.318 ± 0.049 0.318 ± 0.049 0.318 ± 0.049 0.318 ± 0.049 0.318 ± 0.049 0.318 ± 0.049	0.235 ± 0.039 0.317 ± 0.034 0.385 ± 0.056 1.639 ± 0.112 0.706 ± 0.022 0.408 ± 0.034 0.298 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.094 0.363 ± 0.025 0.313 ± 0.025 0.325 ± 0.033 0.325 ± 0.033 0.346 ± 0.095 0.316 ± 0.095 0.316 ± 0.095 0.316 ± 0.095 0.316 ± 0.092 0.316 ± 0.092 0.318 ± 0.094 0.292 ± 0.039 0.293 ± 0.020 0.293 ± 0.043 0.293 ± 0.043 0.398 ± 0.043 0.398 ± 0.043 0.398 ± 0.043	0.237 ± 0.039 0.317 ± 0.034 0.368 ± 0.056 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.034 0.238 ± 0.004 0.361 ± 0.094 0.361 ± 0.032 0.313 ± 0.025 0.315 ± 0.025 0.325 ± 0.033 0.325 ± 0.033 0.335 ± 0.095 0.315 ± 0.095 0.315 ± 0.095 0.275 ± 0.033 0.275 ± 0.033 0.278 ± 0.041 0.292 ± 0.041 0.293 ± 0.041 0.293 ± 0.041 0.293 ± 0.041 0.293 ± 0.043 0.293 ± 0.041 0.293 ± 0.043 0.293 ± 0.043 0.293 ± 0.043 0.293 ± 0.044 0.292 ± 0.043 0.293 ± 0.044 0.293 ± 0.044 0.293 ± 0.044 0.293 ± 0.043 0.293 ± 0.043 0.293 ± 0.044 0.293 ± 0.043 0.293 ± 0.043	0.237 ± 0.039 0.317 ± 0.034 0.368 ± 0.056 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.034 0.238 ± 0.004 1.601 ± 0.094 0.361 ± 0.032 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.033 0.295 ± 0.039 0.295 ± 0.039 0.295 ± 0.039 0.295 ± 0.041 0.288 ± 0.041 0.288 ± 0.048 0.381 ± 0.049 0.382 ± 0.048 0.382 ± 0.048 0.383 ± 0.048 0.384 ± 0.023 0.385 ± 0.048 0.385 ± 0.048 0.382 ± 0.067 0.382 ± 0.067	0.374 ± 0.039 0.377 ± 0.034 0.388 ± 0.056 1.639 ± 0.112 0.706 ± 0.022 0.408 ± 0.034 0.208 ± 0.018 1.601 ± 0.094 0.368 ± 0.035 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.314 ± 0.049 0.369 ± 0.095 0.315 ± 0.039 0.316 ± 0.094 0.327 ± 0.039 0.338 ± 0.041 0.328 ± 0.041 0.329 ± 0.041 0.329 ± 0.041 0.321 ± 0.040 0.323 ± 0.041 0.328 ± 0.041 0.328 ± 0.041 0.328 ± 0.041 0.329 ± 0.043 0.331 ± 0.040 0.322 ± 0.043 0.331 ± 0.040 0.322 ± 0.043 0.331 ± 0.040 0.322 ± 0.043 0.331 ± 0.040 0.322 ± 0.043 0.332 ± 0.043	0.374 ± 0.039 0.377 ± 0.039 0.377 ± 0.039 0.376 ± 0.035 0.408 ± 0.018 0.298 ± 0.018 0.298 ± 0.018 0.298 ± 0.004 0.361 ± 0.094 0.361 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.314 ± 0.025 0.315 ± 0.033 0.348 ± 0.041 0.292 ± 0.039 0.293 ± 0.041 0.298 ± 0.048 0.338 ± 0.049 0.338 ± 0.048 0.338 ± 0.049 0.332 ± 0.064 0.325 ± 0.067 0.325 ± 0.064	0.375 ± 0.039 0.377 ± 0.034 0.387 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.034 0.208 ± 0.018 1.601 ± 0.094 0.361 ± 0.032 0.361 ± 0.032 0.371 ± 0.025 0.381 ± 0.033 0.382 ± 0.095 0.383 ± 0.095 0.383 ± 0.099 0.293 ± 0.099 0.293 ± 0.099 0.293 ± 0.099 0.293 ± 0.041 0.293 ± 0.041 0.293 ± 0.043 0.338 ± 0.044 0.295 ± 0.049 0.338 ± 0.049 0.398 ± 0.066 0.322 ± 0.066 0.322 ± 0.066 0.322 ± 0.066 0.332 ± 0.066 0.332 ± 0.066 0.332 ± 0.066	0.379 ± 0.039 0.377 ± 0.034 0.387 ± 0.036 1.639 ± 0.112 0.706 ± 0.052 0.408 ± 0.034 0.238 ± 0.004 0.361 ± 0.094 0.361 ± 0.032 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.315 ± 0.033 0.348 ± 0.049 0.295 ± 0.039 0.295 ± 0.039 0.295 ± 0.041 0.288 ± 0.041 0.288 ± 0.041 0.288 ± 0.043 0.329 ± 0.041 0.288 ± 0.043 0.329 ± 0.043 0.329 ± 0.043 0.331 ± 0.050 0.329 ± 0.041 0.285 ± 0.043 0.385 ± 0.043 0.385 ± 0.043 0.385 ± 0.044 0.385 ± 0.048 0.385 ± 0.048 0.385 ± 0.048 0.385 ± 0.048 0.385 ± 0.048 0.385 ± 0.048 0.385 ± 0.067 0.395 ± 0.067 0.395 ± 0.067 0.395 ± 0.067	0.375 ± 0.039 0.377 ± 0.034 0.388 ± 0.056 1.639 ± 0.112 0.706 ± 0.022 0.408 ± 0.034 0.208 ± 0.018 1.601 ± 0.034 0.361 ± 0.032 0.361 ± 0.032 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.315 ± 0.033 0.348 ± 0.049 0.348 ± 0.049 0.348 ± 0.049 0.325 ± 0.039 0.348 ± 0.041 0.285 ± 0.048 0.383 ± 0.041 0.288 ± 0.044 0.329 ± 0.044 0.329 ± 0.048 0.331 ± 0.049 0.331 ± 0.049 0.331 ± 0.049 0.332 ± 0.048 0.332 ± 0.048 0.332 ± 0.048 0.332 ± 0.048 0.332 ± 0.067 0.295 ± 0.048 0.332 ± 0.067 0.295 ± 0.048 0.332 ± 0.067 0.295 ± 0.067 0.292 ± 0.067 0.393 ± 0.067 0.393 ± 0.067 0.393 ± 0.067 0.394 ± 0.063	0.374 ± 0.039 0.377 ± 0.034 0.387 ± 0.035 1.639 ± 0.112 0.706 ± 0.022 0.408 ± 0.034 0.208 ± 0.018 1.601 ± 0.094 0.368 ± 0.060 0.361 ± 0.035 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.313 ± 0.025 0.314 ± 0.049 0.292 ± 0.039 0.292 ± 0.039 0.293 ± 0.041 0.292 ± 0.043 0.384 ± 0.040 0.323 ± 0.041 0.288 ± 0.064 0.329 ± 0.064 0.329 ± 0.064 0.329 ± 0.064 0.329 ± 0.064 0.329 ± 0.066 0.320 ± 0.066
DAMIT + DAMIT	0.0417 ± 0.0017	0.0418 ± 0.0016	0.0396 ± 0.0015	$0.1325 \pm 0.0048$	$0.2466 \pm 0.0087$	$0.0430 \pm 0.0017$	$0.0442 \pm 0.0022$	$0.0654 \pm 0.0031$	$0.0403 \pm 0.0015$	Diport - Diport	$0.0417 \pm 0.0019$	$0.0417 \pm 0.0019$ $0.0401 \pm 0.0017$	$0.0417 \pm 0.0019$ $0.0401 \pm 0.0017$ $0.0439 \pm 0.0021$	$0.0417 \pm 0.0019$ $0.0401 \pm 0.0017$ $0.0439 \pm 0.0021$ $0.1669 \pm 0.0064$	$0.0417 \pm 0.0019$ $0.0401 \pm 0.0017$ $0.0439 \pm 0.0021$ $0.1669 \pm 0.0064$ $0.0870 \pm 0.0034$	$0.0417 \pm 0.0019$ $0.0401 \pm 0.0017$ $0.0439 \pm 0.0021$ $0.1669 \pm 0.0064$ $0.0870 \pm 0.0034$ $0.0417 \pm 0.0016$	$0.0417 \pm 0.0019$ $0.0401 \pm 0.0017$ $0.0439 \pm 0.0021$ $0.1669 \pm 0.0064$ $0.0870 \pm 0.0034$ $0.0417 \pm 0.0016$	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0879 ± 0.0064 0.0817 ± 0.0016 0.0407 ± 0.0014	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0064 0.0417 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0012	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0870 ± 0.0054 0.0417 ± 0.0016 0.0407 ± 0.0012 0.1543 ± 0.0046 0.0464 ± 0.0012	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.1669 ± 0.0064 0.0870 ± 0.0016 0.0407 ± 0.0012 0.0407 ± 0.0012 0.1543 ± 0.0046 0.0464 ± 0.0021 0.0462 ± 0.0015	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0870 ± 0.0034 0.0417 ± 0.0016 0.0407 ± 0.0012 0.0407 ± 0.0012 0.0464 ± 0.0021 0.0462 ± 0.0015	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0012 0.1543 ± 0.0015 0.0462 ± 0.0015 0.0423 ± 0.0015 0.0453 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0012 0.1543 ± 0.0015 0.0462 ± 0.0015 0.0453 ± 0.0016 0.0453 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0054 0.0417 ± 0.0016 0.0407 ± 0.0012 0.1543 ± 0.0012 0.1543 ± 0.0015 0.0453 ± 0.0015 0.0453 ± 0.0015 0.0453 ± 0.0016 0.0453 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.1669 ± 0.0064 0.0417 ± 0.0016 0.0407 ± 0.0012 0.1543 ± 0.0046 0.0467 ± 0.0015 0.0453 ± 0.0015 0.0453 ± 0.0015 0.0453 ± 0.0016 0.0453 ± 0.0016 0.0453 ± 0.0016 0.0453 ± 0.0016 0.0453 ± 0.0016 0.0453 ± 0.0016 0.0453 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0870 ± 0.0064 0.0477 ± 0.0016 0.0407 ± 0.0012 0.1543 ± 0.0046 0.0465 ± 0.0015 0.0465 ± 0.0015 0.0465 ± 0.0015 0.0465 ± 0.0016 0.0467 ± 0.0016 0.0465 ± 0.0016 0.0467 ± 0.0016 0.0467 ± 0.0016 0.0467 ± 0.0016 0.0467 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0839 ± 0.0024 0.0817 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0012 0.0462 ± 0.0015 0.0462 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0016 0.0424 ± 0.0015 0.0424 ± 0.0015 0.0424 ± 0.0016 0.0427 ± 0.0014	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0879 ± 0.0054 0.0817 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0012 0.1543 ± 0.0015 0.0422 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0427 ± 0.0016 0.0421 ± 0.0016 0.0421 ± 0.0016 0.0421 ± 0.0016 0.0427 ± 0.0019	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0012 0.0464 ± 0.0012 0.0462 ± 0.0015 0.0462 ± 0.0013 0.0453 ± 0.0016 0.0453 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0012 0.1543 ± 0.0012 0.1543 ± 0.0015 0.0462 ± 0.0015 0.0462 ± 0.0015 0.0423 ± 0.0013 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0019 0.0433 ± 0.0019 0.0433 ± 0.0019 0.0413 ± 0.0026 0.0330 ± 0.0026 0.0330 ± 0.0026	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0012 0.1543 ± 0.0046 0.0407 ± 0.0012 0.1543 ± 0.0015 0.0453 ± 0.0015 0.0453 ± 0.0016 0.0473 ± 0.0019 0.0473 ± 0.0016 0.0378 ± 0.0016 0.0378 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0839 ± 0.0034 0.0817 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0012 0.0462 ± 0.0015 0.0462 ± 0.0015 0.0463 ± 0.0015 0.0423 ± 0.0016 0.0423 ± 0.0019 0.0428 ± 0.0019 0.0428 ± 0.0019 0.0428 ± 0.0015 0.0428 ± 0.0015 0.0433 ± 0.0015 0.0308 ± 0.0015 0.0378 ± 0.0015 0.0378 ± 0.0015 0.0378 ± 0.0015	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0839 ± 0.0021 0.0817 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0012 0.1543 ± 0.0015 0.0453 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0016 0.0427 ± 0.0019 0.0428 ± 0.0016 0.0428 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0338 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0879 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0015 0.0408 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0013 0.0423 ± 0.0016 0.0427 ± 0.0016 0.0428 ± 0.0016 0.0428 ± 0.0016 0.0428 ± 0.0016 0.0428 ± 0.0016 0.0438 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0016 0.0417 ± 0.0016 0.0407 ± 0.0015 0.0462 ± 0.0015 0.0462 ± 0.0015 0.0463 ± 0.0013 0.0423 ± 0.0013 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0433 ± 0.0016 0.0413 ± 0.0019 0.0433 ± 0.0016 0.0433 ± 0.0016 0.0337 ± 0.0016 0.0337 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0339 ± 0.0016 0.0339 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0016 0.0417 ± 0.0016 0.0407 ± 0.0015 0.0462 ± 0.0015 0.0463 ± 0.0015 0.0463 ± 0.0013 0.0423 ± 0.0013 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0433 ± 0.0016 0.0413 ± 0.0019 0.0435 ± 0.0016 0.0435 ± 0.0016 0.0435 ± 0.0016 0.0338 ± 0.0016 0.0435 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0017 0.0398 ± 0.0017	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0879 ± 0.0021 0.0817 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0015 0.0462 ± 0.0015 0.0463 ± 0.0015 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0019 0.0428 ± 0.0019 0.0428 ± 0.0019 0.0438 ± 0.0016 0.0438 ± 0.0016	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0817 ± 0.0016 0.0417 ± 0.0016 0.0407 ± 0.0012 0.0407 ± 0.0015 0.0462 ± 0.0015 0.0463 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0016 0.0427 ± 0.0019 0.0427 ± 0.0019 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± 0.0017 0.0494 ± 0.0017 0.0416 ± 0.0017	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0016 0.0417 ± 0.0016 0.0407 ± 0.0012 0.1543 ± 0.0012 0.0463 ± 0.0013 0.0463 ± 0.0013 0.0423 ± 0.0013 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0433 ± 0.0016 0.0434 ± 0.0016 0.0438 ± 0.0016 0.0339 ± 0.0016 0.0339 ± 0.0016 0.0338 ± 0.0016 0.0338 ± 0.0016 0.0348 ± 0.0016 0.0348 ± 0.0016 0.0348 ± 0.0016 0.0348 ± 0.0017 0.0445 ± 0.0016 0.0348 ± 0.0017 0.0445 ± 0.0016 0.0349 ± 0.0017 0.0494 ± 0.0013 0.0426 ± 0.0017	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0016 0.0407 ± 0.0015 0.0462 ± 0.0015 0.0463 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0427 ± 0.0019 0.0428 ± 0.0016 0.0428 ± 0.0016 0.0439 ± 0.0016 0.0330 ± 0.0017 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0445 ± 0.0011 0.04416 ± 0.0021 0.04416 ± 0.0021 0.04416 ± 0.0021	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0014 0.0407 ± 0.0015 0.0403 ± 0.0015 0.0403 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0433 ± 0.0016 0.0433 ± 0.0016 0.0433 ± 0.0016 0.0433 ± 0.0016 0.0434 ± 0.0016 0.0435 ± 0.0016 0.0435 ± 0.0016 0.0436 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0436 ± 0.0017 0.0436 ± 0.0017 0.0426 ± 0.0021 0.0412 ± 0.0021 0.0412 ± 0.0021 0.0426 ± 0.0021 0.0426 ± 0.0021 0.0426 ± 0.0021 0.0426 ± 0.0021	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0015 0.0407 ± 0.0015 0.0453 ± 0.0015 0.0423 ± 0.0013 0.0423 ± 0.0013 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0433 ± 0.0015 0.0339 ± 0.0015 0.0339 ± 0.0016 0.0339 ± 0.0016 0.0345 ± 0.0016 0.0445 ± 0.0016 0.0445 ± 0.0017 0.0446 ± 0.0017 0.0446 ± 0.0011 0.0446 ± 0.0011	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0014 0.0417 ± 0.0016 0.0407 ± 0.0015 0.0462 ± 0.0015 0.0463 ± 0.0015 0.0453 ± 0.0015 0.0453 ± 0.0016 0.0473 ± 0.0016 0.0473 ± 0.0016 0.0473 ± 0.0016 0.0473 ± 0.0016 0.0473 ± 0.0016 0.0473 ± 0.0016 0.0378 ± 0.0017 0.0454 ± 0.0017 0.0445 ± 0.0017 0.0446 ± 0.0011 0.0446 ± 0.0011	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0879 ± 0.0021 0.0817 ± 0.0016 0.0407 ± 0.0015 0.0407 ± 0.0015 0.0453 ± 0.0015 0.0453 ± 0.0016 0.0427 ± 0.0016 0.0427 ± 0.0019 0.0428 ± 0.0019 0.0428 ± 0.0019 0.0439 ± 0.0015 0.0439 ± 0.0015 0.0439 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0016 0.0438 ± 0.0017 0.0445 ± 0.0017 0.0445 ± 0.0011 0.0446 ± 0.0021 0.0446 ± 0.0021 0.0440 ± 0.0017	0.0417 ± 0.0019 0.0401 ± 0.0017 0.0439 ± 0.0021 0.0439 ± 0.0021 0.0417 ± 0.0016 0.0407 ± 0.0015 0.0407 ± 0.0015 0.0403 ± 0.0015 0.0453 ± 0.0015 0.0423 ± 0.0015 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0423 ± 0.0016 0.0433 ± 0.0016 0.0339 ± 0.0016 0.0339 ± 0.0016 0.0438 ± 0.0017 0.0445 ± 0.0016 0.0445 ± 0.0017 0.0445 ± 0.0016 0.0438 ± 0.0017 0.0445 ± 0.0016 0.0438 ± 0.0017 0.0445 ± 0.0011 0.0445 ± 0.0011 0.0445 ± 0.0011 0.0446 ± 0.0021 0.0430 ± 0.0011 0.0440 ± 0.0021 0.0440 ± 0.0017
79 20102021	30/2103-8/	13072103-89	13072103-90	13072103-91	13072103-92	13072103-93	13072103-94	13072103-95	13072103-96	13072103-97	13072103-98	12073102 00	130/2103-22	13072103-100	13072103-100 13072103-101	13072103-100 13072103-101 13072103-101	13072103-100 13072103-101 13072103-102 13072103-103	13072103-100 13072103-101 13072103-101 13072103-103 13072103-103	13072103-100 13072103-101 13072103-102 13072103-103 13072103-104	13072103-100 13072103-100 13072103-101 13072103-102 13072103-103 13072103-104 13072103-106	13072103-100 13072103-100 13072103-101 13072103-102 13072103-104 13072103-105 13072103-106	13072103-100 13072103-100 13072103-100 13072103-104 13072103-104 13072103-106 13072103-106	13072103-100 13072103-100 13072103-100 13072103-104 13072103-104 13072103-105 13072103-106 13072103-106 13072103-106	13072103-100 13072103-100 13072103-100 13072103-103 13072103-103 13072103-105 13072103-106 13072103-106 13072103-108 13072103-108 13072103-109																								
  |   |  |  |   |  
  |   |  |   |  |  
  |  |   | 그 보다는 아니는 사람들은 요즘 보고 있다면 보다면 보다. 이렇게 되었다면 하는 것이 되었다면 하는데   | 그 부분 사람들은 사람들은 모든 보고 살아보고 보고 보는 것이 없었다. 그 이번 그런  | 그 보이는 아니라 사용을 하다 보고 살아보고 보는 보이 가장이다. 그런 그리고 아니라 그리고 아니라 그리고 아니라 가장이다. 그리고 아니라 그렇게 하는데 그리고 아니라 그리고 아니라 그렇게 되었다.  
   | 그 보이스 아니스 아이들은 그리고 보고하다고 그는 그는 것이 되었다. 그는   | 그 부가 살아내는 생물을 다른 그 살아보고 그는 그는 것이 없었다. 그는 그들은 사람들이 되었다면 살아보다 되었다면 살아보다 되었다면 살아보다 살아보다 살아보다 살아보다 살아보다 살아보다 살아보다 살아보다   | 그 얼마나 되고 있어요. 그리고 얼마나 모든 얼마나 가장이 되었다. 그 그리고 그리고 그리고 그리고 그리고 그리고 그리고 그리고 그리고 그  | 그 얼마나 되고 있어요요. 그는 얼마나 그는 얼마나 그는 말이 가장이다면 하는데 하는데 그리고 있다면 하는데 그는데 하는데 하는데 하는데 하는데 하는데 하는데 하는데 하는데 하는데 하  | 그 얼마나 되고 있어요요. 그는 그 말이다고 그는 말이 가장이 되었다. 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그   | 그 살이는 아니라 사용을 하다가 잘 살았다. 그는 살이 가장하는 것이 되었다면 하는데 그리고 있다면 하는데 하는데 하는데 하는데 하는데 하는데 나를 하는데  
   |

TABLE 1. (Continued)

	0.050 268.8 ± 9.6	
		0.328 ± 0.050 268.8 ± 9.6
	0.046 262.0 ± 8.9	± 0.0014 0.318 ± 0.046 262.0 ± 8.9
	0.064 253.6 ± 12.1	± 0.0019 0.331 ± 0.064 253.6 ± 12.1
	0.040 252.9 ± 8.5	± 0.0013 0.307 ± 0.040 252.9 ± 8.5
	0.133 266.3 ± 15.3	± 0.0024 0.793 ± 0.133 266.3 ± 15.3
	0.042 279.6 ± 8.7	± 0.0014 0.355 ± 0.042 279.6 ± 8.7
	0.014 243.9 ± 4.7	1,0007 0.277 ± 0.014 243.9 ± 4.7
	0.029 282.2 ± 7.0	1,0011 0,338 ± 0.029 282.2 ± 7.0
	0.020 260.4 ± 5.6	1,0009 0.292 ± 0.020 260.4 ± 5.6
	0.041 278.5 ± 8.6	$0.350 \pm 0.041$ $278.5 \pm 8.6$
	0.057 273.8 ± 11.3	$0.342 \pm 0.057$ $273.8 \pm 11.3$
297.4 ± 19.1 255 ± 97	0.109 297.4 ± 19.1	0.0030 0.285 ± 0.109 297.4 ± 19.1
	0,109 297.4 ± 19.1	$0.285 \pm 0.109$ $297.4 \pm 19.1$
		The state of the s
260.4 ± 5.6 278.5 ± 8.6 273.8 ± 11.3 297.4 ± 19.1	0.020 0.041 0.057 0.109	0.0009 0.292 ± 0.020 0.0014 0.350 ± 0.041 0.018 0.342 ± 0.057 0.030 0.285 ± 0.109
	0.381 ± 0.004 0.307 ± 0.040 0.793 ± 0.042 0.277 ± 0.014 0.292 ± 0.020 0.350 ± 0.020 0.350 ± 0.041 0.342 ± 0.057 0.255 ± 0.109	0.0401 ± 0.0019 0.331 ± 0.004 0.0400 ± 0.0013 0.307 ± 0.040 0.0422 ± 0.0024 0.307 ± 0.040 0.0386 ± 0.0007 0.375 ± 0.032 0.0447 ± 0.0011 0.338 ± 0.029 0.0412 ± 0.0009 0.292 ± 0.020 0.0444 ± 0.0014 0.388 ± 0.020 0.0434 ± 0.0014 0.386 ± 0.041 0.0434 ± 0.0018 0.342 ± 0.057